

**SCC 990 Flexible Andon Board  
Structural Design Review & Load Testing  
Of  
Aluminum Frame & Connections**

**PREPARED FOR:**  
STATIC CONTROLS CORPORATION  
30460 Wixom Road  
Wixom, MI 48393

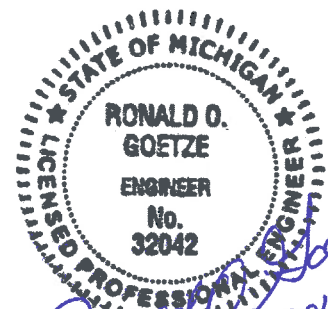
**PREPARED BY:**  
Ruby+Associates, Inc.  
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February 29, 2016

Ruby 16-042

Ronald O. Goetze, PE, SECB  
Senior Project Engineer

The logo for Ruby+Associates, featuring a stylized blue square icon followed by the text "ruby+associates" in a lowercase, sans-serif font.



*Ronald O. Goetze*  
Feb. 29, 2016



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Client: Static Controls Corporation  
 Project: Andon Board Design Review

Joint Mark	Bolt Size	Calculated Strength					Minimum Tested	Applied Force @ Connection	Minimum Safety Factors	
		Tension	Shear	Pullout	Slide	Lowest			Calculated	Min. Test
<b>A</b>	1/4	2850	1425	475	765	475	400	40	11.9	10.0
<b>B</b>	1/4	2850	1425	475	765	475	300	35	13.6	8.6
<b>C</b>	1/4	2850	1425	475	765	475	300	35	13.6	8.6
<b>D</b>	1/4	2850	1425	475	765	475	400	40	11.9	10.0
<b>E</b>	1/4	2850	1425	475	765	475	1100	40	11.9	27.5
<b>F</b>	1/4	2850	1425	475	765	475	300	35	13.6	8.6
<b>G</b>	1/4	2850	1425	475	765	475	300	35	13.6	8.6
<b>H</b>	1/4	2850	1425	475	765	475	1100	40	11.9	27.5
<b>J</b>	3/8	6975	3600	1150	730	730	1100	116	6.3	9.5
<b>K</b>	3/8	6975	3600	1150	730	730	1100	86	8.5	12.8
<b>L</b>	(2) - 3/8	13950	7200	2300	1460	1460	600	185	7.9	3.2

NOTES:

1. For a frame diagram showing joint marks, loads and connection forces, see Appendix A, page A-1.
2. See Table 2 for connection force calculations and allowable force on angles.
3. The minimum safety factor against failure for the bolts, connection angles and aluminum frame is 3.2 for the case of having all the load on the two center mounted safety lugs. Under normal operating conditions, the minimum safety factor is 6.3.

Table 2: Andon Board - Connection Design Forces/ Angle Strengths						
Joint Mark	Bolt Size	Connection Angle	Maximum Design Force		Calculated Allowable Force Applied to Angle	Minimum Calculated Safety Factor
			Components	Total		
A	1/4	L1.5x1.5x0.18	140/4+5=	40	890	22.3
B	1/4	L1.5x1.5x0.18	140/4=	35	890	25.4
C	1/4	L1.5x1.5x0.18	140/4=	35	890	25.4
D	1/4	L1.5x1.5x0.18	140/4+5=	40	890	22.3
E	1/4	L1.5x1.5x0.18	140/4+5=	40	890	22.3
F	1/4	L1.5x1.5x0.18	140/4=	35	890	25.4
G	1/4	L1.5x1.5x0.18	140/4=	35	890	25.4
H	1/4	L1.5x1.5x0.18	140/4+5=	40	890	22.3
J	3/8	L2x2x0.187	40+40+6+30=	116	1130	9.7
K	3/8	L2x2x0.187	40+40+6=	86	1130	13.1
L	(2) - 3/8	(2) L3x1.625x0.132	1/2 of Total Wgt	185	1400	7.6

## NOTES:

1. For a frame diagram showing joint marks, loads and connection forces, see Appendix A, page A-1.
2. See Table 1 for connection bolt allowable loads.
3. The minimum safety factor against failure for the bolts, connection angles and aluminum frame is 3.2 for the case of having all the load on the two center mounted safety lugs. Under normal operating conditions, the minimum safety factor is 6.3.

BOLT STRENGTHS : TENSION & SHEAR

3/8" - 16 BOLT

GRADE 5

$F_u = 120,000 \text{ PSI}$

TENSILE STRENGTH,  $T_u = F_u \cdot A_t$

TENSILE STRESS AREA =  $0.0775 \text{ in}^2$  \*

$T_u = 120,000 (0.0775) = \underline{9300 \text{ LBS.}}$

SHEAR STRENGTH,  $V_u = 0.6 F_u A_s$

AREA OF MINOR DIA.,  $A_s = 0.0678$  \*

$V_u = 0.6 (120,000) (0.0678) = \underline{4880 \text{ LBS.}}$

1/4" - 20 BOLT

GRADE 5

$F_u = 120,000 \text{ PSI}$

$T_u = F_u \cdot A_t$

$A_t = 0.0318 \text{ in}^2$  \*

$T_u = 120,000 (0.0318) = \underline{3800 \text{ LBS.}}$

SHEAR STRENGTH,  $V_u = 0.6 F_u A_s$

AREA OF MINOR DIA.,  $A_s = 0.0269 \text{ in}^2$  \*

$V_u = 0.6 (120,000) (0.0269) = \underline{1900 \text{ LBS.}}$

APPLY STRENGTH RESISTANCE FACTORS

USE  $\phi_T = \phi_S = 0.75$

3/8" BOLTS  $\phi T_u = 0.75 \times 9300 = \underline{6975 \text{ LBS}}$

$\phi V_u = 0.75 \times 4880 = \underline{3660 \text{ LBS}}$

1/4" BOLTS  $\phi T_u = 0.75 \times 3800 = \underline{2850 \text{ LBS}}$

$\phi V_u = 0.75 \times 1900 = \underline{1425 \text{ LBS}}$

\* PER MACHINEERY'S HANDBOOK 23, Table 3a.



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PROJECT

STATIC CONTROL CORP  
ANDON BOARD DESIGN REVIEW

TITLE

ALUMINUM FRAME &  
CONNECTIONS

BY:

RG

SHEET:

1

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BOLT STRENGTHS:

(SLIDE IN T-SLOT)

APPROXIMATE CLAMPING FORCE @ DESIGN BOLT INSTALLATION TORQUE  
3/8-16 TORQUE = 10 ft-lbs  
= 120 IN-LBS.

$$T = KDF$$

- K = 0.15 LUBRICATED
- K = 0.18 ZINC PLATED AND DRY
- K = 0.20 PAINT & DRY
- D = DIAMETER OF BOLT
- F = CLAMP FORCE

$$F = \frac{T}{KD}$$

WHEN K = 0.20,  $F = \frac{120}{0.20(375)} = 1600 \text{ LBS.}$

COEFFICIENT OF FRICTION (SLIP RESISTANCE)

BETWEEN STEEL & ALUMINUM (DRY, UNLUBRICATED)

$$\mu = 0.61 \quad [ \text{APPLIED INO. TECH.} ]$$

RESISTING SLIP FORCE =  $P_n = \mu F$

$$P_n = 0.61(1600) = 970 \text{ LBS.}$$
$$\phi P_n = 0.75(970) = \underline{730 \text{ LBS}}$$

ACTUAL BOLT HEAD WILL DEFORM ALUMINUM AT CONTACT SURFACE INCREASING THE SLIP RESISTANCE.



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BOLT STRENGTHS:

(SLIP IN T-SWT)

1/4-20 BOLTS.

INSTALL TORQUE = 7 FT-LBS = 84 IN-LBS.

FOR  $K = 0.20$  (PLAIN & DRY THREADS)

$$F \approx \frac{T}{K D} = \frac{84}{0.20 (0.25)} = 1680 \text{ LBS.}$$

RESISTING SLIP FORCE,  $P_n = \mu F$

$$P_n = 0.61 (1680) = 1020 \text{ LBS}$$

$$\phi P_n = 0.75 (1020) = \underline{765 \text{ LBS}}$$

ACTUAL BOLT HEAD WILL DEFORM ALUMINUM AT CONTACT SURFACE INCREASING THE SLIDING RESISTANCE.



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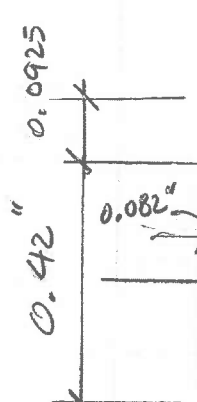
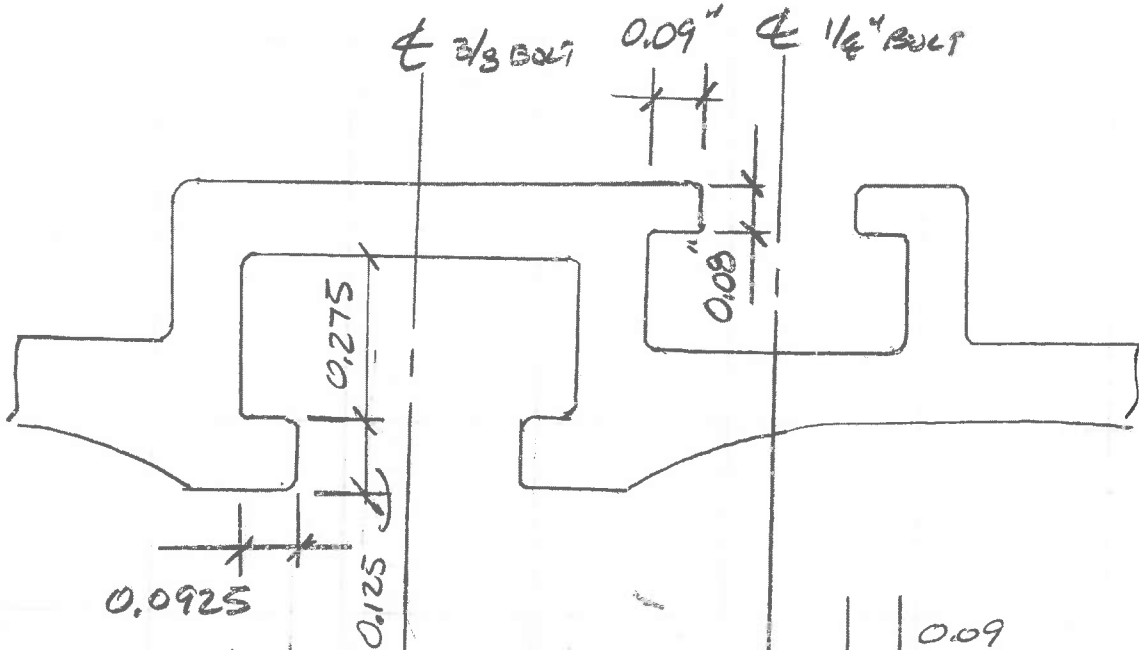
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BOLT STRENGTHS:

PULL-OUT STRENGTH OF ALUMINUM TRACK

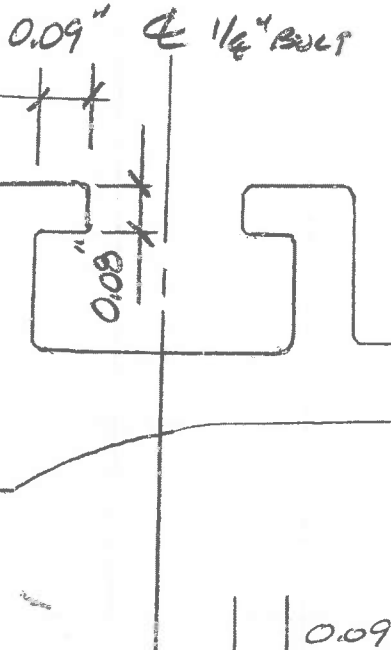
3/8" BOLT



SHEAR LENGTH  
= 13mm  
= 0.512 in

SHADED AREA  
(2)(0.37)(0.092) = 0.061 in<sup>2</sup>

3/8" BOLT



SHEAR LENGTH  
= 11.3mm  
= 0.445 in

SHADED AREA  
(2)(0.30)(0.089) = 0.050 in<sup>2</sup>

1/4" BOLT

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## BOLT STRENGTHS (3/8" PULLOUT)

### SHEAR STRESS IN ALUMINUM

ASSUME BOLT HEAD PULLS THROUGH ALONG  
OUTER EDGE OF BOLT HEAD

$$\text{PERIMETER LENGTH} = 0.512''$$

$$\text{MATERIAL THICKNESS} = 0.125''$$

$$\text{SHEAR AREA, } A_v = (2)(0.512)(0.125)$$

$$A_v = 0.128 \text{ in}^2$$

$$\sigma_s = \frac{P}{A_v} = \frac{P}{0.128} = 7.81 P \quad \text{PSI}$$

### FLEXURAL STRESS IN ALUMINUM

ASSUME LOAD "P" IS APPLIED AT MIDSPOINT OF  
CANTILEVERS. FORCE ON EACH CANTILEVER =  $\frac{P}{2}$

$$M_{\text{MAX}} = \left(\frac{P}{2}\right) \frac{L}{2} = \frac{P}{2} \left(\frac{0.0925}{2}\right)$$

$$M_{\text{MAX}} = \frac{P}{43.2}$$

$$\text{EFFECTIVE BENDING LENGTH} = 0.42'' + 2(0.0925) = 0.60$$

$$I = \frac{bh^3}{12} = \frac{0.60 (0.125)^3}{12} = \frac{1}{10240} \text{ in}^4$$

$$\sigma_b = \frac{M_c}{I} = \frac{(P/43.2)(0.125/2)}{(1/10240)}$$

$$\sigma_b = 14.8 P$$



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# BOLT STRENGTHS (2/3 PULL OUT)

COMBINED STRESS, MOHR CIRCLE

$$\sigma_{max} = \frac{\sigma_x}{2} + \sqrt{\left(\frac{\sigma_x}{2}\right)^2 + \tau_{xy}^2}$$

$$\sigma_{max} = \left(\frac{14.8P}{2}\right) + \sqrt{\left(\frac{14.8P}{2}\right)^2 + (7.91P)^2}$$

$$\sigma_{max} = 7.4P + P\sqrt{\left(\frac{14.8}{2}\right)^2 + (7.91)^2}$$

$$\sigma_{max} = 7.4 + 10.8P$$

$$\sigma_{max} = 18.2P$$

ALUMINUM,  $F_u = 28,000$  PSI

$$P_u = \frac{F_u}{18.2} = \frac{28,000}{18.2} = 1538 \text{ LBS.}$$

$$\phi P_u = 0.75(1538) = \underline{1150 \text{ LBS}}$$

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# BOLT STRENGTHS (1/4" PULLOUT)

