



UNIVERSITY OF
LEICESTER

Engineering performance of thermoelectrics for space radioisotope power systems

Hugo Williams

Ramy Mesalam

Richard Ambrosi

hugo.williams@le.ac.uk

@DrHRWilliams



Acknowledgements

Emily Jane Watkinson, Jon Sykes, Tony Crawford, Alessandra Barco
University of Leicester, Leicester UK



Daniel P. Kramer, Chadwick D. Barklay,
University of Dayton Research Institute, Dayton, Ohio, US



Jorge García-Cañadas
Universitat Jaume I, Castellón, Spain



Keith Stephenson
European Space Agency, ESTEC, Noordwijk, The Netherlands



Susan White, OSU Reactor Team
Ohio State University, Columbus, Ohio, US



Kevin Simpson, Mark Robbins
European Thermodynamics Ltd., Kibworth, Leicestershire, UK.



Mike Reece, Huanpo Ning, Kan Chen
Queen Mary University of London, London, UK.



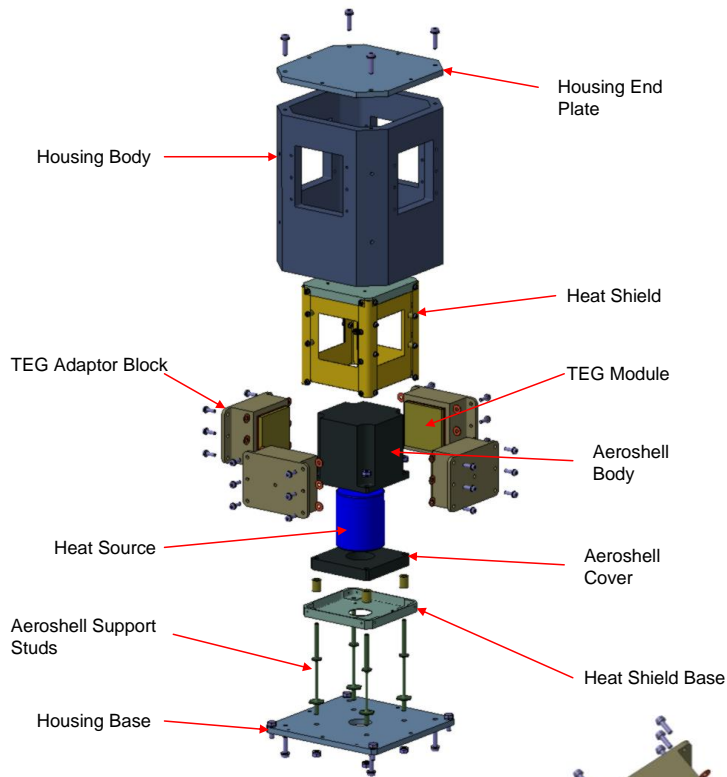
Contents

- European Radioisotope Thermoelectric Generator (RTG) development
 - Update on laboratory 'breadboard' prototype with upgraded cooling performance.
- Engineering challenges for thermoelectric modules in space RTGs
 - Radiation damage
 - Mechanical properties
- Future work

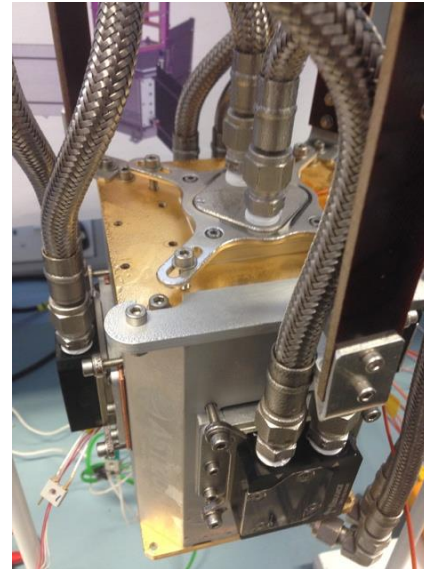
RTG Development in the UK

- UoL has led RTG system development in UK under contract to ESA since 2010:
 - PI: Prof. Richard Ambrosi, UoL
- Aim: Develop a first iteration RTG design for Europe optimised for ^{241}Am fuel
- Designed, built and tested a small-scale lab prototype:
 - Target power $5 W_e$ from $83 W_{th}$ (electrically heated)
 - Develop a test bed for the integrated system performance of thermoelectric materials & modules
- Produced a $10 W_e$ refined flight design based on this architecture

Laboratory RTG System

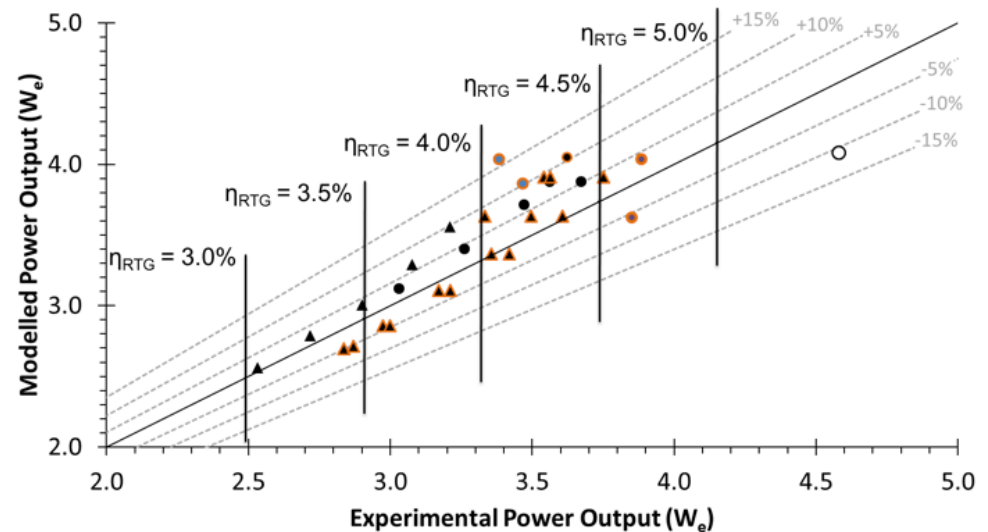
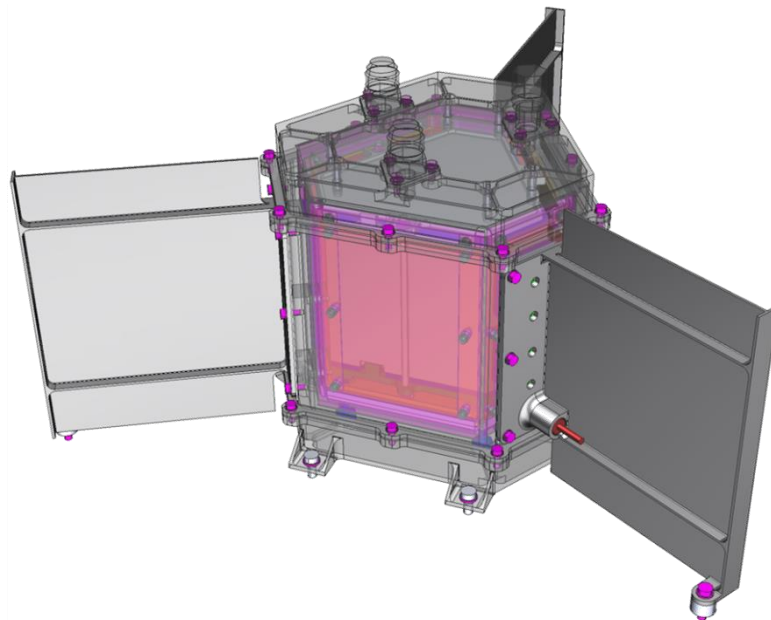


