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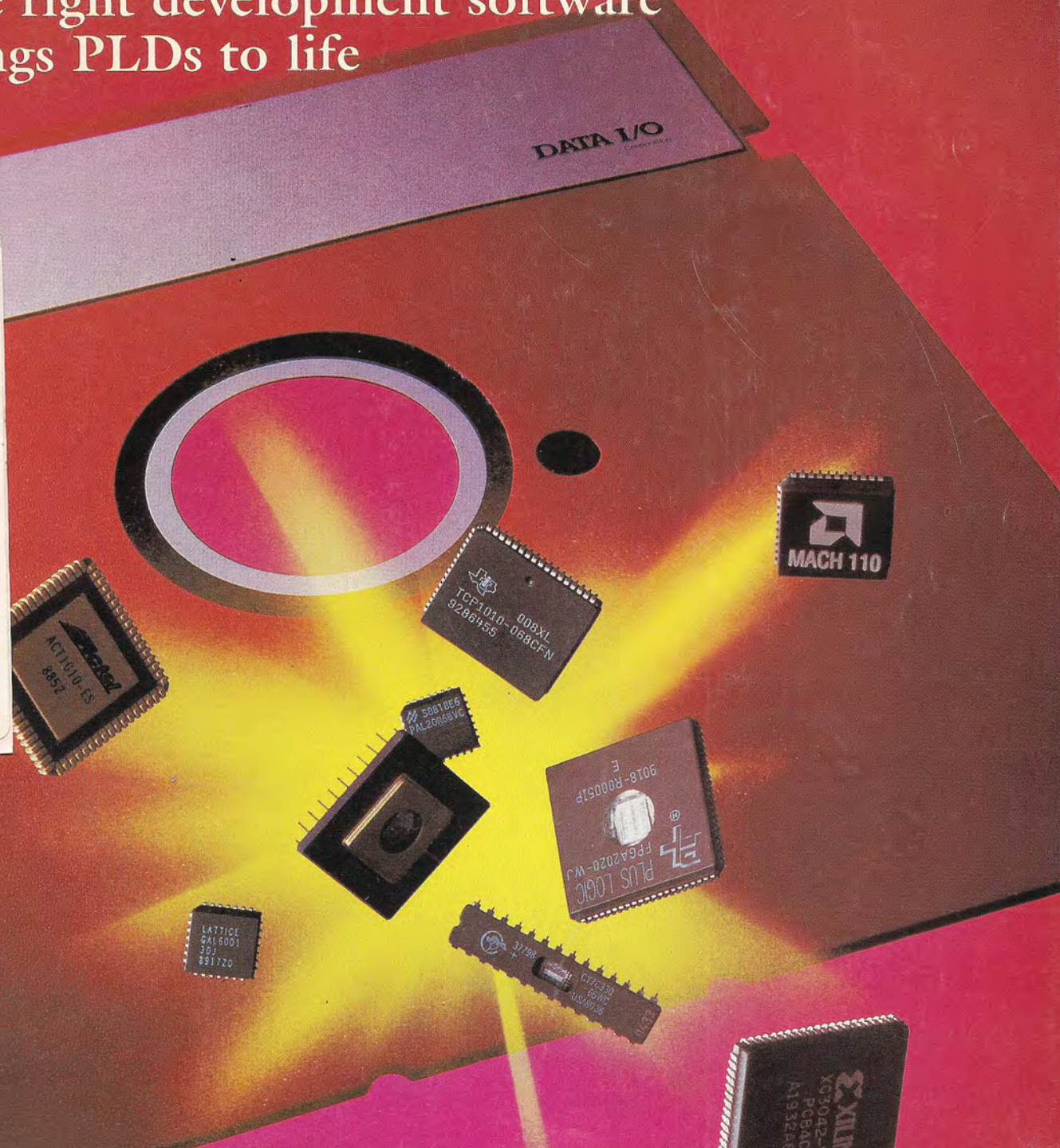
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DESIGN IDEAS

EDITED BY CHARLES H SMALL

Passive network is totally resistive

Prayson Pate
BNR, Research Triangle Park, NC

The circuit in Fig 1a looks trivial, but it isn't. It can provide a resistive termination to a transmission line over a wide bandwidth—much wider than you can achieve with op amps. Further, you can extend the circuit to make multipole lowpass, highpass, and bandpass filters. Note that although the circuit resembles a tank circuit, it doesn't ring. In fact, ringing arising from component mismatch is small for reasonable component tolerances.