## SHEAR STRESS IN ALUMINUM

$$\text{PERIMETER LENGTH} = 0.445''$$

$$\text{MATERIAL THICKNESS} = 0.03''$$

$$\text{SHEAR AREA, } A_v = (2)(0.445)(0.03) = 0.071 \text{ in}^2$$

$$\tau_{xy} = \sigma_s = \frac{P}{A_v} = \frac{P}{0.071} = 14.0 P$$

## FLEXURAL STRESS IN ALUMINUM

ASSUME LOAD "P" IS APPLIED AT MIDSPAN OF CANTILEVERS, FORCE IN EACH CANTILEVER =  $\frac{P}{2}$

$$M_{\text{MAX}} = \left(\frac{P}{2}\right) \frac{L}{2} = \left(\frac{P}{2}\right) \left(\frac{0.09}{2}\right) = \frac{P}{44.4}$$

$$\text{EFFECTIVE BENDING LENGTH} = 0.35 + (2)(0.09) = 0.53$$

$$I = \frac{bh^3}{12} = \frac{0.53(0.09)^3}{12} = \frac{1}{44200}$$

$$\sigma_x = \sigma_b = \frac{M_c}{I} = \frac{\left(\frac{P}{44.4}\right) \left(\frac{0.09}{2}\right)}{\frac{1}{44200}} = 39.8 P$$

## COMBINED STRESSES

$$\sigma_{\text{MAX}} = \frac{\sigma_x}{2} + \sqrt{\left(\frac{\sigma_x}{2}\right)^2 + (\tau_{xy})^2} = \left(\frac{39.8 P}{2}\right) + P \sqrt{\left(\frac{39.8}{2}\right)^2 + (14.0)^2}$$

$$\sigma_{\text{MAX}} = 19.9 P + 24.3 P = 44.2 P$$

$$P_u = \frac{F_u}{44.2} = \frac{28,000}{44.2} = 633 \text{ LBS.}$$

$$\phi P_u = 0.75(633) = \underline{475 \text{ LBS}}$$

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## EXTRUDED ALUMINUM

MATERIAL 6063-T6

$$F_{tu} = 30 \text{ ksi}$$

$$F_{ty} = 25 \text{ ksi}$$

SECTION PROPERTIES

$$F_{cy} = 25 \text{ ksi}$$

$$F_{su} = 19 \text{ ksi}$$

$$E = 10,100 \text{ ksi}$$

$$A = 1.30 \text{ in}^2$$

$$I_{x-x} = 0.078 \text{ in}^4$$

$$I_{y-y} = 4.036 \text{ in}^4$$

$$C_b = -0.327''$$

$$C_L = -2.691''$$

$$C_t = 0.800''$$

$$C_r = +2.800''$$

$$S_x)_b = \frac{I_{x-x}}{C_b} = \frac{0.078}{0.327} = 0.238 \text{ in}^3$$

$$S_x)_t = \frac{I_{x-x}}{C_t} = \frac{0.078}{0.80} = 0.097 \text{ in}^3 \quad \leftarrow \text{CONTROLS.}$$

BENDING DESIGN STRESS  $\phi_y F_{ty}$  (GROSS SECTION)

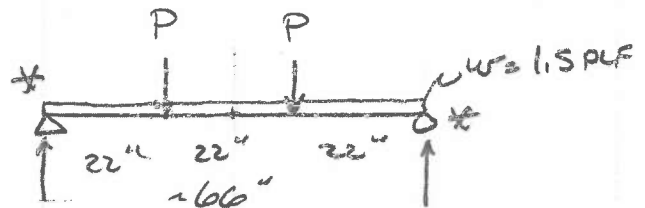
$$\phi_y = 0.95$$

$$\phi M_n = 0.95 (25) (0.097) = 2.3 \text{ k-in.} \\ = 2300 \text{ LB-IN.}$$

CHECK 65" FRAME w/ 70" LOADS

$$P = \frac{140}{2} = 70 \text{ \#}$$

$$w = 1.5 \text{ PLF}$$



$$M_{max} \leq 22(P) + w \left( \frac{22^2}{2 \cdot 12} \right)$$

$$M_{max} \leq 22(70) + 1.5 \left( \frac{22^2}{2 \cdot 12} \right) = 1570 \text{ LB-IN} < 2300 \text{ OK.}$$

\* ACTUAL MAXIMUM IS LESS DUE TO "FIXED" MOMENT AT CORNERS.

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EXTRUDED ALUMINUM

$$\begin{aligned} \text{SHEAR AREA} &\approx (2) 1'' \times 0.12 + (4) 0.52 \times 0.12 \\ &= 0.73 \text{ in}^2 \end{aligned}$$

$$\phi V_n = 0.80 (F_u) A_v = 0.80 (19) (0.73)$$

$$\phi V_n = \underline{11.1 \text{ kips}}$$

OK. BY  
INSPECTION.

TENSILE STRENGTH

$$\phi T_n = 0.95 (F_{ty}) A_T$$

$$= 0.95 (25) (1.30) = 30.9 \text{ kips} \quad \text{OK.}$$

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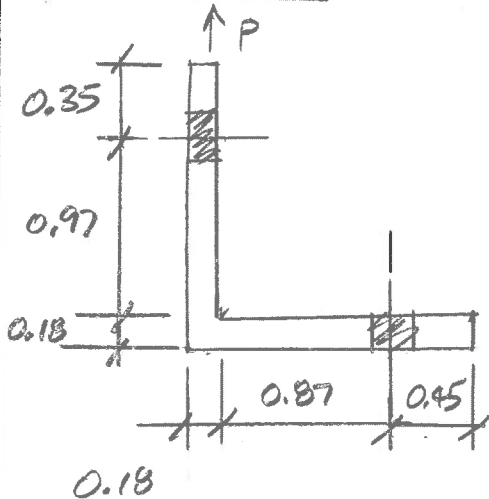
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CONNECTION ANGLES.

CORNER: L 1/2 x 1/2 x 0.18" x 0'-5 1/8



LIMITED STATE: FLEXURAL STRESS  
 MAXIMUM MOMENT = 0.97 x P

$$S = 5.125 (0.18)^2 / 6 = 0.028 \text{ in}^3$$

$$\phi M_n = 1.3 \phi_y (S) (F_{ty})$$

$$= 1.3 (0.95) (0.028) (25)$$

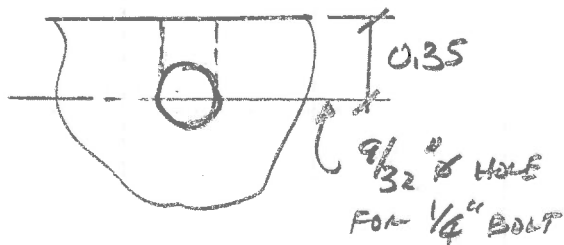
$$\phi M_n = 0.36 \text{ K-in} = 860 \text{ LB-in}$$

$$P_{\text{max}} = \frac{\phi M_n}{e} = \frac{860}{0.97} = 890 \text{ \#}$$

2 CONTROLS

LIMITED STATE TENSION  $\Rightarrow$  OK. BY INSPECTION

TEAR OUT (SHEAR ROW)



$$l_v \approx 2 (0.35) = 0.70 \text{ in}$$

$$A_v = t \cdot l_v = 0.18 (0.70) = 0.126 \text{ in}^2$$

$$\phi V_n = 0.80 (F_{34}) (A_v)$$

$$= 0.80 (19) (0.126)$$

$$= 1.9 \text{ KIPS} = 1900 \text{ LBS.}$$

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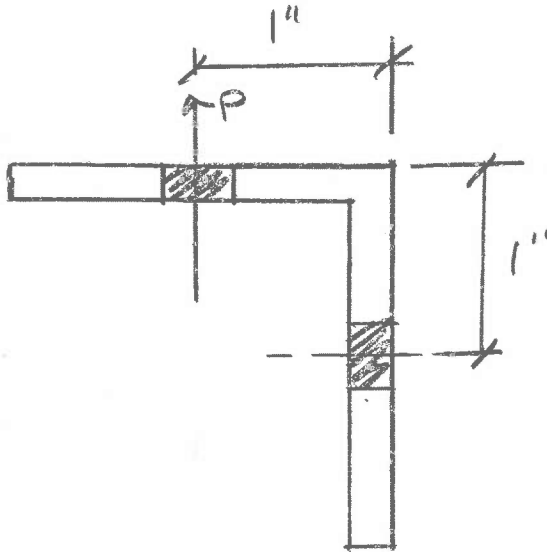
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SIDE ANGLES.

L 2x2x0.187"

ASTM A36



LIMITED STATE:  
LEG BENDING.

$$\text{MAX } M. \leq 1" \times P$$

ASSUME 4" EFFECTIVE  
ANGLE LENGTH

$$Z = bt^2/4$$

$$Z = 4(0.187)^2/4$$

$$Z = 0.035 \text{ IN}^3$$

$$\phi M_n = 0.90 F_y Z$$

$$= 0.90 (36)(0.035)$$

$$= 1.13 \text{ K-IN}$$

$$\phi M_n = 1130 \text{ LB-IN}$$

TEAR OUT  $\Rightarrow$  OK. BY INSPECTION.  $\therefore P_{\text{allow}} = \frac{1130}{1"} = 1130 \#$

LIMIT STATE: SINGLE ANGLE BENDING



$$M = \frac{PL}{4} = \frac{P(24)}{4} = 0.5 P \quad \text{K-FT}$$

FOR  $P = 400 \text{ LBS}$

$$M_{\text{MAX}} = 0.4(0.5) = 0.2 \text{ K-FT}$$

$$M_u = 112 \times 0.2 = 0.24 \text{ K-FT}$$

FROM SINGLE ANGLE CALCULATION (P. 12 to 13)

$$\text{UNITY} = 0.525 \quad \therefore \text{ALLOW. LOAD} = \frac{400}{0.63} = 635 \# > 370 \#$$

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## Single-Angle Member Design

(Load and Resistance Factor Design Specification for Single-Angle Members)

Beam Properties: Units: ksi := 1000 ·  $\frac{\text{lbf}}{\text{in}^2}$  kip := 1000 · lbf

L2x2x3/16  $b := 2 \cdot \text{in}$   $t := 0.1875 \cdot \text{in}$  Material Properties:  $E := 29000 \cdot \text{ksi}$   $F_y := 36 \cdot \text{ksi}$

$A_g := 0.72 \cdot \text{in}^2$   $S_c := 0.188 \cdot \text{in}^3$   $r := 0.389$  Strength Reduction Factors:  $\phi_b := 0.90$   $\phi_c := 0.90$

Span Information:

Unbraced Length:  $l_u := 24 \cdot \text{in}$   $K := 2$   $P := 0.0 \cdot \text{kip}$   $P_r := 1.6 \cdot P = 0 \cdot \text{kip}$

$M_{\max}$  = absolute value of maximum moment in the unbraced beam segment

$M_A$  = absolute value of moment at quarter point of the unbraced segment

$M_B$  = absolute value of moment at the centerline of the unbraced segment

$M_C$  = absolute value of the moment at the three-quarter point of the unbraced segment

$M_{\max} := 1.2 \cdot 0.2 \cdot \text{kip} \cdot \text{ft}$   $M_A := 1.2 \cdot 0.1 \cdot \text{kip} \cdot \text{ft}$   $M_B := 1.2 \cdot 0.2 \cdot \text{kip} \cdot \text{ft}$   $M_C := 1.2 \cdot 0.20 \cdot \text{kip} \cdot \text{ft}$

COMPRESSION:

Reduction factor for local buckling (Q):

$$Q := \begin{cases} 1.0 & \text{if } \frac{b}{t} \leq \sqrt{\frac{E}{F_y}} \\ \left( 1.34 - 0.76 \cdot \frac{b}{t} \cdot \sqrt{\frac{F_y}{E}} \right) & \text{if } 0.446 \cdot \sqrt{\frac{E}{F_y}} < \frac{b}{t} \leq 0.910 \cdot \frac{b}{t} \cdot \sqrt{\frac{E}{F_y}} \\ \left[ 0.534 \cdot \frac{E}{F_y \cdot \left( \frac{b}{t} \right)^2} \right] & \text{otherwise} \end{cases} \quad Q = 1$$

Critical compression stress,  $F_{cr}$ :

$$\lambda_c := \frac{K \cdot l_u}{r \cdot \pi} \cdot \sqrt{\frac{F_y}{E}} \quad \lambda_c = 1.384 \cdot \text{in}$$

$$F_{cr} := \begin{cases} \left[ Q \cdot \left[ 0.658 + Q \cdot \left( \frac{\lambda_c}{\text{in}} \right)^2 \right] \right] \cdot F_y & \text{if } \sqrt{Q} \leq 1.5 \\ \left[ \frac{0.877}{\left( \frac{\lambda_c}{\text{in}} \right)^2} \right] \cdot F_y & \text{otherwise} \end{cases}$$

$$F_{cr} = 16.151 \cdot \text{ksi}$$

$$\phi P_n := \phi_c \cdot F_{cr} \cdot A_g$$

$$\phi P_n = 10.466 \cdot \text{kip}$$



**FLEXURE:**

Limit state of yielding when the tip of an angle leg is in compression:

$$M_{n1} := \begin{cases} (1.5 \cdot F_y \cdot S_c) & \text{if } \frac{b}{t} \leq 0.54 \cdot \sqrt{\frac{E}{F_y}} \\ \left[ F_y \cdot S_c \cdot \left[ 1.5 - 0.93 \cdot \left[ \frac{\frac{b}{t} - 1}{\left( 0.54 \cdot \sqrt{\frac{E}{F_y}} \right)} \right] - 1 \right] \right] & \text{if } 0.54 \cdot \sqrt{\frac{E}{F_y}} < \frac{b}{t} \leq 0.91 \cdot \sqrt{\frac{E}{F_y}} \\ (1.34 \cdot Q \cdot F_y \cdot S_c) & \text{otherwise} \end{cases}$$

$$M_{n1} = 0.846 \cdot \text{kip} \cdot \text{ft}$$

$$\phi M_{n1} := \phi_b \cdot M_{n1} = 0.761 \cdot \text{kip} \cdot \text{ft}$$

Limit state of yielding when the tip of an angle leg is in tension:

$$M_y := 0.8 \cdot S_c \cdot F_y = 0.451 \cdot \text{kip} \cdot \text{ft}$$

$$M_n := 1.5 \cdot M_y = 0.677 \cdot \text{kip} \cdot \text{ft}$$

$$CB := \frac{12.5 \cdot M_{\max}}{2.5 \cdot M_{\max} + 3 \cdot M_A + 4 \cdot M_B + 3 \cdot M_C}$$

$$C_b := \begin{cases} CB & \text{if } CB < 1.5 \\ 1.5 & \end{cases}$$

$$C_b = 1.5$$

With maximum compression at the angle-leg tips:

$$M_{ob} := \frac{0.66 \cdot E \cdot b^4 \cdot t \cdot C_b}{l_u^2} \cdot \left[ \sqrt{1 + 0.78 \cdot \left( \frac{l_u \cdot t}{b^2} \right)^2} - 1 \right]$$

$$M_{ob} = 5.105 \cdot \text{kip} \cdot \text{ft}$$

For the limit state of lateral-torsional

$$M_{n2} := \begin{cases} \left[ \left( 0.92 - 0.17 \cdot \frac{M_{ob}}{M_y} \right) \cdot M_{ob} \right] & \text{if } M_{ob} \leq M_y \\ \left( 1.92 - 1.17 \cdot \sqrt{\frac{M_y}{M_{ob}}} \right) \cdot M_y & \text{otherwise} \end{cases}$$

$$M_{n2} := \begin{cases} M_{n2} & \text{if } M_{n2} \leq 1.5 \cdot M_y \\ (1.5 \cdot M_y) & \text{otherwise} \end{cases}$$

$$M_{n2} = 0.677 \cdot \text{kip} \cdot \text{ft}$$

$$\phi M_{n2} := \phi_b \cdot M_{n2} = 0.609 \cdot \text{kip} \cdot \text{ft}$$

With maximum tension at the angle-leg tips:

$$M_{ob} := \frac{0.66 \cdot E \cdot b^4 \cdot t \cdot C_b}{l_u^2} \cdot \left[ \sqrt{1 + 0.78 \cdot \left( \frac{l_u \cdot t}{b^2} \right)^2} + 1 \right]$$

$$M_{ob} = 30.027 \cdot \text{kip} \cdot \text{ft}$$

For limit state of lateral-torsional buckling:

$$M_{n3} := \begin{cases} \left[ \left( 0.92 - 0.17 \cdot \frac{M_{ob}}{M_y} \right) \cdot M_{ob} \right] & \text{if } M_{ob} \leq M_y \\ \left[ \left( 1.92 - 1.17 \cdot \sqrt{\frac{M_y}{M_{ob}}} \right) \cdot M_y \right] & \text{otherwise} \end{cases}$$

$$M_{n3} := \begin{cases} M_{n3} & \text{if } M_{n3} \leq 1.5 \cdot M_y \\ (1.5 \cdot M_y) & \text{otherwise} \end{cases}$$

$$M_{n3} = 0.677 \cdot \text{kip} \cdot \text{ft}$$

$$\phi M_{n3} := \phi_b \cdot M_{n3} = 0.609 \cdot \text{kip} \cdot \text{ft}$$

$$\phi M_n := \min(\phi M_{n1}, \phi M_{n2}, \phi M_{n3})$$

$$\phi M_n = 0.609 \cdot \text{kip} \cdot \text{ft}$$

INTERACTION (UNITY) EQUATION:

$$P_c := \phi P_n \quad M_{rx} := 1.6 \cdot M_{\max} \quad M_{ry} := 0 \cdot \text{kip} \cdot \text{ft}$$

$$M_{cx} := \phi M_n \quad M_{cy} := \phi M_n$$

$$U := \begin{cases} \left[ \frac{P_r}{P_c} + \frac{8}{9} \cdot \left( \frac{M_{rx}}{M_{cx}} + \frac{M_{ry}}{M_{cy}} \right) \right] & \text{if } \frac{P_r}{P_c} \geq 0.2 \\ \frac{P_r}{2 \cdot P_c} + \left( \frac{M_{rx}}{M_{cx}} + \frac{M_{ry}}{M_{cy}} \right) & \text{otherwise} \end{cases}$$

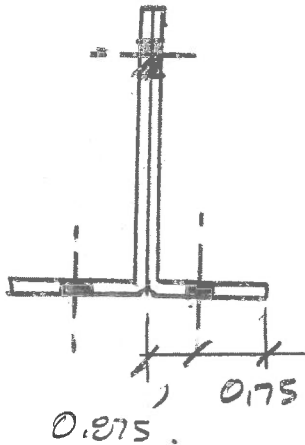
$$U = 0.63$$

$$\text{Design\_Check} := \begin{cases} \text{"OK"} & \text{if } U \leq 1 \\ \text{"No Good"} & \text{if } U > 1 \end{cases}$$

Design\_Check = "OK"

SAFETY LUG

(2) L 3 x 1 5/8 x 0.135" x 3 1/2" LG.



LIMIT STATE: FLEXURE (SHORT LEG)

$$Z = 3.5 (0.135)^2 / 4 = 0.016 \text{ in}^3$$

$$\phi M_n = 0.90 (F_y) Z = 0.90 (36) (0.016)$$

$$\phi M_n = 0.518 \text{ k-in / LEG} \times 2 = 1.04 \text{ k-in}$$

$$M = (0.975 - 0.135) P = 0.74 P$$

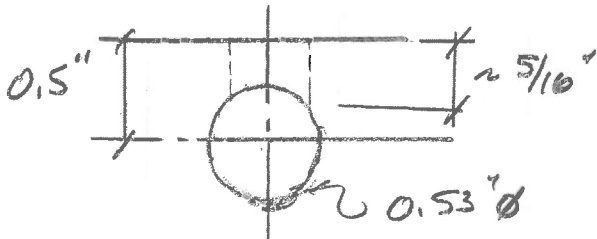
$$P_{allow} = \frac{1.04 \times 1000}{0.74} = 1400 \text{ LBS.}$$

↑ CONTROLS.

$$\phi V_n = 0.90 (0.6 (F_y) A_w) = 0.90 (0.6) (36) (9.135) (3.5) (2) = 18.3 \text{ kips.}$$

OK.

TEAR OUT @ TOP HOLE:



$$L_v = 0.3125$$

$$L_u = 2(0.3125) = 0.625$$

$$A_w = 2(0.625 \times 0.135) = 0.17 \text{ in}^2$$

$$\phi V_n = 0.90 (0.6) (36) (0.17) = 3.3 \text{ kips} = \underline{\underline{3300 \text{ LBS}}}$$

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PROJECT

STATIC CONTROL CORP  
ANDON BOARD DESIGN REVIEW

TITLE

ALUMINUM FRAME &  
CONNECTIONS

BY:

RG

SHEET:

15

CHKD:

RA

PROJECT NO:

16-042

DATE:

02/29/16

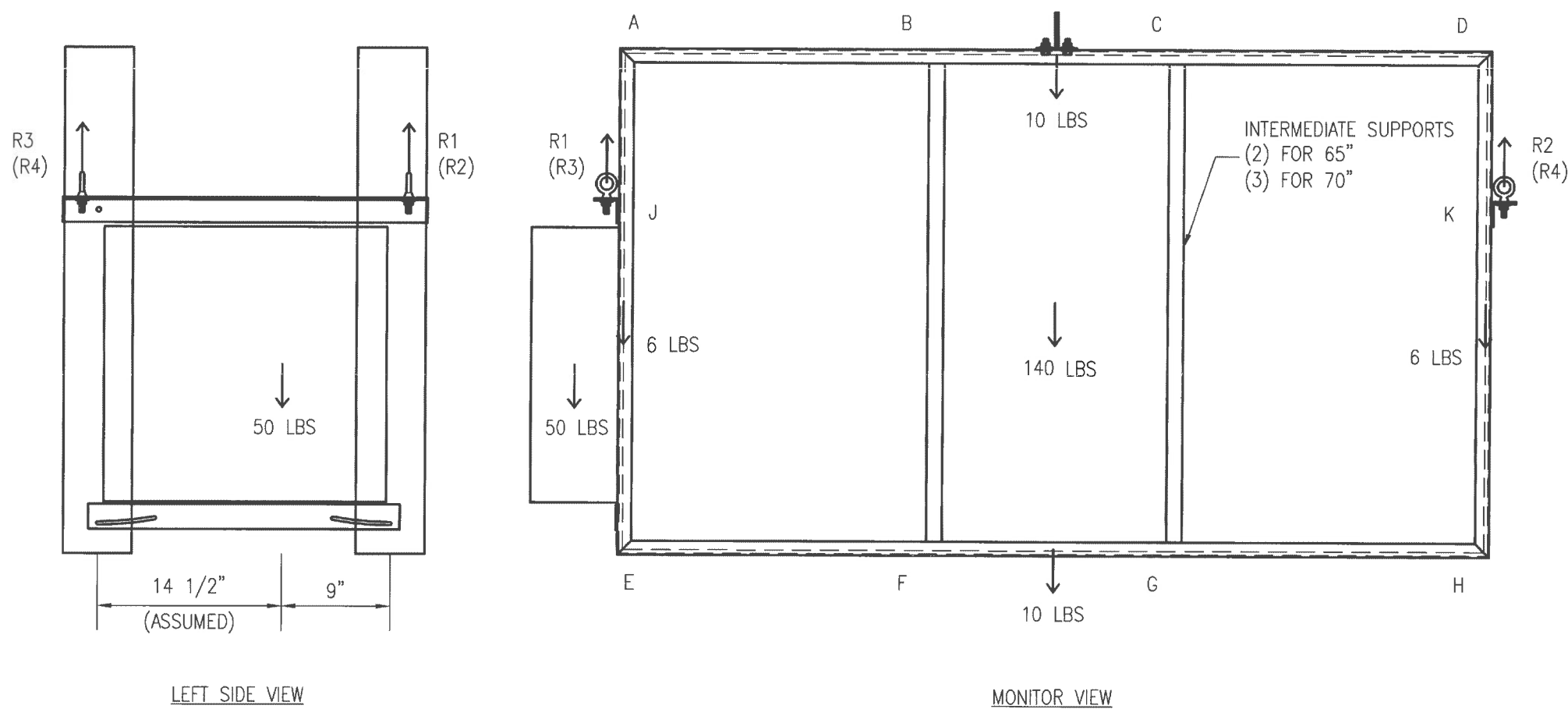
PAGE:

17



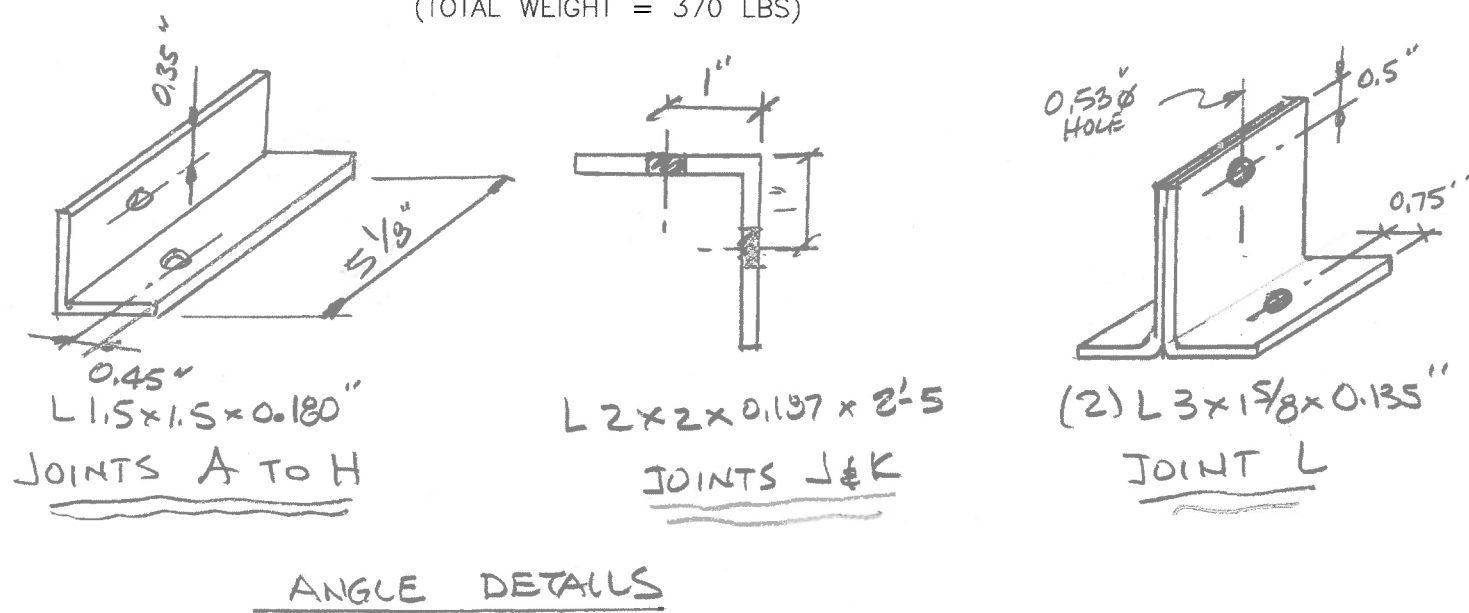
# Appendix A

## (Frame Loads & Properties)



**65"/70" DS LCD MONITOR, W/ CONTROL BOX (+MUSIC)**

(TOTAL WEIGHT = 370 LBS)



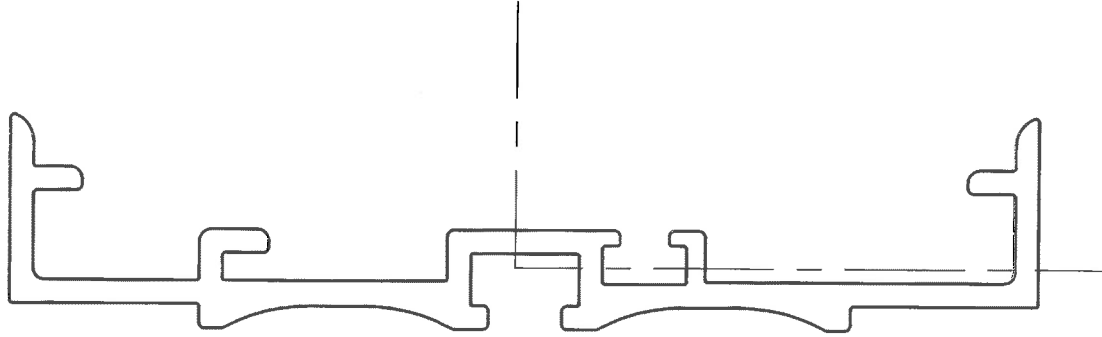
NOTES:

1. CONSERVATIVELY APPLY HEAVIER 370 POUND LOAD OF 70" DISPLAY TO 65" FRAME WHICH HAS ONE LESS INTERMEDIATE SUPPORT THAT DIRECTLY RESISTS THE LCD DISPLAY WEIGHT.
2. LOADS/FORCES SHOWN OCCUR ON EACH FRAME EXCEPT FOR THE 50 POUND CONTROLLER WHICH IS SHARED (ASSUMED 60%/40% SPLIT) BETWEEN THE TWO FRAMES.