- 80 W thermal.
- 4.5 W electric.



European Design

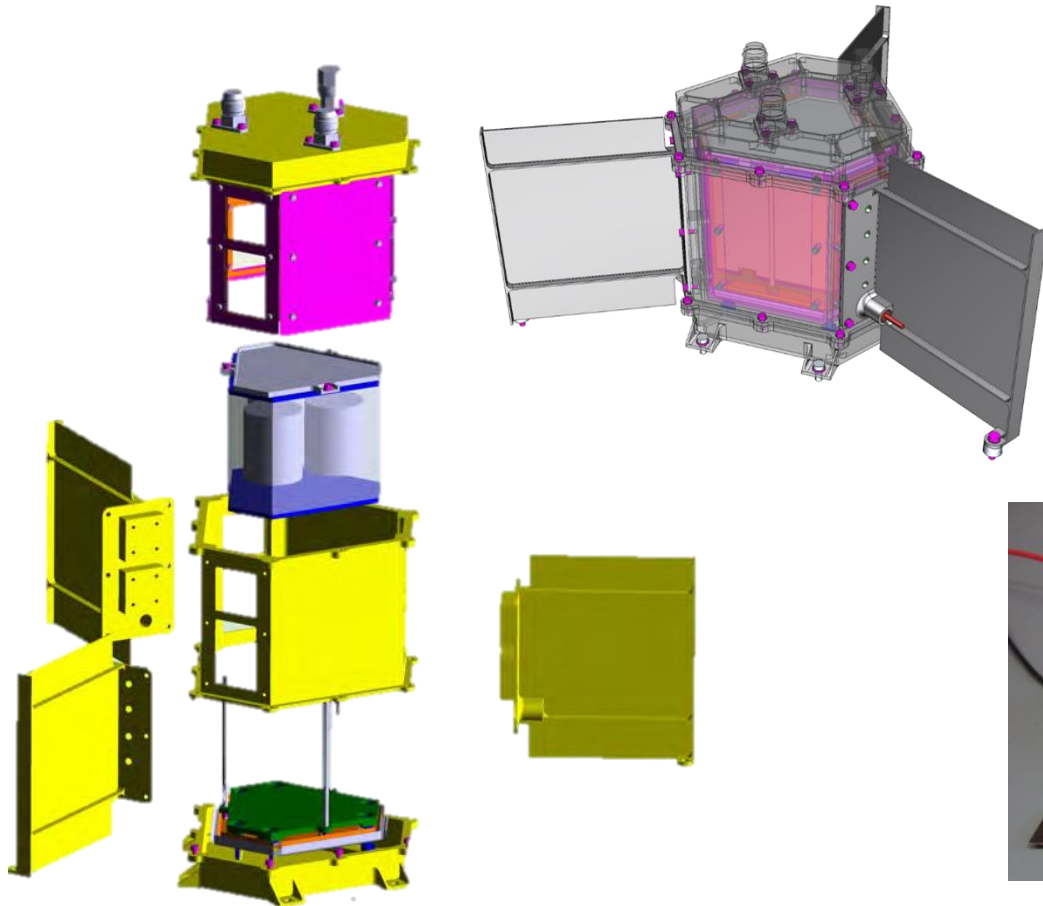
- Lab prototype produced up to ~4.5 W of electrical power, matching predictions and delivering an efficiency ~5.5%.



- 6 mm, Ti heatshield
- 6 mm BST, Au heat shield
- ▲ 8 mm, Ti heatshield
- 6 mm + Au heat shield
- ▲ 8 mm, Ti heatshield
- 6 mm BST + B4C, Au heat shield
- 6mm, BST+B4C, Au h/s New cooling Sys

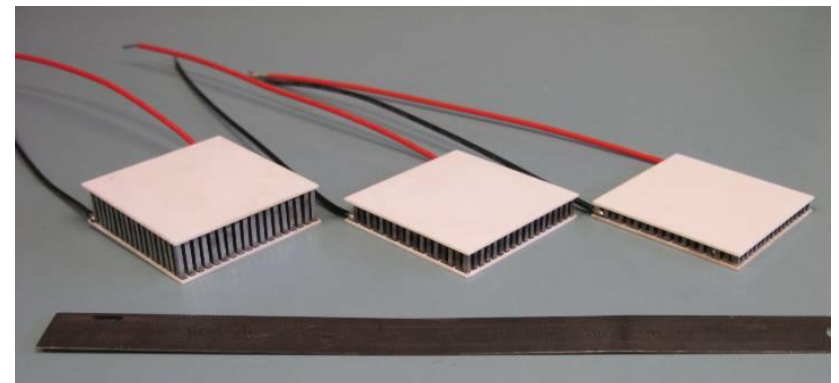
- Flight design would produce 10 W of electrical power.
- Flight designs would be scalable to 50 W.
- Flexibility to tailor to mission requirements.

