## PREDICTING THE RESPONSE TIME OF FIRE DETECTORS

Fire and Security Consulting Services is frequently asked about the response time of fire detectors.
Fire Engineering calculations often require that the response time of thermal (heat), and smoke detectors be determined to effect further calculations in respect to:-

1. Activation of occupant warning alarms;
2. Activation of Fire Brigade Alarms; and
3. Activation of smoke exhaust or ventilation systems.

Many computer fire modelling software programmes such as BranzFire and CFast incorporate subroutines that determine smoke detector and / or sprinkler activation with others such as FireCalc only providing calculations for sprinkler operation.

All these programmes are based on data determined by both testing and basic principles such as described below which can be used to determine activation times without recourse to the programmes.

## Thermal Detectors

The response time of thermal detectors can be determined by using the suite of computer programmes from the National Bureau of Standards in the USA known generally as DETACT. Within that suite there are four programmes:

DET 12 Fixed Temperature Operation, Metric Units.
DET 13 Fixed Temperature Operation, Imperial Units.
DET 13C Fixed Temperature Operation, Imperial Units, file input.
DETACT-T2 Fixed Temperature and Rate of Rise operation, metric or Imperial Units.
Within Australia, it is recommended that the programme DETACT-T2 be used where AS 1670 contemplates the use of combination fixed temperature and Rate of Rise detectors.

To properly determine the response time of a thermal detector the following data is required:

- Ambient temperature, usually $21^{\circ} \mathrm{C}$.
- Activation temperature, usually $57^{\circ} \mathrm{C}$, but may be $88^{\circ} \mathrm{C}$ (see note 1 below).
- $\quad$ Rate of Rise, usually $6^{\circ} \mathrm{C}$ per minute (see note 1 below).
- Ceiling Height.
- Detector spacing, for AS 1670 systems, 7.2metres (see note 2 below).
- Fire growth rate.
- Detector Response Time Index. RTI.

Note 1 In Australia there are five standard types of thermal detector:-

1. Type A - Fixed temperature of $57^{\circ} \mathrm{C}$ and 'rate of rise'.
2. Type B - Fixed temperature of $57^{\circ} \mathrm{C}$ only.
3. Type C - Fixed temperature of $88^{\circ} \mathrm{C}$ and 'rate of rise'.
4. Type D - Fixed temperature of $88^{\circ} \mathrm{C}$ only'.
5. Type E-Fixed temperature of varying temperatures.

Note 2 In Australia, detector spacing is determined by Australian Standard AS1670.1 - Fire detection, warning, control and intercom systems - System design, installation and commissioning. Part 1: Fire. This standard contemplates installation at 7.2 m centres as depicted in Figure 1 below.


Figure 1 - AS1670 Thermal Detector Spacing
In Australia you will be hard pressed to find out the RTI of detectors from manufacturers so the following will be of assistance.
The SFPE Handbook of Fire Protection Engineering in Section 3, Chapter 1, page 3-9, table 3-1.4 reproduces the chart shown in Figure 2 from NFPA 72E. This chart provides the "time constants" for any detector dependant on the activation temperature and "listed" spacing. The text then goes on to show how the RTI can be determined using the formula shown where 'tau' is the time constant from the table and 'u' is the reference velocity as either $5 \mathrm{ft} / \mathrm{sec}$ or $1.5 \mathrm{~m} / \mathrm{sec}$. The resultant RTI will be either imperial or metric dependant on which number for ' $u$ ' is used as the 'tau' number from the table is dimensionless.

| TABLE 3-1.4 Time Constants for Any Listed Detector$\left(D E T \text { TC) }(s)^{*}\right.$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Listed Spacing (ft) | $\mathrm{UL}\left({ }^{\circ} \mathrm{F}\right)$ |  |  |  |  |  | FM All Temp. |
|  | $128^{\circ}$ | $135^{\circ}$ | $145^{\circ}$ | $160^{\circ}$ | $170^{\circ}$ | $196^{\circ}$ |  |
| 10 | 400 | 330 | 262 | 195 | 160 | 97 | 195 |
| 15 | 250 | 190 | 156 | 110 | 89 | 45 | 110 |
| 20 | 165 | 135 | 105 | 70 | 52 | 17 | 70 |
| 25 | 124 | 100 | 78 | 48 | 32 |  | 48 |
| 30 | 95 | 80 | 61 | 36 | 22 |  | 36 |
| 40 | 71 | 57 | 41 | 18 |  |  |  |
| 50 | 59 | 44 | 30 |  |  |  |  |
| 70 | 36 | 24 | 9 |  |  |  |  |
| NOTE: These time constants are based on an analysis of the Underwriters Laboratories inc. and Factory Mutual listing test procedures. Plunge test results performed on the detector to be used will give a more accurate time constant. <br> - $A:$ a reference velocity of $5 \mathrm{Hs}(1.5 \mathrm{~m} / \mathrm{sec})$ <br> (Reproduced from NFPA 72E-1984, Appendix C. ${ }^{2}$ ) |  |  |  |  |  |  |  |
| $\mathrm{RTI}=\tau_{0} u_{0}^{1 / 2}$ |  |  |  |  |  |  |  |

Figure 2 - NFPA 72E Chart
The next requirement is to obtain the listed spacing. Figure 3 shows an extract from the UL listing shows that for a Wormald Mk. 1 combination detector (Type A); the time constant is 44 and the listed spacing is 50 ft .