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PROJECT: **STATIC CONTROLS CORPORATION ANDON BOARD CONNECTION REVIEW**  
 TITLE: **65"/70" DS LCD MONITOR FRAMES LOADS/FORCES ON FRAME CONNECTIONS**

DESIGN BY: **RG**  
 DRN BY: **RG**  
 DATE: **02/16/16**  
 PROJECT NO.: **16-042**  
 SHEET NO.: **A-1**  
 REVISION



----- REGIONS -----

Area: 1.3002 sq in  
 Perimeter: 19.1976 in  
 Bounding box: X: -2.6915 -- 2.7991 in  
 Y: -0.3266 -- 0.8005 in  
 Centroid: X: 0.0000 in  
 Y: 0.0000 in  
 Moments of inertia: X: 0.0777 sq in sq in  
 Y: 4.0364 sq in sq in  
 Product of inertia: XY: -0.0061 sq in sq in  
 Radii of gyration: X: 0.2444 in  
 Y: 1.7620 in  
 Principol moments (sq in sq in) and X-Y directions about centroid:  
 I: 0.0777 along [1.0000 -0.0015]  
 J: 4.0364 along [0.0015 1.0000]

WEIGHT  
 $A \times 1.13 \text{ LB} = 1.53 \text{ PCF}$   
 $\frac{1.3}{1.13}$   
 F1

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PROJECT

**STATIC CONTROLS CORP.  
 ANDON BOARD REVIEW**

TITLE

**ALUM. FRAME PROPERTIES**

DRN BY:

**SCC**

DATE:

**2/16/16**

DESIGN BY:

**SCC**

PROJECT NO.

**16-042**

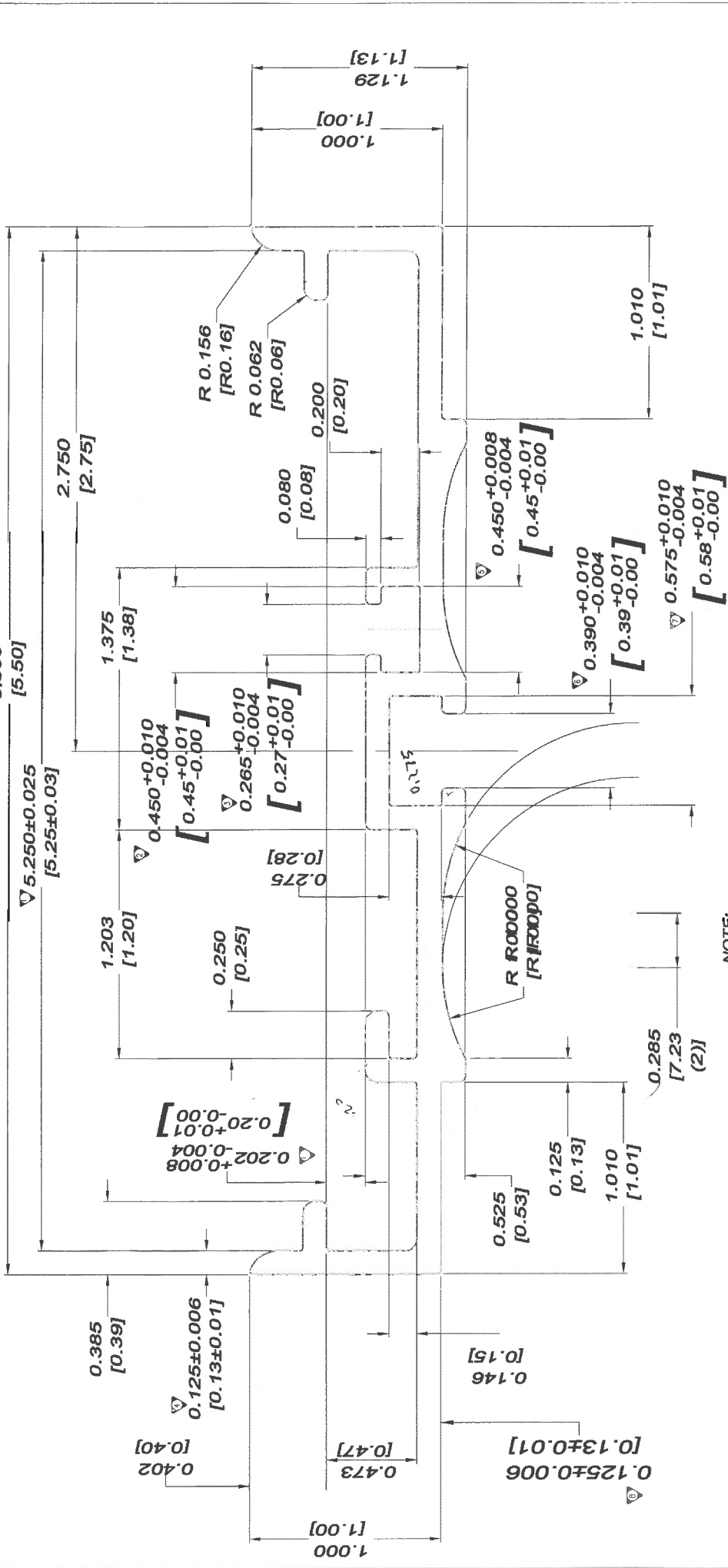
SHEET NO.

**A-2**

REVISION

ALUMINUM ASSOCIATION STANDARD TOLERANCES WILL APPLY UNLESS OTHERWISE SPECIFIED  
 DRAW LINES OR STRUCTURAL STREAKS MAY OCCUR WERE INDICATED

LENGTH OF BILLET	PRESS NO.	BACKER PLATE	BOULDER FEEDER	NO. CAV.	1	DIA. POCKET	276.61 X 139.70
	1650	7-29017 X 68.90	15-22				19.05
	5.500	7-29017 X 50.80					



NOTE:  
 1. ALL DIMENSIONS IN "INCHES"  
 METRIC "mm"  
 2. NO EXPOSED SURFACES

DAICOR Aluminum Ltd.		155 BINA STREET CHATHAM, ONT. N7M-5J5 Web Site: www.daicor.com	
STATIC CONTROLS			
CUSTOMER	5.50" 990 - SIGN FRAME	DIE TYPE	SOLID
CUSTOMER'S DWG. NO.	6063-T6	SCALE	2:1
MATERIAL	IAN COLQUHOUN	DATE	11-13-2014
DRAWN	CHD.	DWG. NO.	7-29017
DATE	19.235 (488.564)	FACTOR 12 (213)	
REVISION	8.429	ANOD.FERM.	29
LETTER	1.306	LBS/FT	
AREA SQ. IN.	8.429	KG/M	
AREA SQ. CM			



RUNOUT PLANE

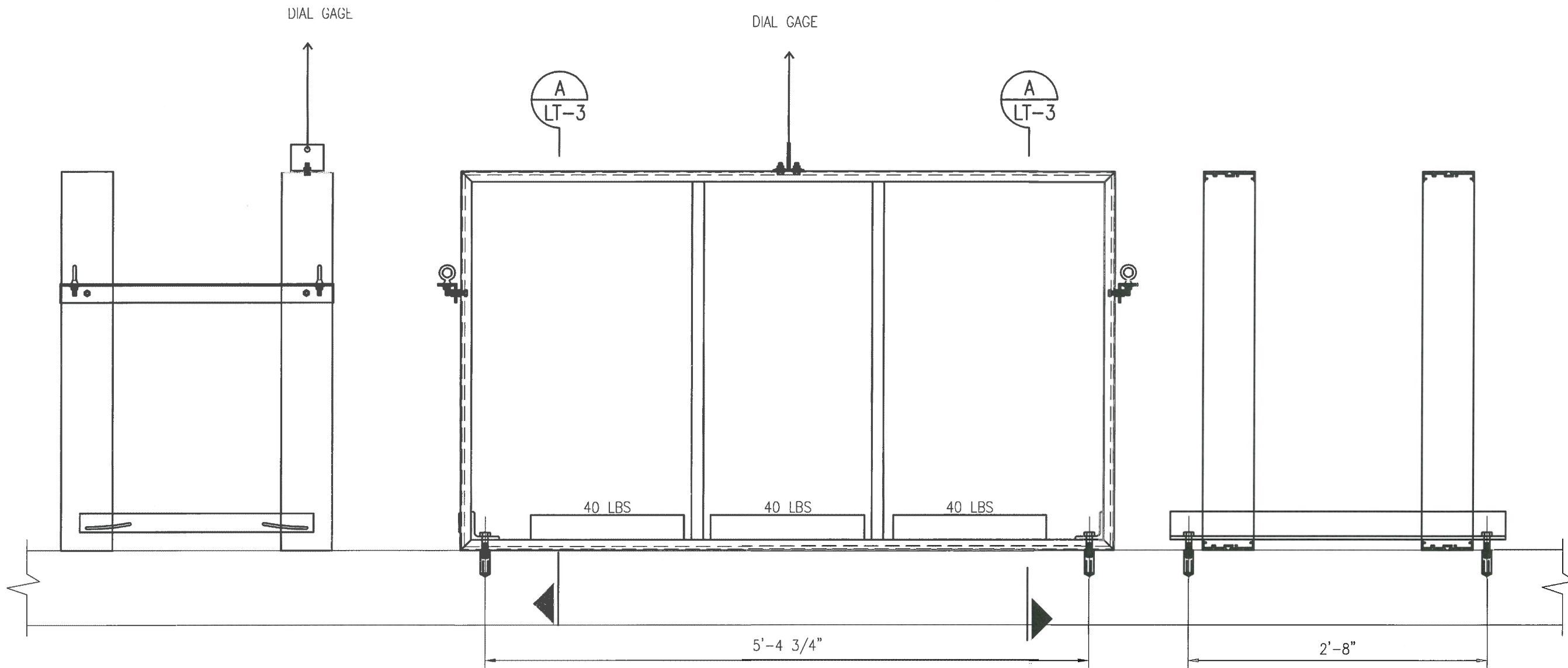
RUST  
 16.042  
 A-3



# Appendix B

## (Load Tests)





HOLD DOWN SUPPORT:  
 L3 x 3 x 3/8 or HSS x 3'-0" LONG  
 + (2) 5/8" DIA. HILTI HDI DROP-IN ANCHORS  
 (INSTALLED PER MANUFACTURER'S INSTRUCTIONS)  
 + (2) 5/8" DIA. X 2 1/4 GRADE 5 BOLTS

SECTION A  
 1"=1'-0" LT-1

## 65"/70" DS LCD MONITOR, TEST SETUP 1

SAFETY CABLE LUG/CENTER STRUT CONNECTIONS

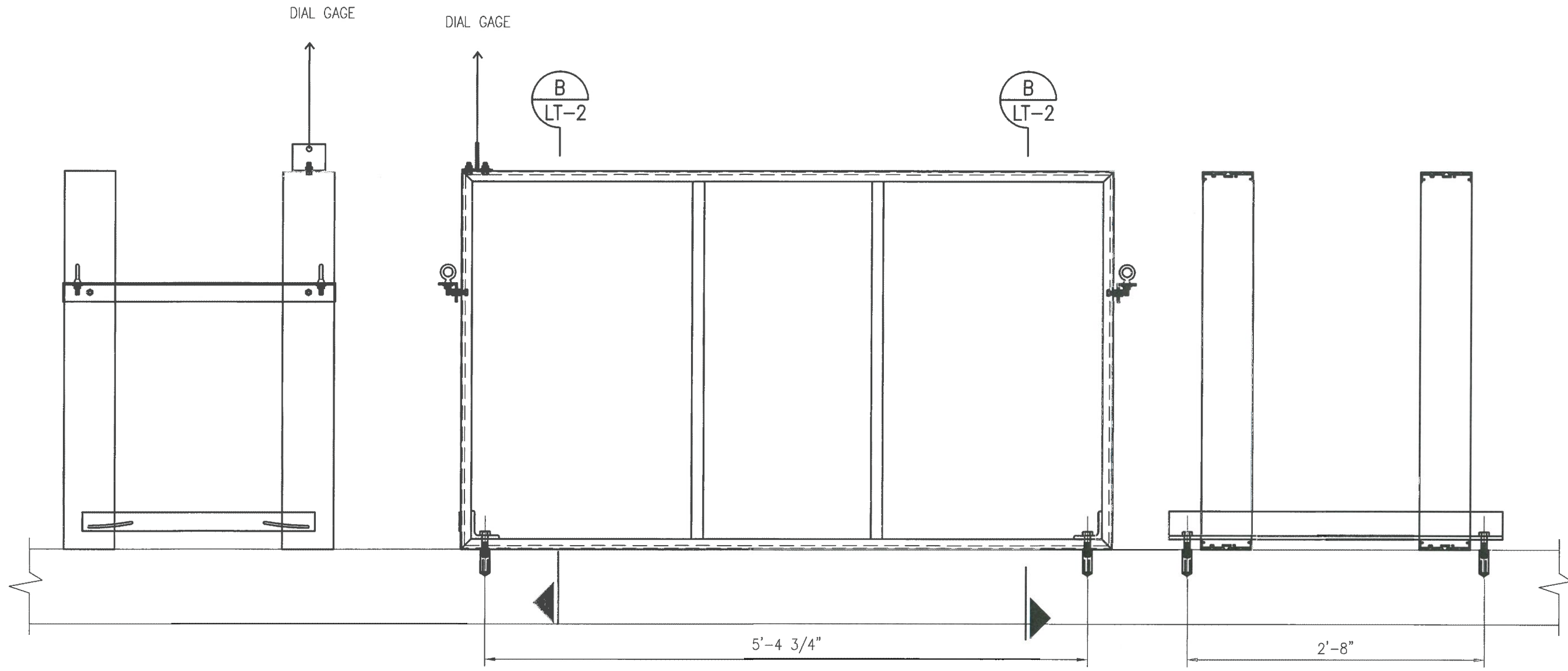
DATE OF TEST: FEB. 23, 2016  
 TESTED TO: 600 LBS  
 OBSERVATIONS: VERTICAL FRAME DEFLECTION ~ 1.5"  
 NO FAILURES

WITNESS: Ronald O Goetze  
 Ronald Goetze, PE

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PROJECT: STATIC CONTROLS CORPORATION  
 ANDON BOARD CONNECTION REVIEW  
 TITLE: 65"/70" DS LCD MONITOR FRAMES  
 CENTER SAFETY LUG TEST

DESIGN BY: RG  
 DRN BY: RG  
 DATE: 02/16/16  
 PROJECT NO.: 16-042  
 SHEET NO.: LT-1  
 REVISION



HOLD DOWN SUPPORT:  
 L3 x 3 x 3/8 or HSS x 3'-0" LONG  
 + (2) 5/8" DIA. HILTI HDI DROP-IN ANCHORS  
 (INSTALLED PER MANUFACTURER'S INSTRUCTIONS)  
 + (2) 5/8" DIA. X 2 1/4 GRADE 5 BOLTS