RTG Architecture & implications



For the thermoelectrics:

- Bi_2Te_3 based materials
- Compression & shear loading
- Modules with high aspect ratio legs



RTG Neutron Emission

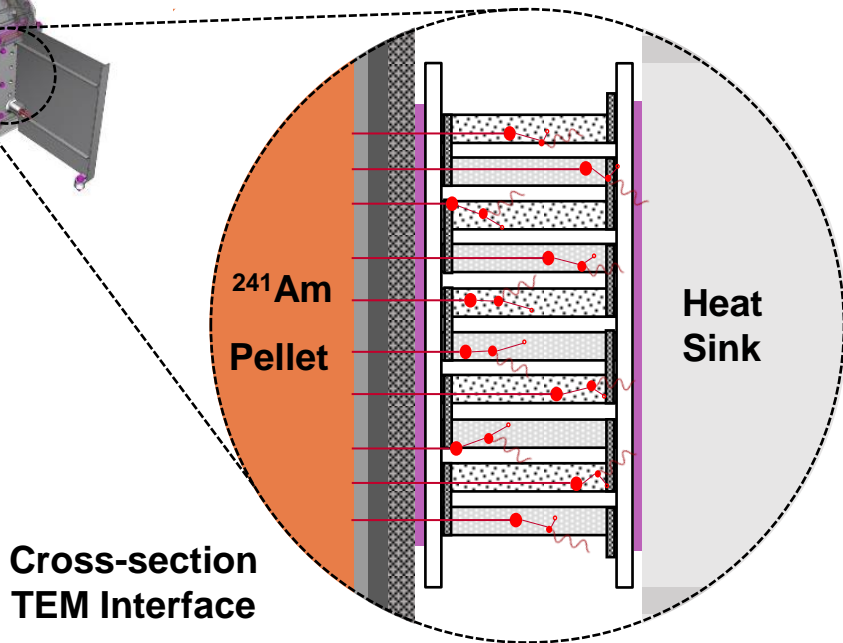
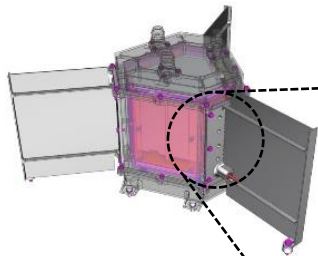
Assuming a
10 year life span

5 years of initial exposure

System assembly and integration, storage, transfer to launch site and then integration on spacecraft and finally launch.

5 year nominal mission exposure

$$\sim 5 \times 10^{13} \text{ n/cm}^2 \text{ (>1MeV)}$$



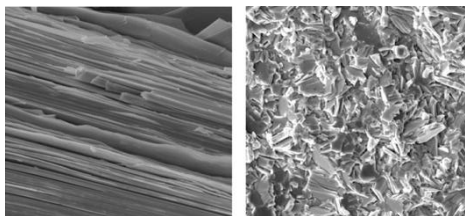
- Neutron Radiation
- Fuel Pellet Cladding
- Insulation
- Aeroshell
- Thermal Interface Material (TIM)
- } Thermoelectric Module Clusters
- }

**Cross-section
TEM Interface**

Literature Review

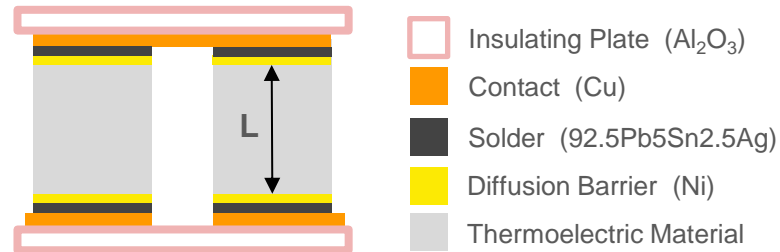
| Research group | Year | Specimen | Total Integrated Flux | | $\frac{S_1^1}{S_2^0}$ | $\frac{\rho_1^1}{\rho_2^0}$ | $\frac{\lambda_1^1}{\lambda_2^0}$ | Annealing Temp (°C) |
|--------------------|------|---------------------------------------------------------------------------|------------------------|------------------------|-----------------------|-----------------------------|-----------------------------------|---------------------|
| | | | Thermal | >1Mev | | | | |
| Danko et al. [1] | 1962 | Bi _{0.05} Ge _{0.95} Te | 9.4 x 10 ¹⁸ | | 1.15 | 1.10 | ~ | 300 |
| Danko et al. [1] | 1962 | Bi _{0.05} Ge _{0.95} Te | 2.7 x 10 ¹⁹ | 1.5 x 10 ²⁰ | 2.40 | 2.00 | ~ | 300 |
| Corelli et al. [2] | 1960 | Bi ₂ Te ₃ -n type | 1.5 x 10 ²⁰ | 1.6 x 10 ¹⁹ | 1.16 | 5.00 | 0.88 | 200 |
| Corelli et al. [2] | 1960 | Bi ₂ Te ₃ -n type | ~ | 1.6 x 10 ¹⁹ | 1.04 | 2.60 | ~ | 200 |
| Idnurm et al. [3] | 1967 | Bi ₂ Te ₃ -n type | 2.0 x 10 ¹⁸ | ~ | 1.03 | 1.13 | 0.96 | ~ |
| Corelli et al. [2] | 1960 | Bi ₂ Te ₃ -p type | 1.5 x 10 ²⁰ | 1.6 x 10 ¹⁹ | -1.05 | 2.00 | ~ | 200 |
| Corelli et al. [2] | 1960 | Bi ₂ Te ₃ -p type | ~ | 1.6 x 10 ¹⁹ | -0.82 | 1.2 | ~ | 200 |
| Idnurm et al. [3] | 1967 | Bi ₂ Te ₃ -p type | 2.0 x 10 ¹⁸ | ~ | 1.00 | 1.13 | 0.98 | ~ |
| Idnurm et al. [3] | 1967 | Bi ₂ Te ₃ - Sb ₂ Te ₃ -n type | 2.0 x 10 ¹⁸ | ~ | 0.95 | 1.18 | 0.97 | ~ |
| Idnurm et al. [3] | 1967 | Bi ₂ Te ₃ - Sb ₂ Te ₃ -p type | 2.0 x 10 ¹⁸ | ~ | 0.99 | 0.93 | 1.02 | ~ |