To calculate the circuit's impedance, first let $Z_1 = R \parallel L$ and $Z_2 = R \parallel C$. If $\omega_1 = R/L$ and $\omega_2 = 1/RC$, then

$$Z_1 = R/(1 + j\omega/\omega_1)$$

and

$$Z_2 = R/(1 + j\omega_2/\omega)$$

Thus the circuit's input impedance equals $Z_1 + Z_2$, or

$$Z_{IN} = R(1 + (j\omega/\omega_2 + \omega_1/j\omega) + 1)/(1 + j\omega/\omega_2 + \omega_1/j\omega + \omega_1/\omega_2)$$

This expression reduces to simply R if $\omega_1 = \omega_2 = \omega_0$.

You can calculate values for L and C simply:

$$L = \omega_0/R = 2\pi/F_0$$

and

$$C = 1/\omega_0 R = 1/2\pi F_0$$

The circuit's transfer function is then:

$$H(j\omega) = Z_2/Z_{IN} = 1/(1 + j\omega/\omega_0),$$

which is the same transfer function as a simple LC lowpass filter.

You can realize more elaborate circuits by various combinations of the RL and RC subcircuits. Swapping the subcircuits in the circuit in Fig 1a yields a highpass circuit with the same pole. Fig 1b shows a 2-pole lowpass filter, and Fig 1c shows a bandpass filter. In Figs 1b and 1c, the resistive input impedance of the second filter stage acts as the parallel resistor for the first stage. You can repeat this arrangement many times. The bandpass filter in Fig 1c does have the disadvantage of a 3-dB loss in its passband. **EDN**

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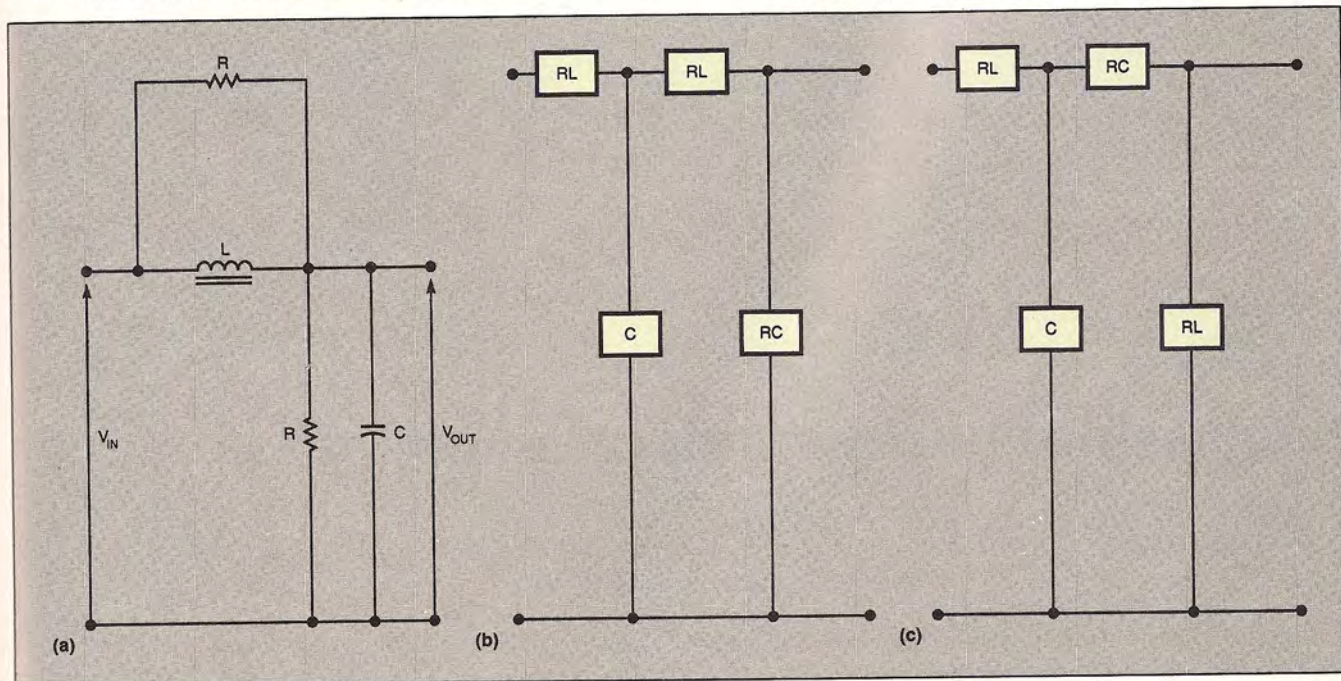
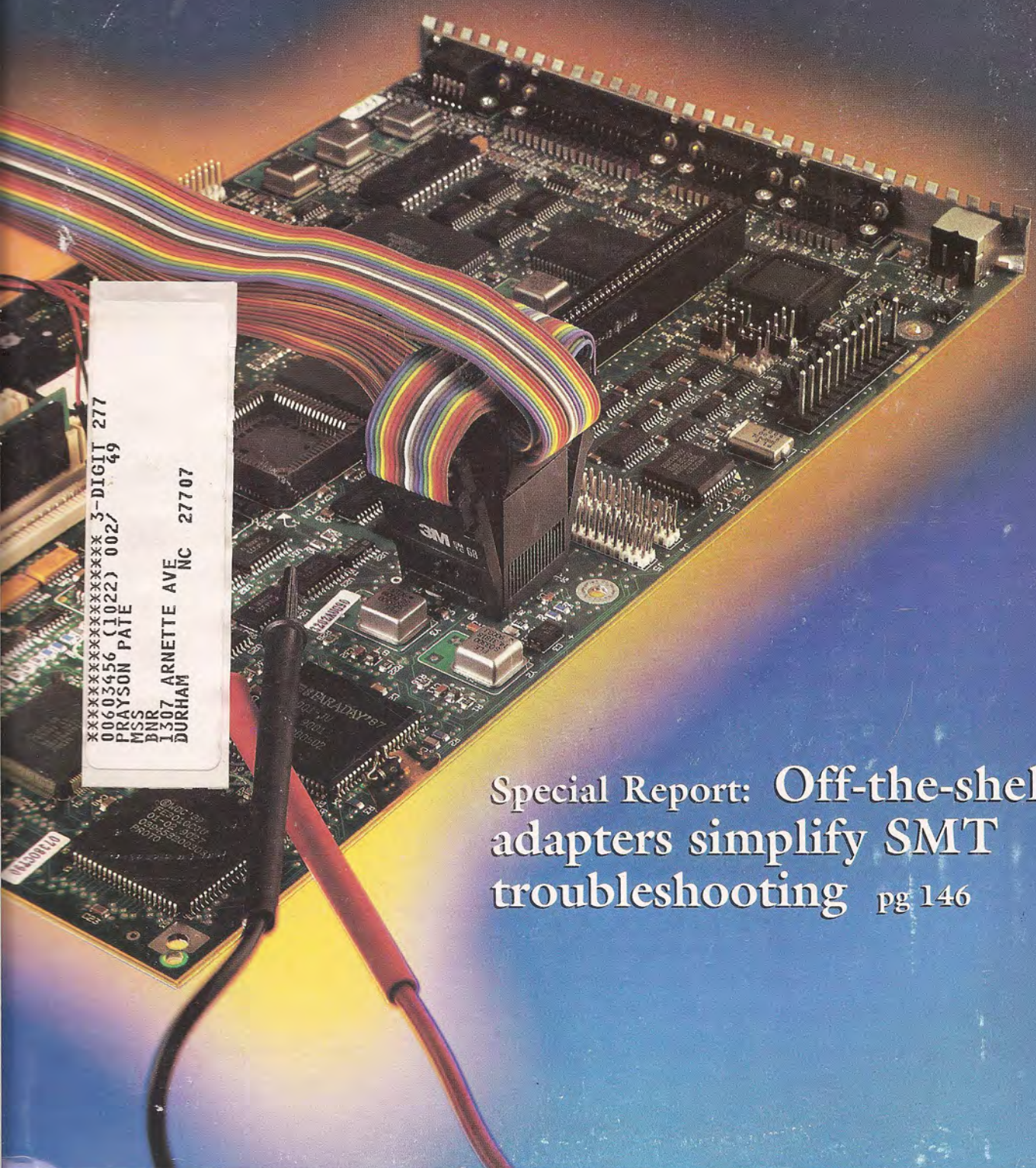