SECTION B  
 1"=1'-0" LT-2

65"/70" DS LCD MONITOR, TEST SETUP 2

SIDE FRAME/SAFETY CABLE LUG CONNECTIONS

DATE OF TEST: FEB. 23, 2016  
 TESTED TO: 500 LBS  
 OBSERVATIONS: SLIGHT FRAME DESTORTION  
 NO FAILURES

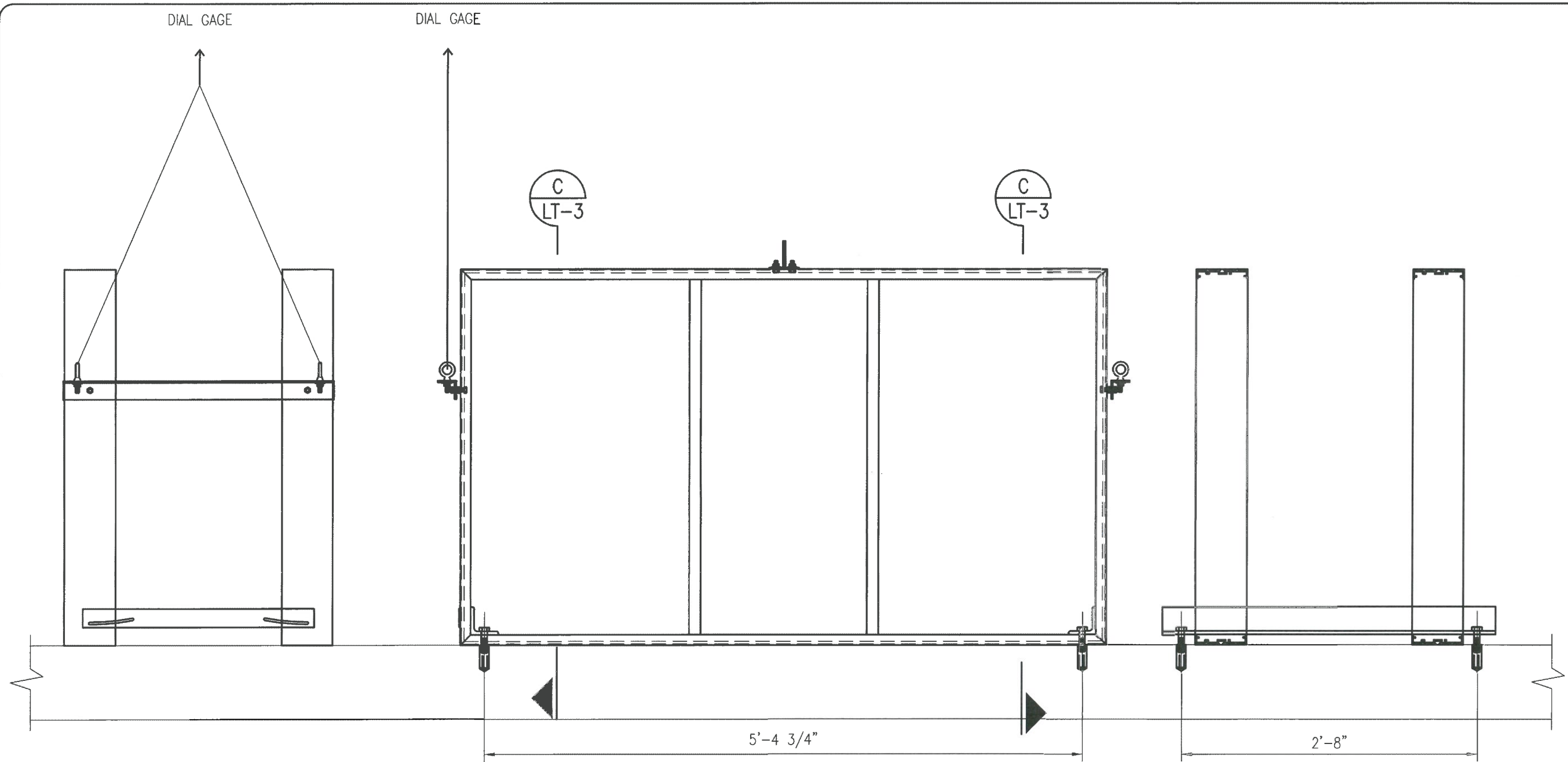
WITNESS:

*Ronald Goetze*  
 Ronald Goetze, PE

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PROJECT: STATIC CONTROLS CORPORATION  
 ANDON BOARD CONNECTION REVIEW  
 TITLE: 65"/70" DS LCD MONITOR FRAMES  
 SIDE FRAME CONNECTION TEST

DESIGN BY: **RG**  
 DRN BY: **RG**  
 DATE: **02/16/16**  
 PROJECT NO.: **16-042**  
 SHEET NO.: **LT-2**  
 REVISION



HOLD DOWN SUPPORT:  
 L3 x 3 x 3/8 or HSS x 3'-0" LONG  
 + (2) 5/8" DIA. HILTI HDI DROP-IN ANCHORS  
 (INSTALLED PER MANUFACTURER'S INSTRUCTIONS)  
 + (2) 5/8" DIA. X 2 1/4 GRADE 5 BOLTS

SECTION C  
 LT-3  
 1"=1'-0"

65"/70" DS LCD MONITOR, TEST SETUP 3

MAIN LUG CONNECTION

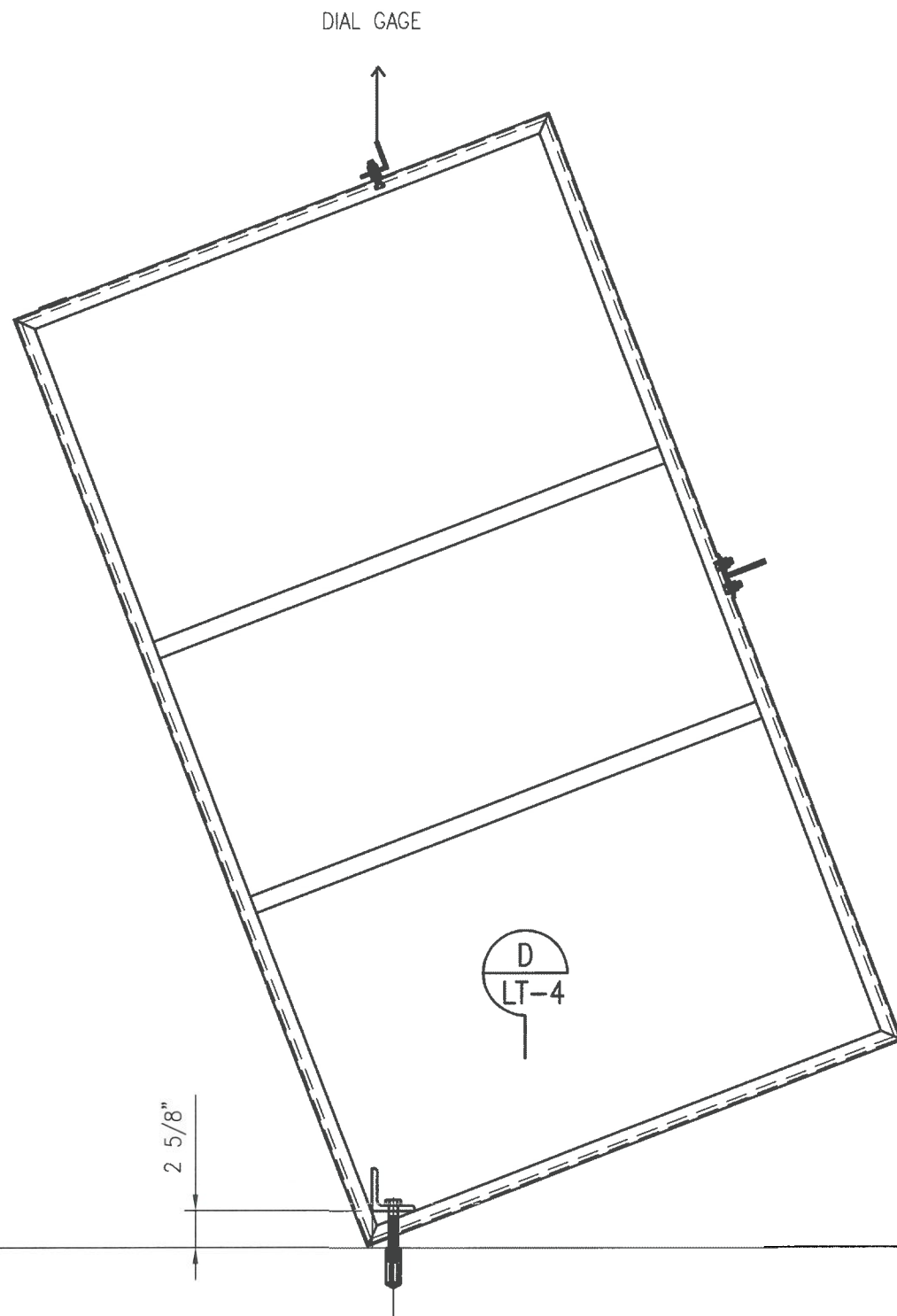
DATE OF TEST: FEB. 23, 2016  
 TESTED TO: 800 LBS  
 OBSERVATIONS: VERTICAL FRAME DEFLECTION ~ 1.5"  
 NO FAILURES

WITNESS: Ronald O Goetze  
 Ronald Goetze, PE

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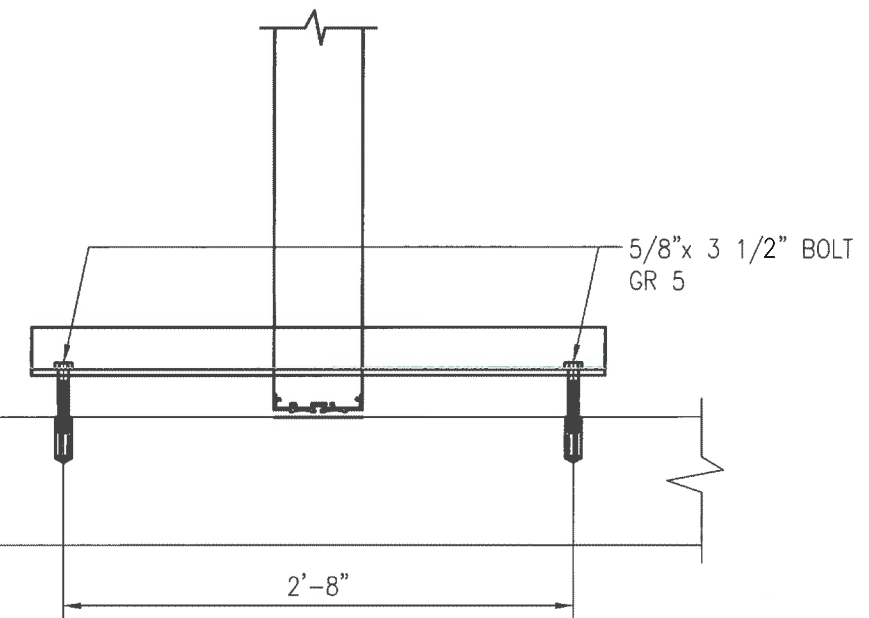
PROJECT: 65"/70" DS LCD MONITOR FRAMES  
 TITLE: ANDON BOARD CONNECTION REVIEW  
 SIDE ANGLE TEST 1

DESIGN BY: RG  
 DRN BY: RG  
 DATE: 02/16/16  
 PROJECT NO.: 16-042  
 SHEET NO.: LT-3  
 REVISION



DATE OF TEST: FEB. 23, 2016  
 TESTED TO: 500 LBS  
 OBSERVATIONS: FRAME DISTORTION,  
 NO FAILURES

WITNESS: *Ronald O Goetze*  
 Ronald Goetze, PE



65"/70" DS LCD MONITOR, TEST SETUP 4  
 FRAME & CONNECTIONS WHEN LOAD ON END SAFETY CABLE

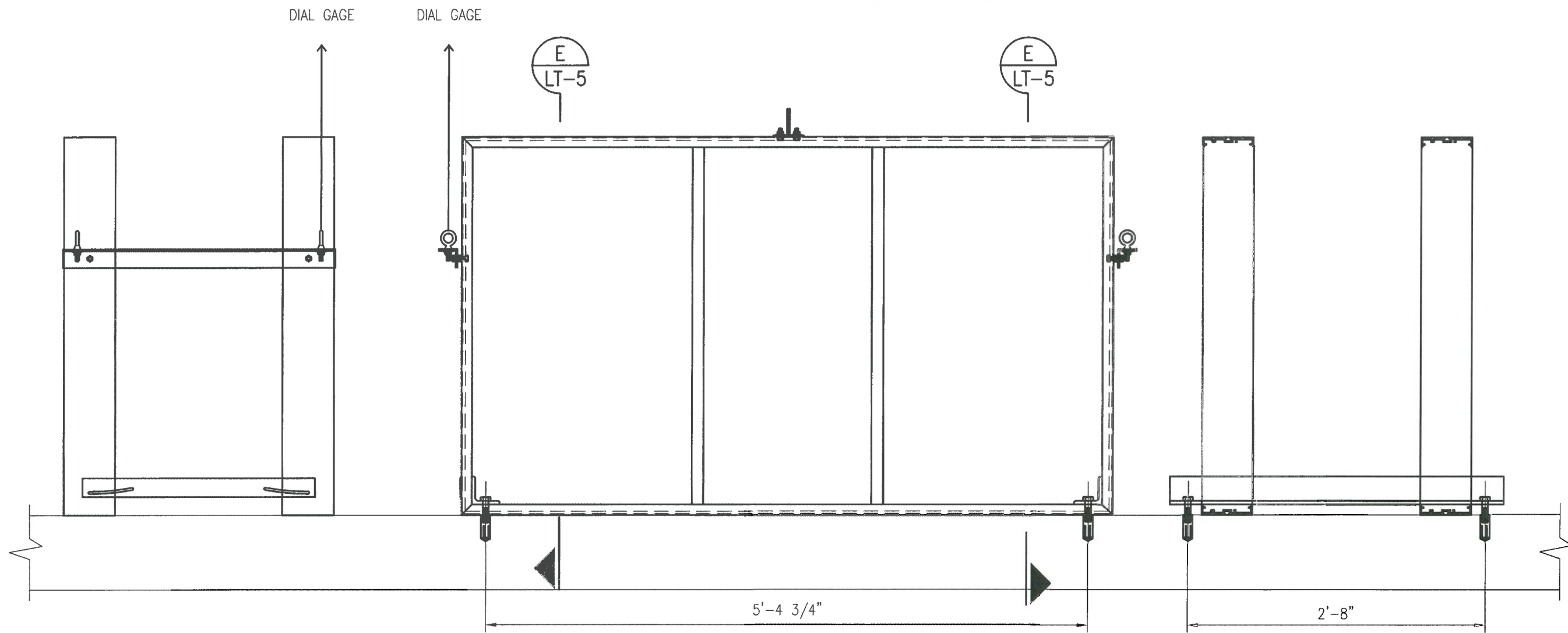
SECTION D  
 LT-4  
 1"=1'-0"