Pre-irradiation Characterisation



Directional

Polycrystalline



| Module No. | P-type | N-type | Crystallographic Structure | L (mm) | No. of Couples |
|------------|---------------------------------------------|--------------------------|-------------------------------------------------------|--------|----------------|
| 2 | Bi_2Te_3 | Bi_2Te_3 | Directional Solidification | 8 | 161 |
| 3 | Bi_2Te_3 | Bi_2Te_3 | Directional Solidification | 8 | 161 |
| 4 | Bi_2Te_3 | Bi_2Te_3 | Directional Solidification | 6 | 161 |
| 5 | $\text{Bi}_{0.5}\text{Sb}_{1.5}\text{Te}_3$ | Bi_2Te_3 | p - Polycrystalline n - Directional Solidification | 6 | 161 |

TEG Irradiation Procedure

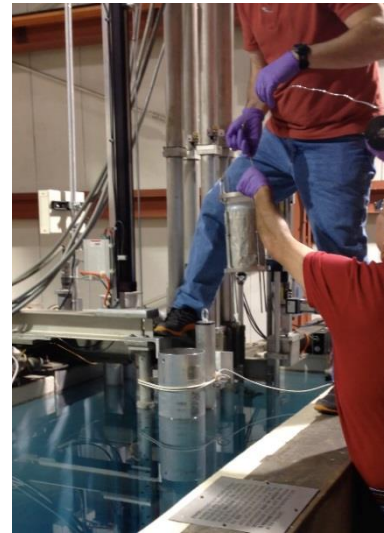
Placing into dry tube



TEG hanger assembly



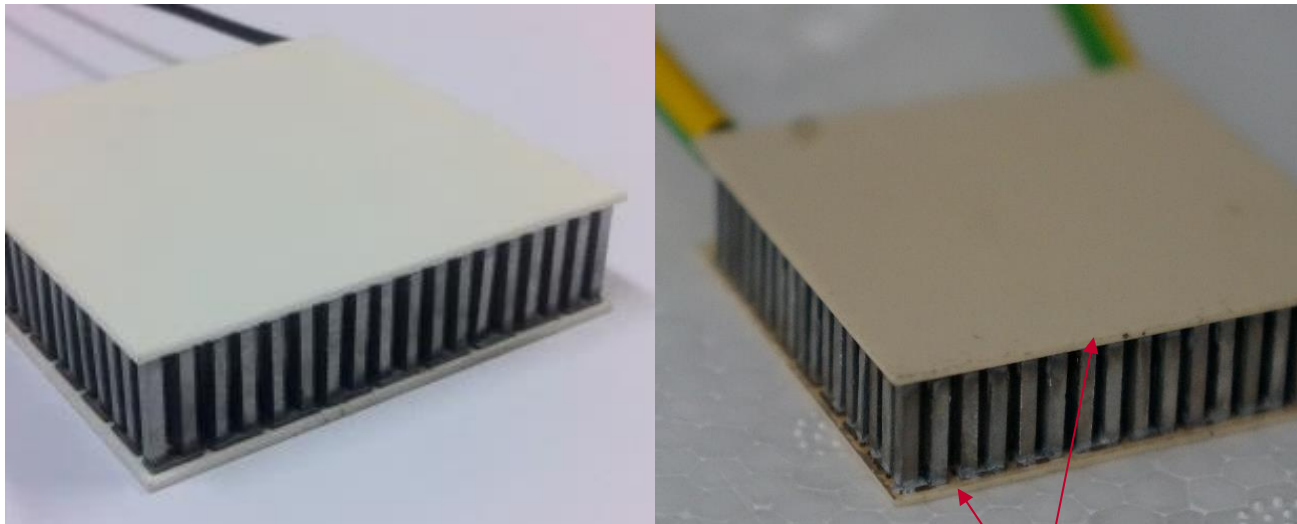
Cadmium shielded enclosure



Acute 2hr exposure

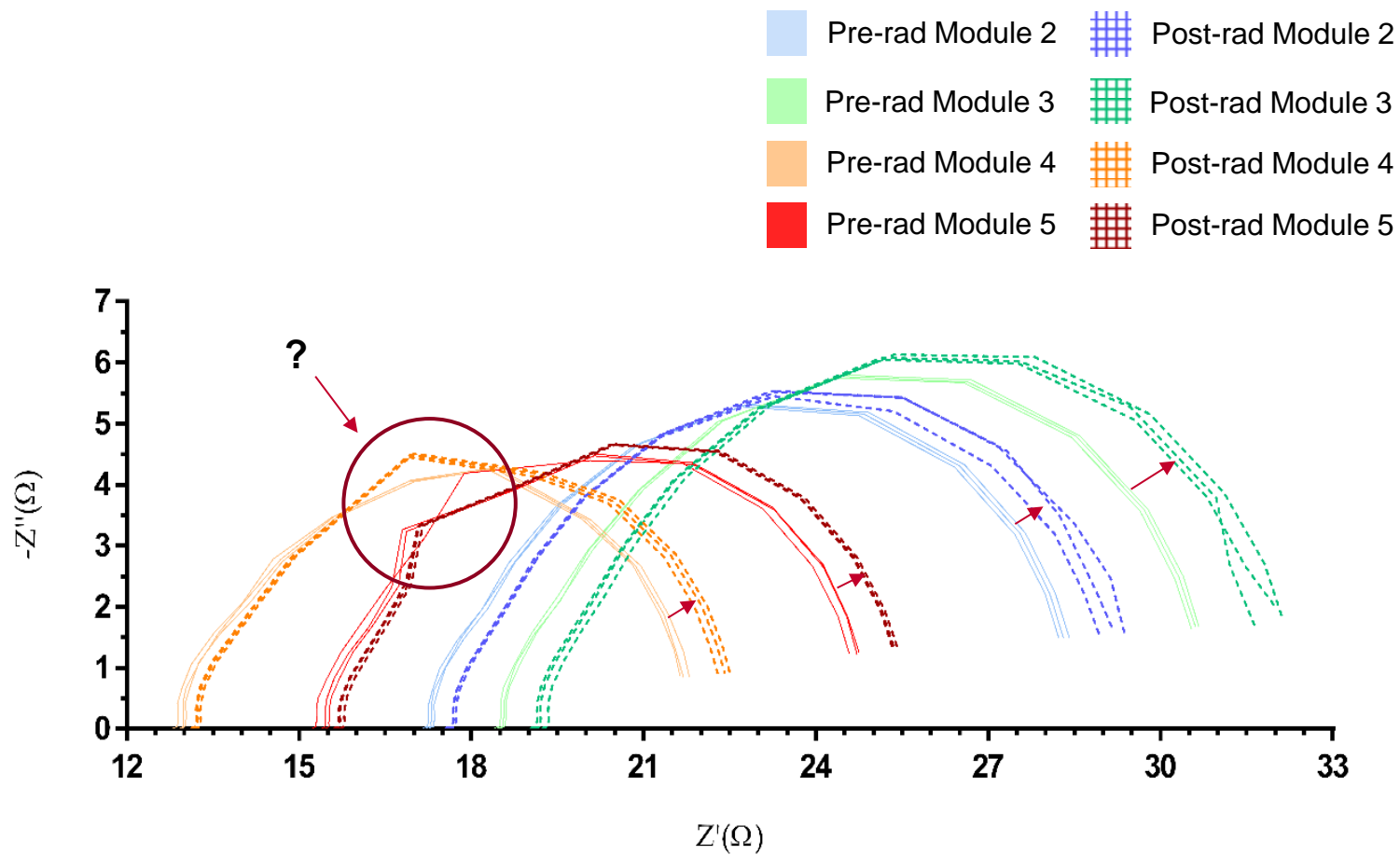
Post-irradiation Observations

Pre Post

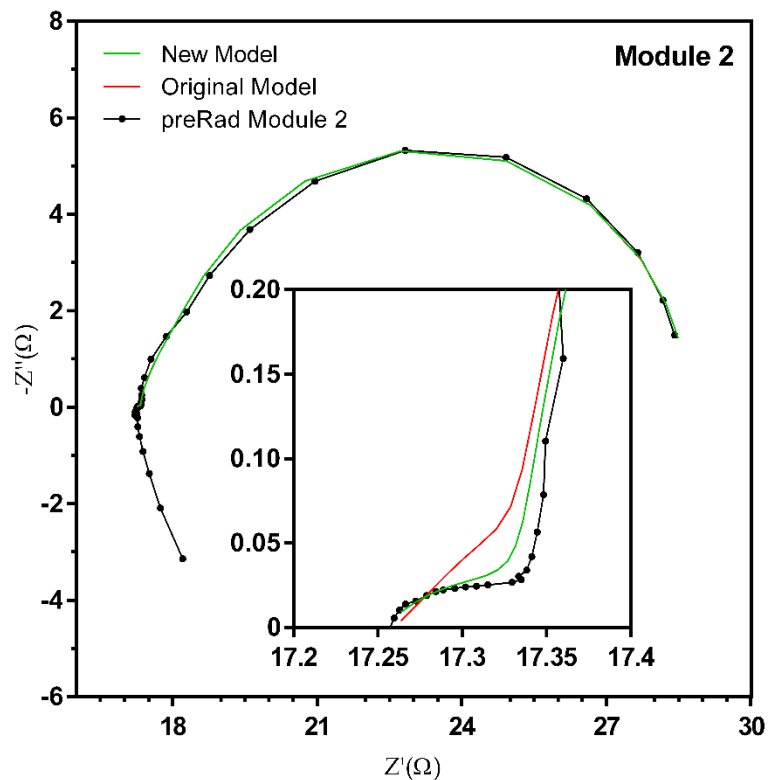
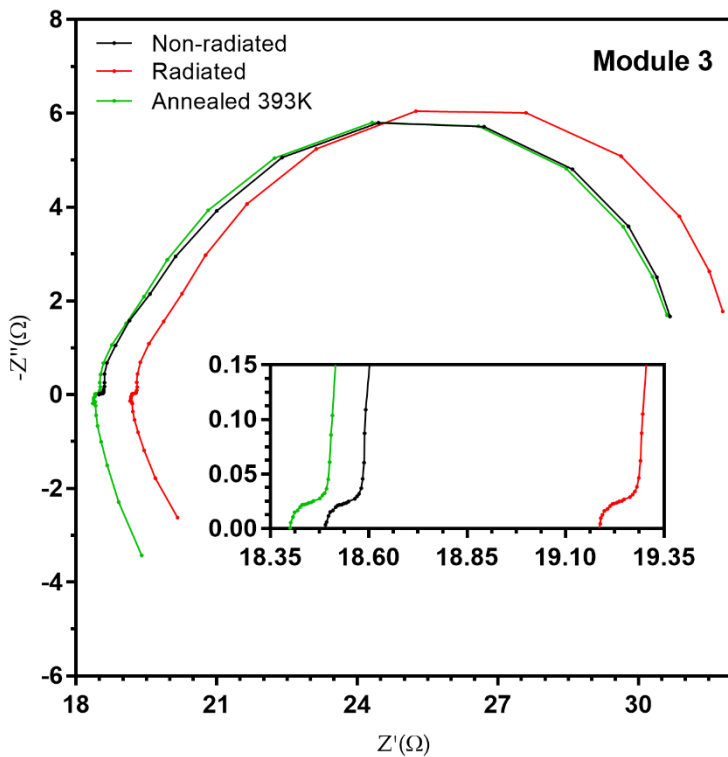