[^0]Figure 3 - UL Listing of a typical detector (Wormald Mk. 1)

Therefore for this detector, RTI $=44 \times(1.5)^{0.5}=53.8$ metric.
With the above information at hand we can now use DETACT-T2 to determine the response time in any given situation.
Figure 4 shows the input of a particular scenario and Figure 5, the corresponding results.

| ci DETACTT2.EXE | - $\square \times$ |
| :---: | :---: |
| DETACT-T2 VERSION 1.0 WRITTEN BY D. ${ }^{\text {VI }}$. STROUP | $\triangle$ |
| CONTRIBUTION OF THE <br> NATIONAL BUREAU OF STANDARDS (U.S.). <br> NOT SUBJECT TO COPYRIGHT. |  |
| Calculates detector actuation time BELOW UNCONFINED CEILINGS WITH time squared fire growth rates. |  |
| FOR COMPILED VERSION ONLY <br> Portions (C) Copyright Microsoft Corp., 1981, 1983, 1984, 1985. <br> All rights reserved. |  |
| $\begin{aligned} & \text { ENTER: } 12 \text { FOR ENGLISH UNIT INPUT } \\ & 2 \end{aligned}$ |  |
| enter the ambient temperature in degrees c. 21 |  |
| ENTER THE DETECTOR RESPONSE TIME INDEX (RTI) IN (M-SEC)**1/2. 53.8 |  |
| ENTER THE DETECTOR ACTIVATION TEMPERATURE IN DEGREES C. 57 |  |
| ENTER A DETECTOR RATE OF RISE IN DEGREES C/MINUTE. 6 |  |
| ENTER THE CEILING HEIGHT IN METERS. 2.7 |  |
| ENTER THE DETEGTOR SPACING IN METERS. 7 |  |
| ENTER: S FOR SLOW FIRE GROWTH RATE <br> M FOR MEDIUM FIRE GROWTH RATE <br> F FOR FAST FIRE GROWTH RATE <br> U FOR ULTRAFAST FIRE GROWTH RATE OR <br> 0 FOR OTHER |  |
| F | $\checkmark$ |

Figure 4 - DETACT-T2 Inputs


Figure 5 - DETACT-T2 Results

## Smoke Detectors

The response time of smoke detectors will depend entirely on three factors:

1. The type of detector, either ionisation or photo-optical.
2. The type of fuel involved.
3. The optical density of the smoke produced.

In the NIST programme HAZARD $I$, it is suggested that the response time of smoke detectors be calculated by the resident DETACT programme using an RTI of 1 . This is probably valid for the purposes of the entire HAZARD I programme in residential occupancies, where other criteria such as Tenability is accounted for, but where we need to demonstrate in isolation the response time it is suggested the following. The NIST programmes FAST and CFAST are an evolution of HAZARD I and maintain the same system of determining smoke detector activation.

In the CSIRO suite of programmes entitled FIRECALC, the programme HotLayer is used to determine compartment conditions in a fire. Part of the output is the optical density of the smoke layer at the ceiling and these figures can be used to estimate the time for smoke detector activation.
Figure 6 depicts a fire scenario in the fist 30 seconds of an ULTRA-FAST fire in a specified situation. You will see that at 10 seconds that the ceiling jet optical density is $0.061 / \mathrm{m}$.


Figure 6 - HotLayer Results
Figure 7 below, is a comparison of optical density and obscuration based on data from Drysdale - An Introduction to Fire Dynamics, and data from the SSL test requirements for smoke detectors, AS1603.2, which requires tested smoke detectors to activate when the smoke outside the detector is between 3 and $12 \%$ per metre.


Figure 7 - Optical Density / Obscuration
The optical density of 0.06 equates to an obscuration of $10.5 \%$ which is above the average value allowable in the AS 1603.2/SSL tests for operation of the detector.
Acordingly the predicted response time in this scenario is 10 seconds. In practice and using an analogue addressible detection system where detector polling time needs to be included, the alarm response time is likely to be between 30 and 60 seconds.
I trust that this paper provides information that you will find helpful.
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[^0]:    WORMALD U S INC, MARINETTE WI 54143
    S2575 (N)
    Model MK1, fixed-temperature, combination fixed temperature, rate-of-rise operation. Temperature ratings, $135,194 \mathrm{~F}$
    Distance between thermostats on smooth ceilings and large bays shall not be in excess of 50 f and distance of thermostat from any wall or partition shall not be more than 25 ft for the combination type.
    Distance between thermostats on smooth ceilings and large bays shall not be more than 15 ft and distance of thermostat from any wall or partition shall not be more than $7 \frac{1}{2} \mathrm{ft}$ for the fixed temperature type.