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PROJECT: STATIC CONTROLS CORPORATION  
 ANDON BOARD CONNECTION REVIEW  
 TITLE: 65"/70" DS LCD MONITOR FRAMES  
 SIDE ANGLE TEST 2 (SIMULATE SAFETY CABLE ONLY)

DESIGN BY: RG  
 DRN BY: RG  
 DATE: 02/16/16  
 PROJECT NO.: 16-042  
 SHEET NO.: LT-4  
 REVISION

B-4



HOLD DOWN SUPPORT:  
 L3 x 3 x 3/8 or HSS x 3'-0" LONG  
 + (2) 5/8" DIA. HILTI HDI DROP-IN ANCHORS  
 (INSTALLED PER MANUFACTURER'S INSTRUCTIONS)  
 + (2) 5/8" DIA. X 2 1/4 GRADE 5 BOLTS

SECTION E  
LT-5  
 1"=1'-0"

65"/70" DS LCD MONITOR, TEST SETUP 5

MAIN LUG CONNECTION

DATE OF TEST: FEB. 23, 2016  
 TESTED TO: 1100 LBS  
 OBSERVATIONS: CORNER CONNECTION SLIPPED  
 NO FAILURES

WITNESS: *Ronald O. Goetze*  
 Ronald Goetze, PE

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PROJECT: 65"  
 TITLE: ANDON BOARD CONNECTION REVIEW  
 70" DS LCD MONITOR FRAMES  
 SIDE ANGLE TEST 3

DESIGN BY: **RG**  
 DRN BY: **RG**  
 DATE: **02/16/16**  
 PROJECT NO.: **16-042**  
 SHEET NO.: **LT-5**  
 REVISION

B-5



# Appendix C

## (Load Test Pictures)





Photo 1: Test LT-1, Center Safety Lug [600 LBS]



Photo 2: Test LT-2, Side Frame Connection Test [400 LBS]



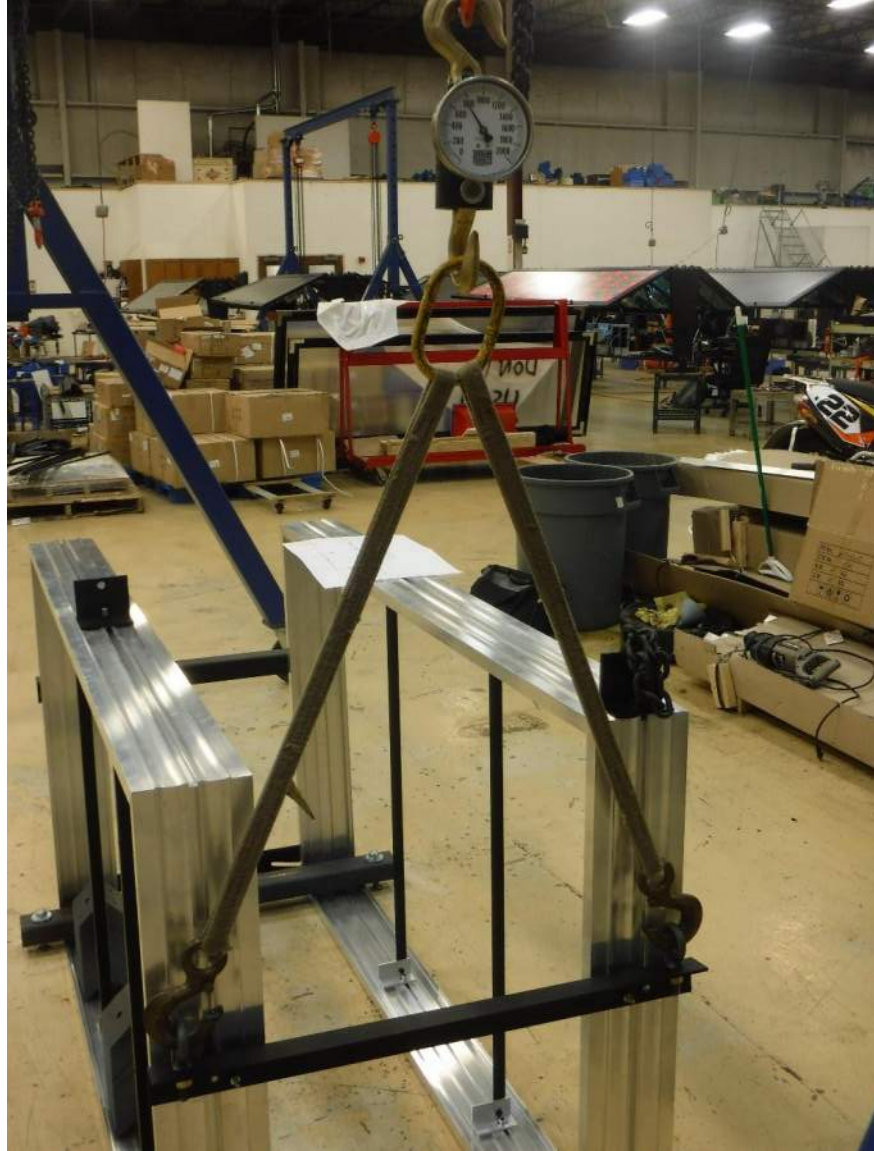


Photo 3: Test LT-3, Side Angle Test [800 LBS]



Photo 4: Test LT-4, Side Angle Test 2 [600 LBS]



Photo 5: Side Angle Test 2 [600 LBS]



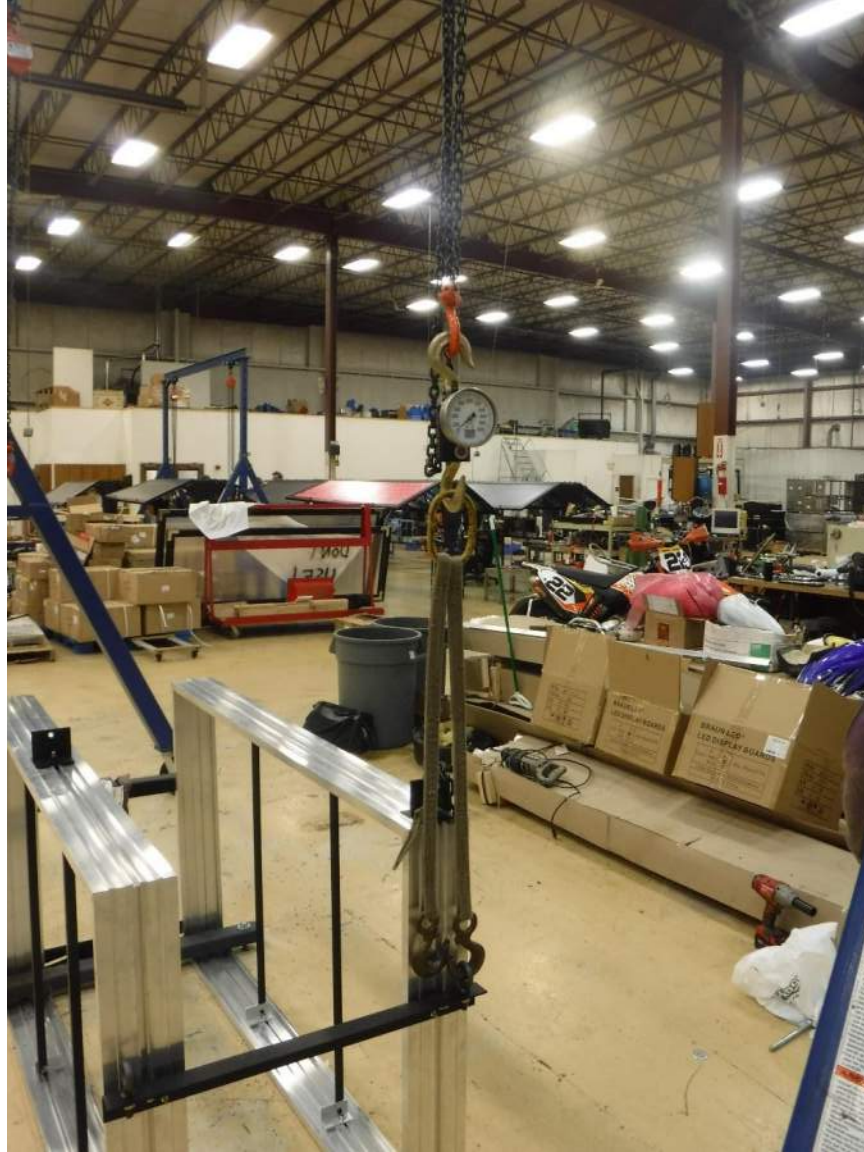


Photo 6: Test LT-5, Side Angle Test 3 [1100 LBS]



Photo 7: Test LT-5, Side Angle Test 3 [1100 LBS]

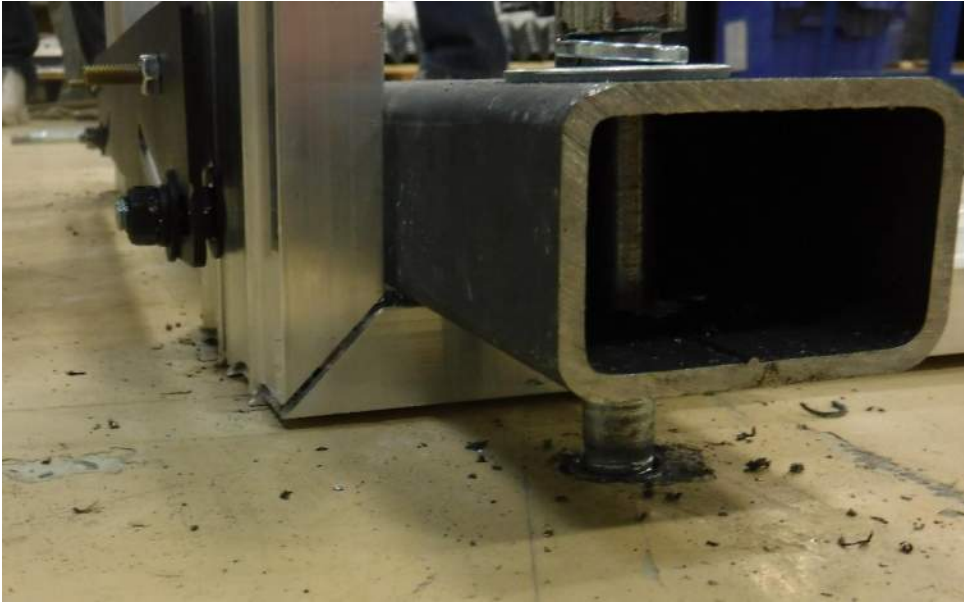


Photo 8: Test LT-5, Side Angle Test 3 [1100 LBS]



Photo 9: Test LT-5, Side Angle Test 3 [1100 LBS]



# Appendix D

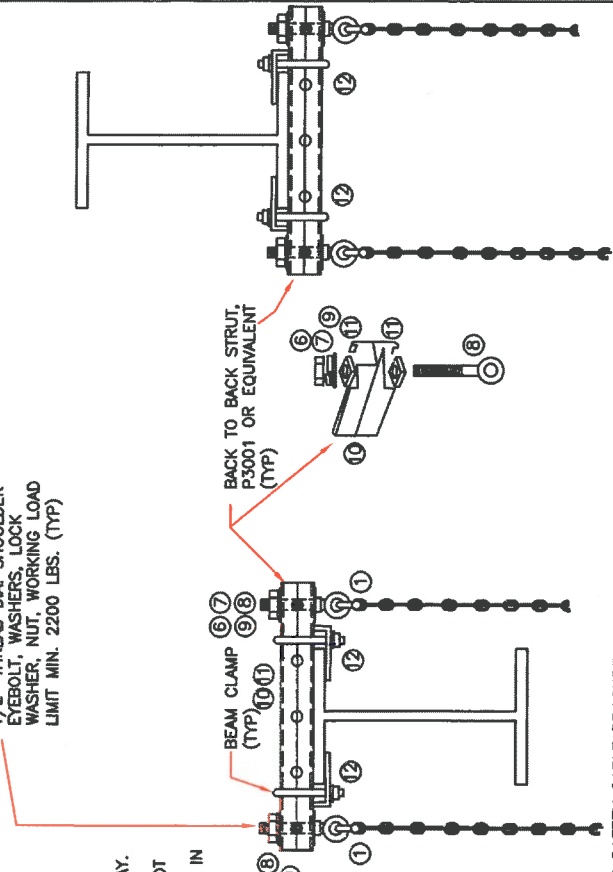
## (Andon Board Drawings)



SYM	REVISION	APP	DATE
A	ADDED SAFETY CABLE NOTE CHANGED TORQUE ON CONTROL BOX NUT.	BG	01/28/10

CHAIN AND UPPER AND LOWER SHACKLES SHALL BE OF CORROSION RESISTANT MATERIAL AND BE RATED FOR OVERHEAD LIFTING WITH A WORKING LOAD LIMIT OF 3000 LBS. VERTICAL CHAIN LOADING ONLY.

5/16" GRADE 80 CHAIN WITH (2 TOP & BOTTOM) 3/8" GALV BOLT NUT & COTTER ANCHOR SHACKLE-(3000 LB WILL)



1/2" THREAD DIA. SHOULDER EYEBOLT, WASHERS, LOCK WASHER, NUT, WORKING LOAD LIMIT MIN. 2200 LBS. (TYP)

SUPPORT FROM EACH EYEBOLT WITH EQUAL CHAIN LENGTHS.

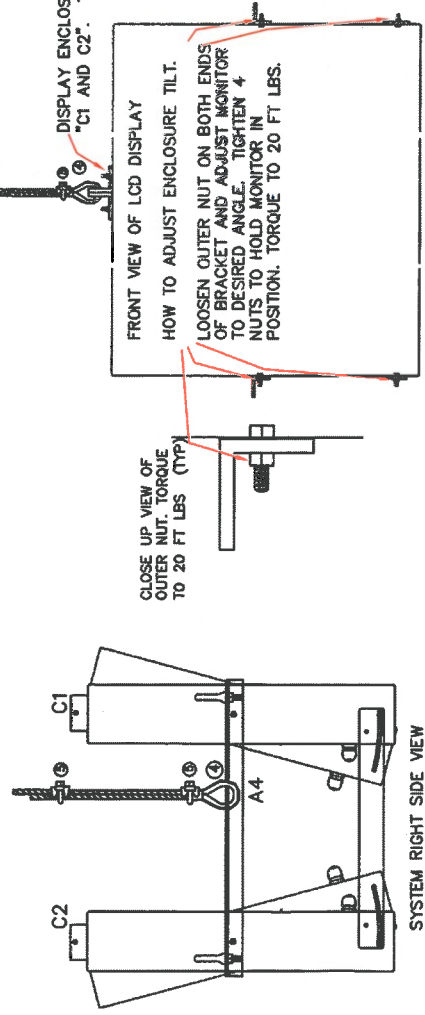
(2) SAFETY CABLES REQUIRED FOR EACH DISPLAY. LOOP AROUND BUILDING STEEL. (2) CROSBY CLAMPS AT EACH CONNECTION. CABLE SHALL NOT BE ROUTED OVER SHARP EDGES. NOTE: DO NOT LEAVE MORE THAN 2" OF SLACK IN SAFETY CABLE.