Discolouration

Impedance Spectroscopy

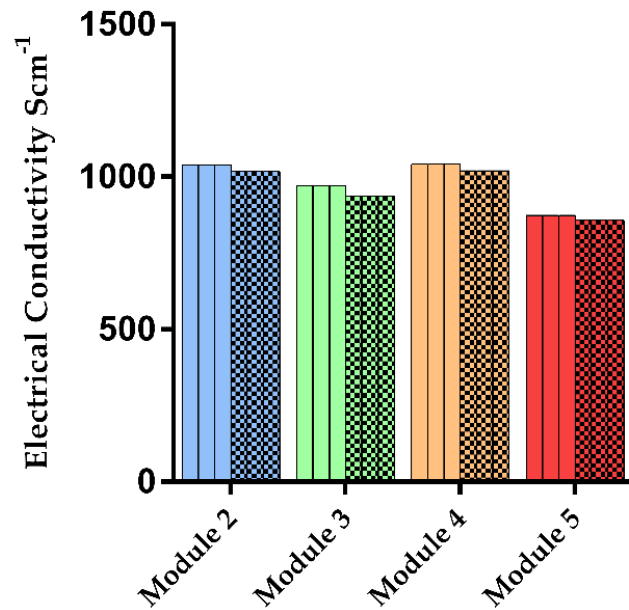


Impedance Spectroscopy

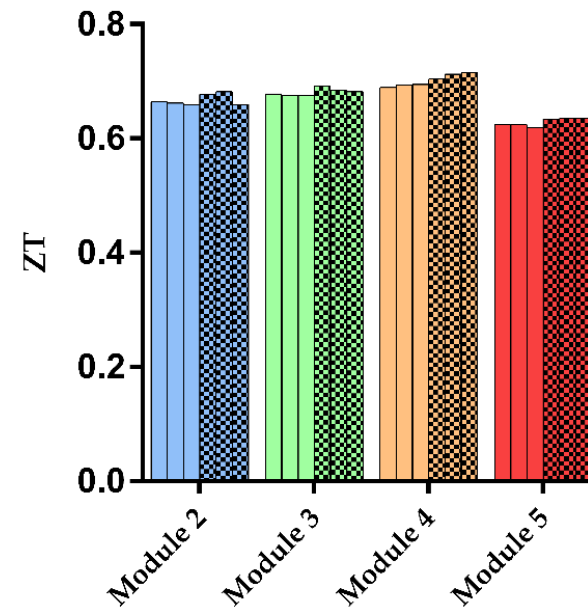


Thermoelectric Properties

~2% increase in Resistivity

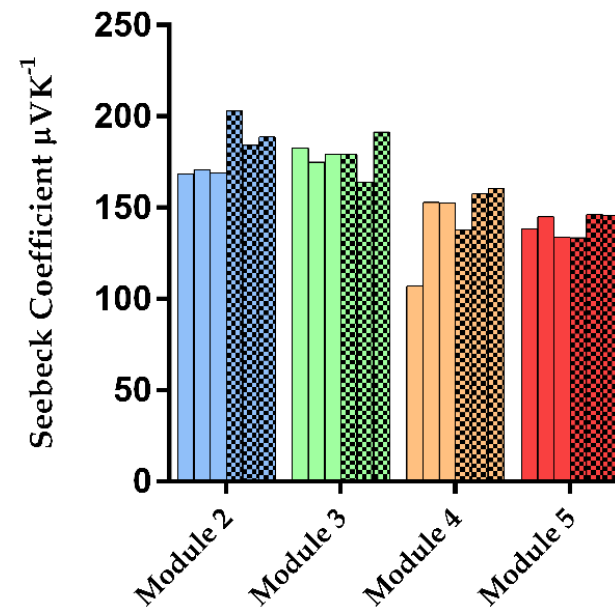
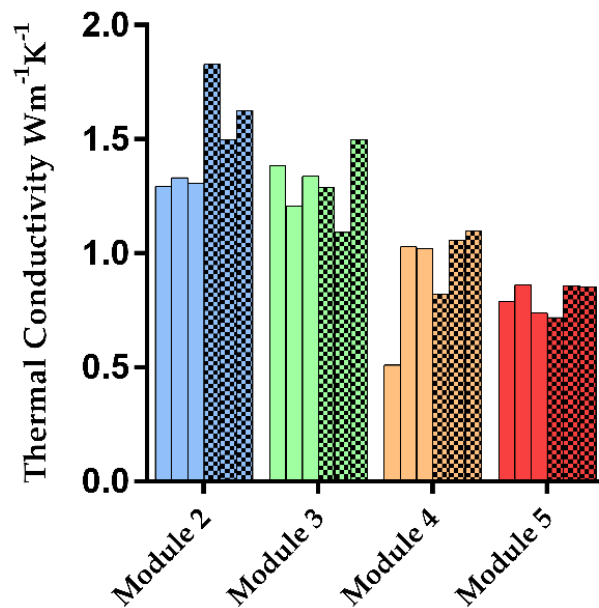


~2% increase in ZT



Thermoelectric Properties

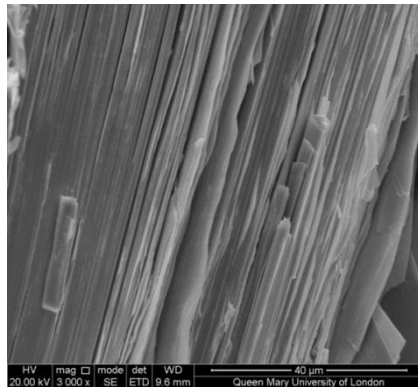
Peak increases observed however results suffer greater variation



Enhanced Bi_2Te_3 thermoelectrics

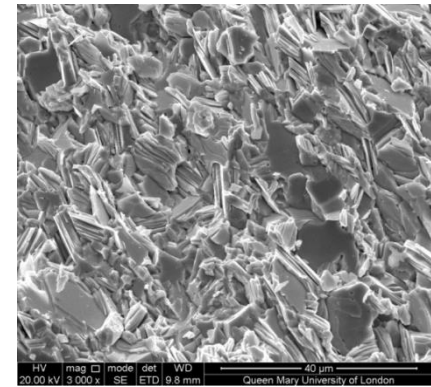
- Most active research on thermoelectric materials focuses on zT
- Mechanical properties and behaviour of materials and modules is under-represented in the literature.