Fig 1—The simple circuit in a provides resistive termination at all frequencies. Combining and swapping the circuit's elements yields the 2-pole lowpass filter in b and the bandpass filter in c.

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DESIGN IDEAS

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FEEDBACK AND AMPLIFICATION

on the common pin. Also, parts cost drops from \$3.50 (1000) to \$1 (100) if you use a generic 74HC5043 triple dpst switch rather than a quad switch. Fig 1 shows my suggested redesign.

Lastly, Tian Jin Qin's "Inverters mimic interlocked switches" on pg 132 also has problems. First, the circuit won't always switch. If you use CMOS logic, the worst-case current through B_1 , C, R_3 , S, and D_{1B} available to a switch, assuming a $5V \pm 10\%$ supply, is 5.5 mA. For the circuit to work correctly, this current should be larger than the maximum inverter sink current, or at least 20 mA. Next, the circuit has an indeterminate state at power-on. Lastly, you could inadvertently turn on multiple outputs by pressing more than one button simultaneously. Fig 2 shows my suggested revision.

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Author corrects equations

The Design Idea I contributed, "Passive network is totally resistive" (EDN, August 2, 1990, pg 135), contains two errors. The equation for L should be

$$L = \frac{R}{\omega_0} = \frac{R}{2\pi F_0}$$

and the equation for C should be

$$C = \frac{1}{\omega_0 R} = \frac{1}{2\pi F_0 R}$$

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