MINIMUM CLEARANCES BETWEEN BOARD AND NEARBY SURFACES:  
TOP: 6"  
BOTTOM: 12"  
SIDES: 36"  
FACE: 36"

DO NOT MOUNT BOARD ABOVE EQUIPMENT WHICH GENERATES HEAT.

CONTROL BOX ATTACHMENT NUTS. TORQUE TO 7 FT LBS (TYP)

SYSTEM LEFT SIDE VIEW



MONITOR FRONT VIEW TYP. PER SIDE

DB Size	System Foot Print Size	MAX (AMPS)	Weight (LBS)
70" SS LCD Monitor, with Control Box w/Music	40.5"H x 76"W x 29"D	7	210
70" DS LCD Monitor, with Control Box w/Music	40.5"H x 76"W x 29"D	10	370
65" SS LCD Monitor, with Control Box w/Music	37.5"H x 71"W x 29"D	7	170
65" DS LCD Monitor, with Control Box w/Music	37.5"H x 71"W x 29"D	10	290
55" SS LCD Monitor, with Control Box w/Music	31.5"H x 61"W x 29"D	6	150
55" DS LCD Monitor, with Control Box w/Music	31.5"H x 61"W x 29"D	9	250
42" SS LCD Monitor, with Control Box w/Music	26"H x 51"W x 29"D	5	130
42" DS LCD Monitor, with Control Box w/Music	26"H x 51"W x 29"D	8	210
Stand alone Control Box w/Music	19.5"H x 22.5"W x 8.6"D	3	50

TYPICAL ATTACHMENT OF BOARD SUPPORT CHAIN TO BUILDING STEEL

STATIC CONTROLS 990 FLEXIBLE ANDON BOARD MOUNTING (NOT TO SCALE)

1. LOCATION AND ELEVATION OF EACH UNIT TO BE DETERMINED IN FIELD PER SKETCH PROVIDED BY THE GM PROJECT ENGINEER.
2. MOUNTING METHOD(S) SHOWN ARE FOR REFERENCE ONLY. FINAL MOUNTING METHOD SHALL BE APPROVED BY CCRW AND PLANT ENGINEERING REPRESENTATIVES.

Installation contractor responsible for all local practices/codes and structural load verification


Customer Approved by M/T Date (6/18/08) Approved for Print (6/18/08) Scale (1/8"=1'-0") Part # SCC 990 Title (990W-INST-SCC) Rev # 1 of 8  
 990W-INST-SCC  
 FLEXIBLE ANDON BOARD INSTALLATION DRAWING VERSION W

SYM	REVISION	APP DATE
A		

**Install of one SCC 990 Flexible Andon Board & 8 Speaker Installation Hardware**

#	Description:	Manufacture	Part/Model Number	Unit of Measure	Purchase Quantity
1	3/8" 3000lb-WLL Galvanized Bolt Nut & Cotter Anchor Shackle	Fastenal Pricing	0504876	each	8
2	5/16" Grade 80 Chain 500 foot drum	Fastenal Pricing	45034	per foot	80
3	1/4" Class 6 x 19 Fiber Core Wire Rope 500 foot need about 80 per board	Fastenal Pricing	45576	per foot	80
4	1/4" Closed Galvanized Wire Rope Thimble	Fastenal Pricing	43443	each	4
5	1/4" Drop Forged Wire Rope Clip	Fastenal Pricing	43423	each	8
6	1/2" High Strength Nut (Furnished with item 8)	Fastenal Pricing		each	4
7	1/2" Heavy Lock Washer	Fastenal Pricing	33895	each	4
8	1/2"-13 x 4-1/2" Shank Length Hot Dipped Galvanized Drop Forged Eye Bolt	Fastenal Pricing	42445	each	4
9	1/2" High Strength Flat Washer	Fastenal Pricing	33847	each	4
10	Unistrut Channel: 1-5/8" x 2 3/4", 12 Gage, Back-to-Back, Slotted Holes P3001SH	Unistrut (Atkore)	P3001SH	1' (10' sticks)	1
11	Unistrut Flat Plate Fitting: Width 1-5/8" x 1-5/8", Thickness 1/4" P1064	Unistrut (Atkore)	P1064	each	8
12	Unistrut Beam Clamp: 1-5/8" x 5" P2786	Unistrut (Atkore)	P2786	each	4
13	Andon Speaker, SPEAKER STATIC CNTRL 977-SPKR-R EXTERNAL	SCC	1032-006X	each	8
14	1/4" Beam Clamp: Speaker Installation	Appleton	BH-500	each	100
15	Speaker Cable/Wire: Order in 1,000' spools	Belden	8471	per foot	1,000
16	Bridle Rings and Saddles: 1/4"-20 x 7/8" 2 Boxes (50/Box)	B-Line	each	BRS-32A	60
17	Cat5e Cable: General Cable GenSPEED® 5000, 1,000 ft. Pull-Pac® II, Non-Plenum, Blue For one board using 333feet of 1000foot roll	General Cable	each	5133299E	333
18	Wire Nuts: For Speaker Terminations		each		16

Installation contractor responsible for all local practices/codes and structural load verification

 Static Controls Corporation 30490 WIXOM ROAD WIXOM, MI 48196 (248) 926-4400 FAX (248) 926-4412		Customer Approved By: _____ Date: 10/20/08 Scale: N/A Part # SCC 990 Title: FLEXIBLE ANDON BOARD INSTALLATION DRAWING VERSION W Page # 2 of 3 990W-INST-SCC
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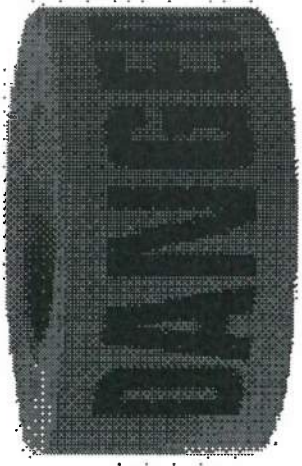
SYM	REVISION	APP DATE
A	ADDED SAFETY CABLE NOTE CHANGED TORQUE ON CONTROL BOX NUT.	06/28/16

**BARRICADE PERIMETER TAPE**

RED DANGER TAPE (INDICATES HAZARD TO PEOPLE); CROSSING THIS BARRICADE COULD LEAD TO INJURY. NEVER CROSS RED BARRICADE TAPE UNLESS GRANTED PERMISSION BY AN AUTHORIZED EMPLOYEE.

**SOME EXAMPLES INCLUDE:**

- OVERHEAD WORK, ARIAL LIFT, MOBILE CRANE, ETC.
- RIGGING APPLICATIONS



**SEE WEB LINKS FOR MORE INFO.**

[https://www.construction.safety.ca.gov/toolbox/documents/wireropesafety\\_000.pdf](https://www.construction.safety.ca.gov/toolbox/documents/wireropesafety_000.pdf)  
<https://www.cdrules.com/articles.html>  
<https://www.safetymag.com/articles/view-article.html?id=602&itemid=178>

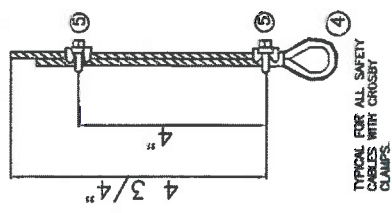
**WARNINGS AND APPLICATION INSTRUCTIONS.**

- THIS APPLICATION REQUIRES TWO CROSSBY WIRE ROPE CLAMPS - INSTALLATION INSTRUCTIONS
- 1st CLAMP APPLY APPROXIMATELY 3/4" FROM DEAD END ABOUT IS PLACED OVER DEAD END OF 1/4" WIRE ROPE. LIVE END REST IN THE SADDLE.
  - 2ND CLAMP APPLY NEAR THE THIMBLE.
  - NOTE: ALL NUTS TIGHTEN EVENLY, ALTERNATING TURNS.

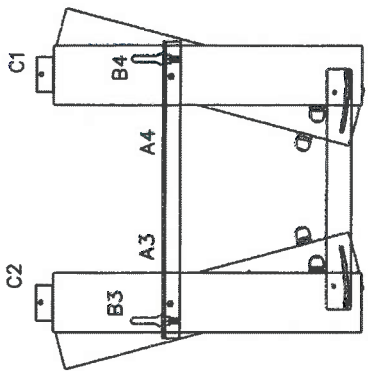
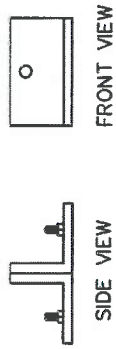
Installation contractor responsible for all local practices/codes and structural load verification

<p>Static Controls Corporation          30450 WIXOM ROAD          WIXOM, MI 48393          TEL: (248) 926-4412          FAX: (248) 926-4412</p>	Customer Approval	By	Date	Part # SCC 990 Rev # 1 Date # 06/28/16 Page # 1 of 8
	Flexible Andon Board Installation Drawing Version W	MT	App	06/28/16

990W-INST-SCC



SAFETY CABLE BRACKET C1 AND C2



SYSTEM RIGHT SIDE VIEW NON CONTROL BOX SIDE



TOP VIEW ANGLE BRACKET NON CONTROL BOX SIDE



SYSTEM LEFT SIDE VIEW -CONTROL BOX SIDE



TOP VIEW ANGLE BRACKET CONTROL BOX SIDE



SYSTEM RIGHT SIDE VIEW NON CONTROL BOX SIDE

1 - BEAM OF BUILDING STEEL

(2) SAFETY CABLES REQUIRED FOR EACH DISPLAY BOARD SYSTEM. LOOP AROUND BUILDING STEEL.

(2) CROSSBY CLAMPS AT EACH CONNECTION. CABLE SHALL NOT BE ROUTED OVER SHARP EDGES.

NOTE: DO NOT LEAVE MORE THAN 2" OF SLACK IN SAFETY CABLE.

**RIGGING POINTS - A1, A2, A3, A4 WITH INSTALLATION CONTRACTORS HARDWARE. HOLE SIZED FOR 1/2" HARDWARE (0.53").**

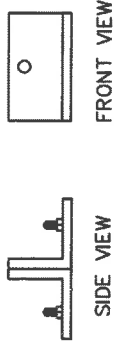
**MOUNTING POINTS - B1, B2, B3, B4 WITH CHAIN AS SHOWN ON PAGE 1.**

**SAFETY CABLE POINTS - A1 TO A4, AND C1 TO C2. NOTE: DO NOT LEAVE MORE THAN 2" OF SLACK IN SAFETY CABLE.**

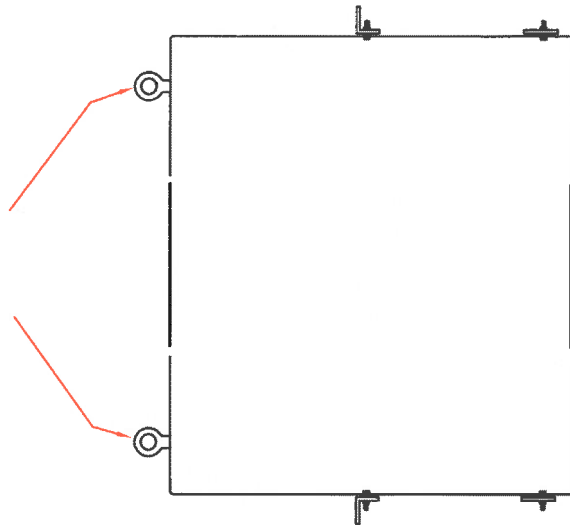
# MODIFICATIONS REQUIRED TO ACCOMMODATE NEW GM SAFETY CABLE REQUIREMENTS PERFORM ALL MODIFICATIONS WITH 990 SYSTEM ON THE GROUND

SYM	REVISION	APP DATE
A	ADDED SAFETY CABLE NOTE CHANGED TORQUE ON CONTROL BOX NUT.	06/01/2010
B	ITEMS MOVED TO PAGES 2,3,4,5	06/09/2010

SAFETY CABLE BRACKET C1 AND C2

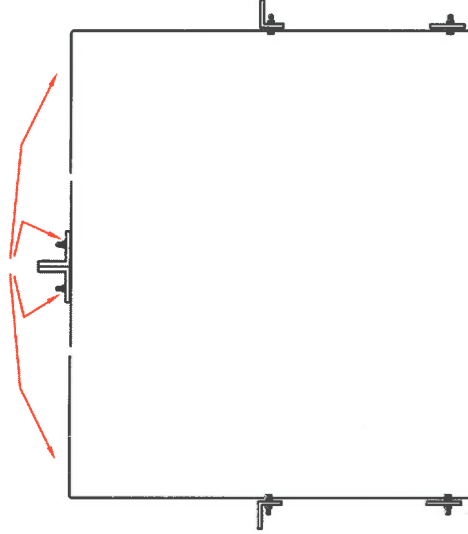


STEP 1 - REMOVE EYE NUTS ON TOP OF  
DISPLAY (2 PER DISPLAY)



MONITOR FRONT VIEW

STEP 2 - USE EXISTING BOLTS AND WASHERS, SLIDE TO  
THE CENTER OF DISPLAY TO MOUNT C1 (BACK  
DISPLAY) AND C2 (FRONT DISPLAY) BRACKET USING  
NYLOC NUTS AT 10 FT LBS OF TORQUE.