Conventional material production is by directional solidification



Very poor strength and/or toughness
← due to cleavage along the basal crystallographic plane || to growth

Polycrystalline, fine grained materials: better mechanical properties

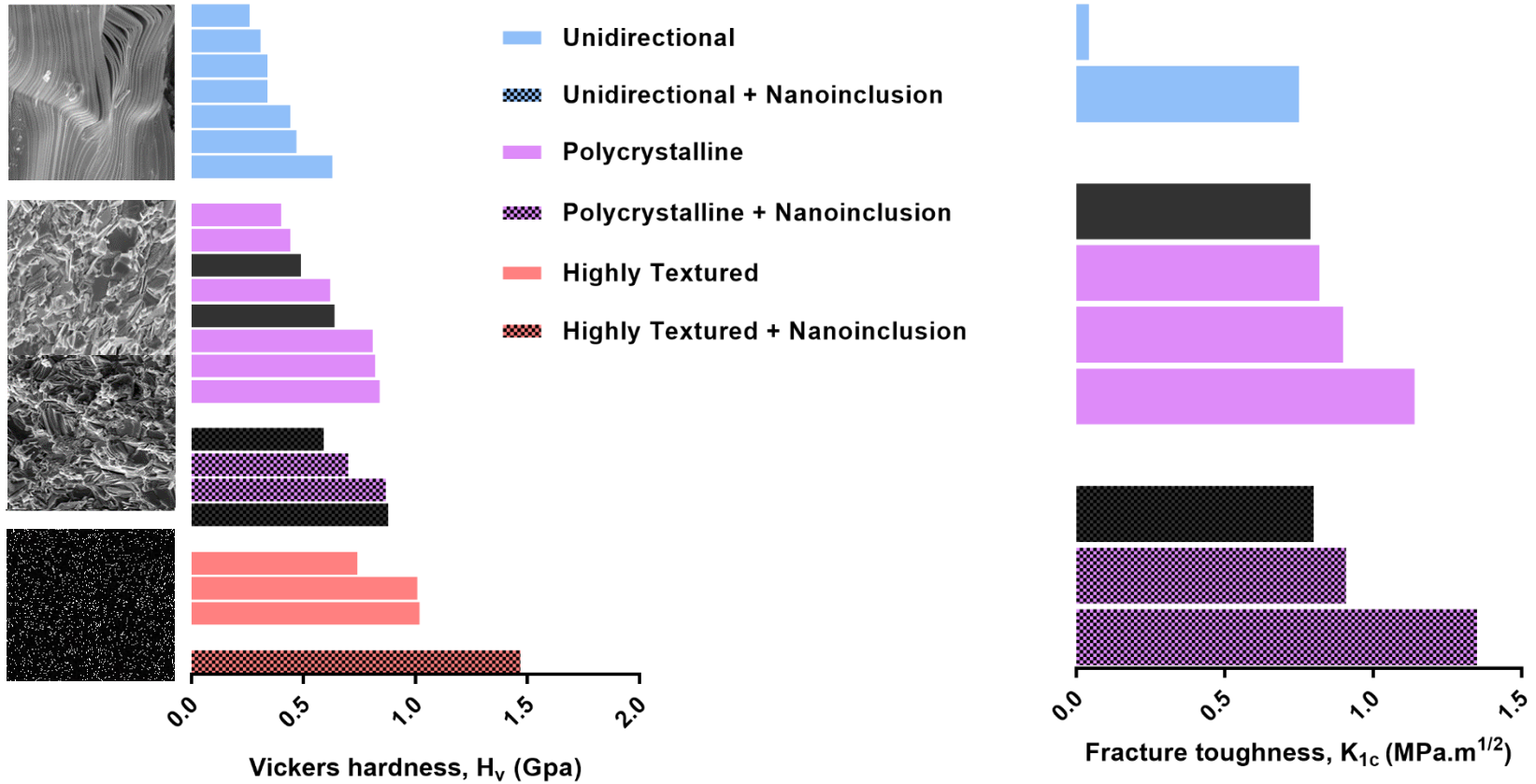


Williams HR et al. 2015. Spark Plasma Sintered bismuth telluride-based thermoelectric materials incorporating dispersed boron carbide. *Journal of Alloys and Compounds*. **626**. 368-374.

Room Temperature Characterisation

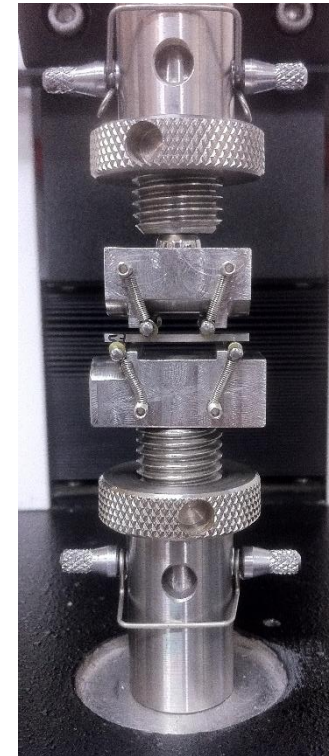
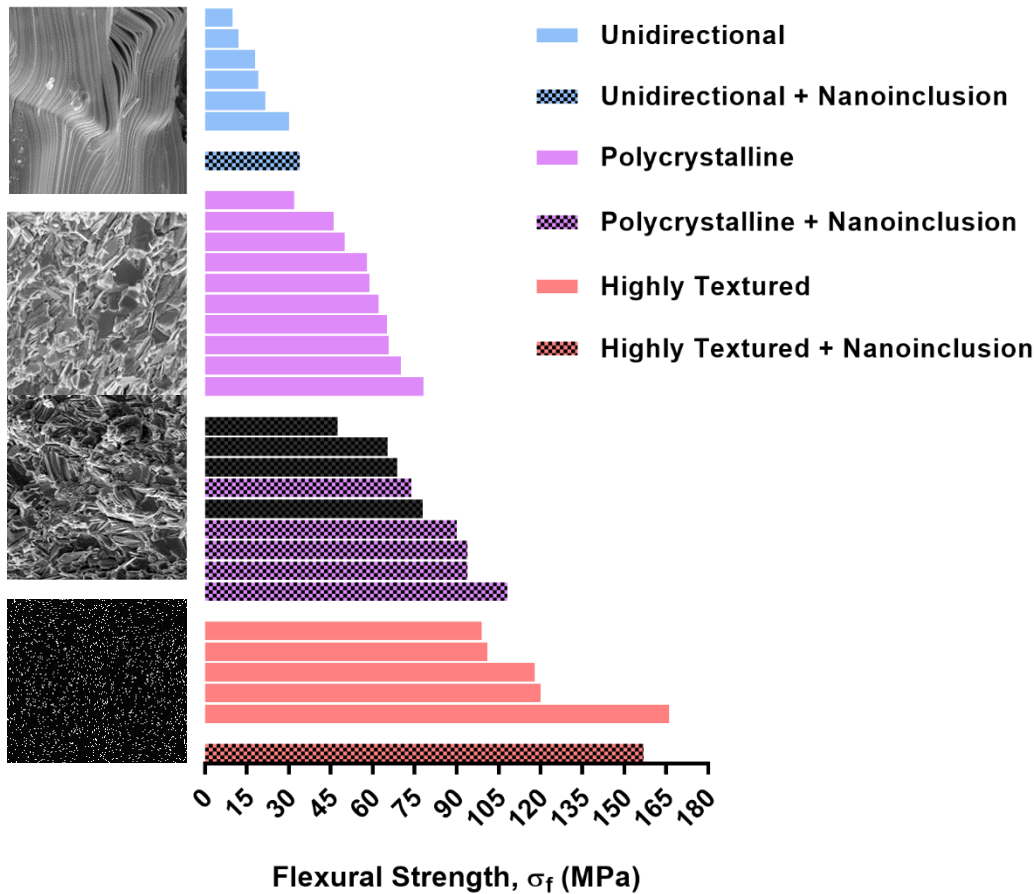
| Property | | Procedure | Coupon Size | Sample Size | Statistical Analysis |
|------------|--------------------|-------------------------------------|--------------------------------|-------------|----------------------|
| σ_f | Flexural Strength | ASTM C1161 (4pt-Bending) | 1.5 x 2.0 x 25 mm ³ | 30 | Weibull |
| K_{Ic} | Fracture Toughness | ISO 23146 (SEVNB) | 3.0 x 4.0 x 25 mm ³ | 30 | N/S |
| E | Elastic Modulus | ISO 14577 (Nanoindentation) | N/S | 30 | N/S |
| H | Hardness | ASTM C1327 (Vickers Indentation) | N/S | 30 | N/S |

Hardness & Fracture Toughness

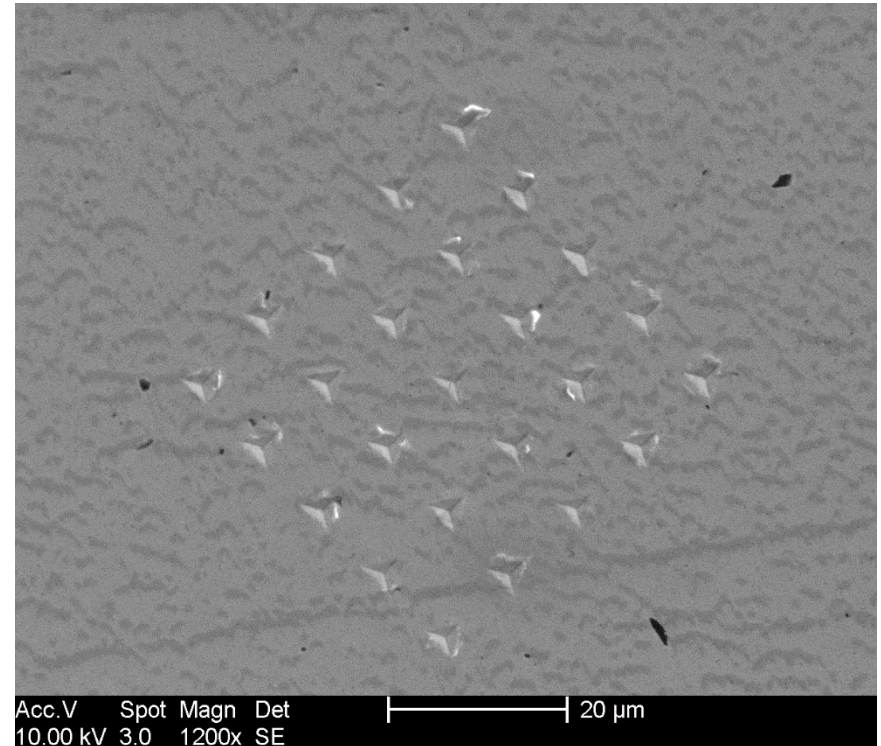
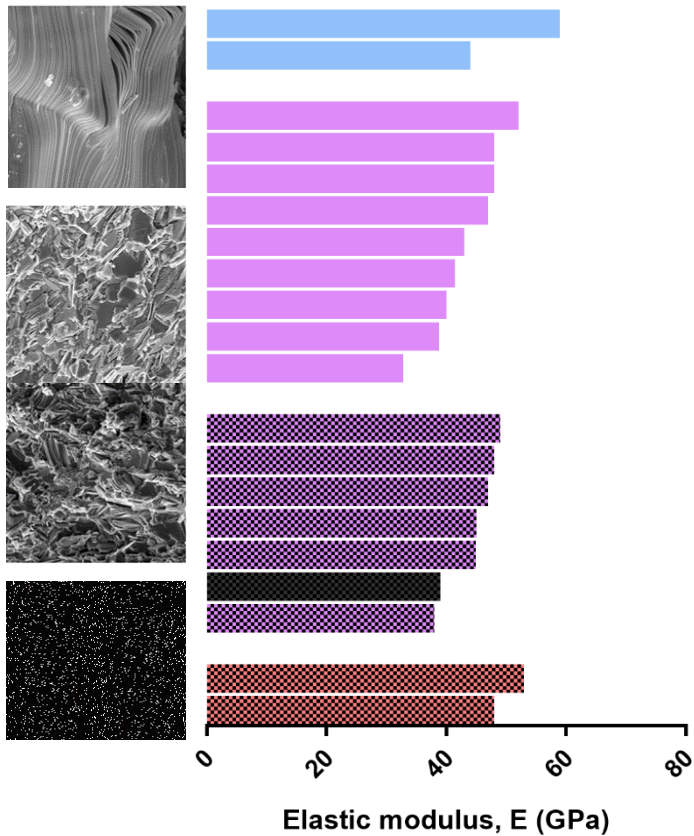


Flexural Strength Testing

500N Instron



Elastic Modulus



- Unidirectional
- Unidirectional + Nanoinclusion
- Polycrystalline
- Polycrystalline + Nanoinclusion
- Highly Textured
- Highly Textured + Nanoinclusion

Future Work

- Flight-like RTG lab prototype under development.
- Radioisotope Heater Unit Prototype also under development for ESA.
- Impedance spectroscopy shows promise for module level characterisation even if just on a comparative level.
- Devise a more robust and repeatable Impedance spectroscopy characterisation experimental setup.
- Further improve Impedance spectroscopy fitting.
- Investigate mechanical properties changes due to texturing on n-type bismuth telluride using a hot forging process combined with SPS