MONITOR FRONT VIEW

Installation contractor responsible for all local practices/codes  
and structural load verification

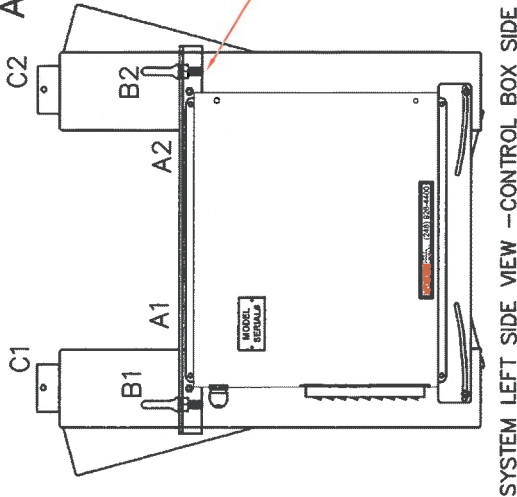
 <b>SOC</b> Stalder Cable Corporation 30460 WIXOM ROAD WIXOM, MI 48196 (519) 826-4400 FAX (248) 826-4412	Customer Approved By	MTY	DATE
	by	App	10/29/2008
	Approved for Print	DATE	BY
		10/29/2008	MTY
	Customer Name	FLEXIBLE ANDON BOARD	
	Customer Part #	SAFETY CABLE	
	Customer Part #	MODIFICATION DRAWING	
	Customer Part #	Part # 9900 080	
	Customer Part #	Page #	
	Customer Part #	Page 1 of 3	
	Customer Part #	990INST MOD	

# MODIFICATIONS REQUIRED TO ACCOMMODATE NEW GM SAFETY CABLE REQUIREMENTS

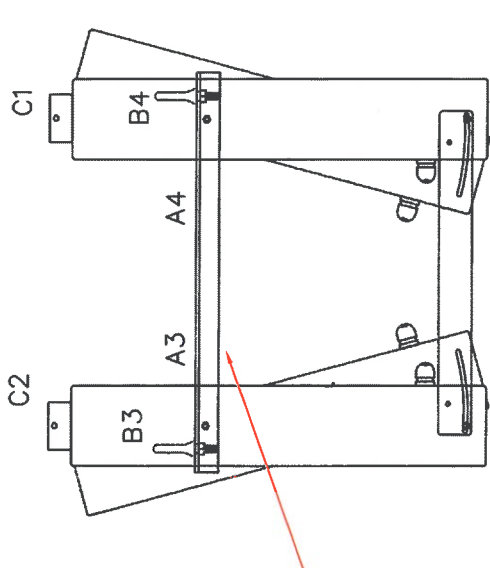
## PERFORM ALL MODIFICATIONS WITH 990 SYSTEM ON THE GROUND

SYM	REVISION	APPL DATE
A	ADDED SAFETY CABLE NOTE CHANGED TORQUE ON CONTROL BOX NUT.	BG 01/28/10
B	ITEMS MOVE TO PAGES 3,4,5	BG 02/03/10

STEP 3 - DRILL 9/16" HOLE FOR A1, A2, A3, AND A4.

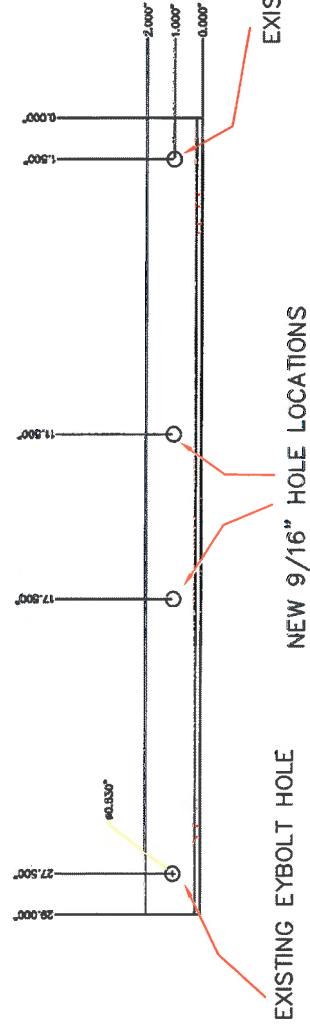


SYSTEM LEFT SIDE VIEW - CONTROL BOX SIDE



SYSTEM RIGHT SIDE VIEW NON CONTROL BOX SIDE

STEP 3 - DRILL TWO 9/16" HOLES IN EACH SIDE HANGING BRACKET FOR A1, A2, A3, AND A4.



Installation contractor responsible for all local practices/codes and structural load verification

RIGGING POINTS - A1, A2, A3, A4 WITH INSTALLATION CONTRACTORS HARDWARE.

SAFETY CABLE POINTS - A1 TO A4, AND C1 TO C2.

 SOUTHERN UNION State Controls Corporation 3000 WILSON ROAD WILSON, NC 27157 (252) 828-4400 FAX (252) 928-4412	Customer Approved By App Date (M/D/Y)	Project No. (M/D/Y)	Issue (M/D/Y)
	Project Name (M/D/Y)	Scale (M/D/Y)	Drawing No. (M/D/Y)
Project: FLEXIBLE ANDON BOARD SAFETY CABLE MODIFICATION DRAWING Part: J.E.C.G. 990 Rev: 7 Drawn By: J.E.C.G. Checked By: J.E.C.G. Approved By: J.E.C.G. Date: 01/28/10 Scale: N/A Drawing No.: 990INST MOD			

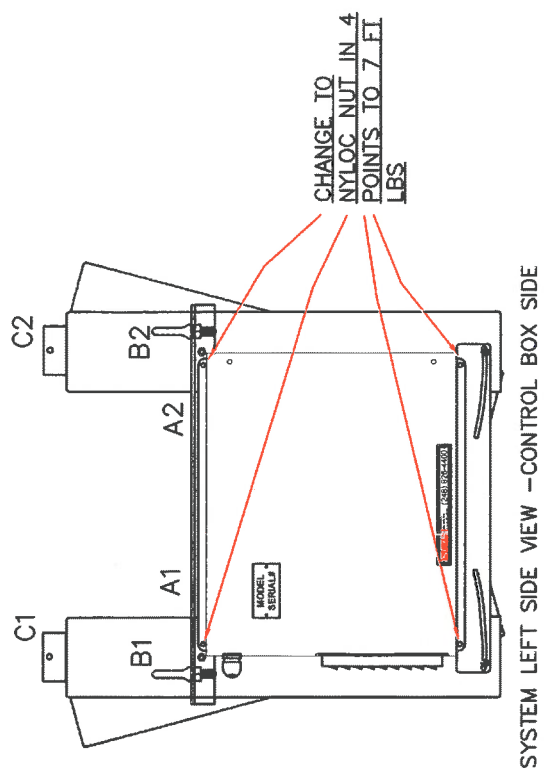


# MODIFICATIONS REQUIRED TO ACCOMMODATE NEW GM SAFETY CABLE REQUIREMENTS

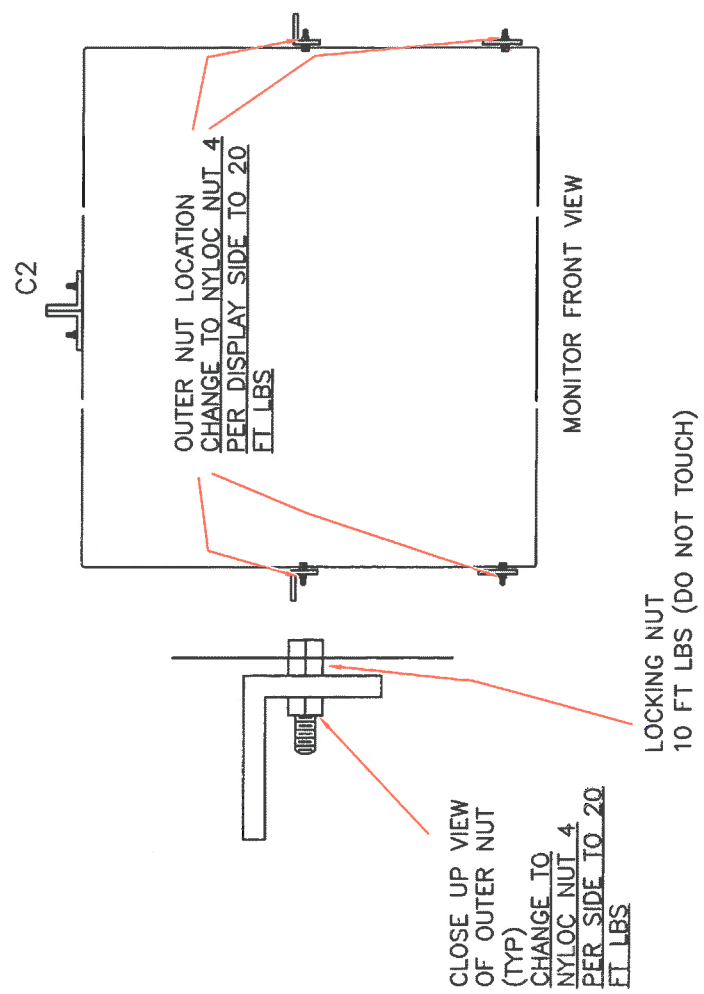
## PERFORM ALL MODIFICATIONS WITH 990 SYSTEM ON THE GROUND

SYM	REVISION	APP	DATE
A	ADDED SAFETY CABLE NOTE CHANGED TORQUE ON CONTROL BOX NUT.	BC	01/28/10
B	PAGE ADDED	BC	06/05/10

**STEP 4 - REPLACE (4) HOLDING NUTS ON CONTROL BOX WITH NYLOC NUTS. TORQUE TO 7 FT LBS.**



**STEP 5 - REPLACE OUTER NUTS (4) PER DISPLAY ON SIDE BRACKETS WITH NYLOC NUTS. TORQUE TO 20 FT LBS.**



Installation contractor responsible for all local practices/codes and structural load verification

<p><b>SOC</b> Stable Controls Corporation</p> <p>5046D WIXOM ROAD WIXOM, MI 48196 (313) 826-4400 FAX (248) 826-4412</p>	Customer Approved	By	App	Date	Scale	Sheet
	<p>MT</p> <p>App</p>	<p>10/29/2008</p> <p>10/29/2008</p> <p>10/29/2008</p>	<p>10/29/2008</p> <p>10/29/2008</p> <p>10/29/2008</p>	<p>10/29/2008</p> <p>10/29/2008</p> <p>10/29/2008</p>	<p>10/29/2008</p> <p>10/29/2008</p> <p>10/29/2008</p>	<p>10/29/2008</p> <p>10/29/2008</p> <p>10/29/2008</p>
<p>Customer Approved</p> <p>By</p>		<p>Part # 990C 990</p> <p>(See Engineering Approval Page # 2 of 8)</p>		<p>990INST MOD</p>		

# MODIFICATIONS REQUIRED TO ACCOMMODATE NEW GM SAFETY CABLE REQUIREMENTS

## PERFORM ALL MODIFICATIONS WITH 990 SYSTEM ON THE GROUND

SYM	REVISION	APP	DATE
A	ADDED SAFETY CABLE NOTE CHANGED TORQUE ON CONTROL BOX NUT.	EG	01/28/18
B	PAGE ADDED	EG	02/05/18

### SCC TESTING (VERTICAL LOAD)

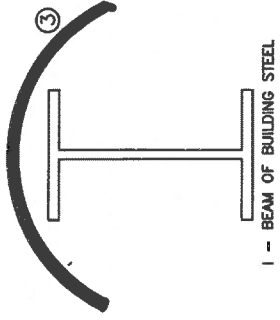
B1, B2, B3, OR B4 - SUCCESSFUL AT 1400 LBS PER POINT  
 C1, OR C2 - SUCCESSFUL AT 1400 LBS PER POINT

**RIGGING POINTS - A1, A2, A3, A4 WITH  
 INSTALLATION CONTRACTORS HARDWARE.**

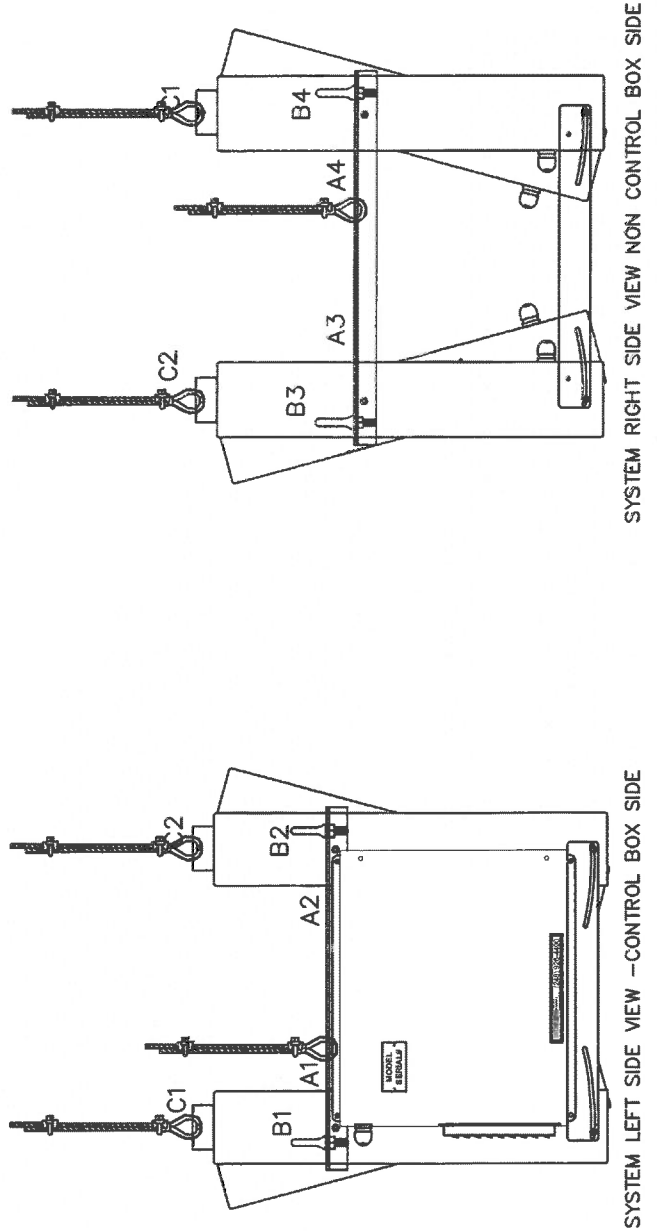
**MOUNTING POINTS - B1, B2, B3, B4 WITH  
 CHAIN AS SHOWN ON PAGE 5.**

**SAFETY CABLE POINTS - A1 AROUND BUILDING  
 STEEL TO A4, AND C1 AROUND BUILDING  
 STEEL TO C2**

**NOTE: DO NOT LEAVE MORE THAN 2" OF SLACK  
 IN SAFETY CABLE.**



- (2) SAFETY CABLES REQUIRED FOR EACH DISPLAY BOARD SYSTEM. LOOP AROUND BUILDING STEEL.
  - (2) CROSBY CLAMPS AT EACH CONNECTION. CABLE SHALL NOT BE ROUTED OVER SHARP EDGES.
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Installation contractor responsible for all local practices/codes and structural load verification

<p><b>SOC</b>                  Safety Cable Corporation                  30450 WIXOM ROAD                  WIXOM, MI 48196                  (248) 826-4400                  FAX (248) 926-4412</p>	Approved For MT App	Approved For Pract. Date 10/29/18	Project Name 990INST MOD
	By Date 10/29/18	Project # 990INST MOD	Drawing # 990INST MOD

SYM	REVISION	APP	DATE
A	ADDED SAFETY CABLE NOTE CHANGED TORQUE ON CONTROL BOX NUT.	BC	01/28/10
B	PAGE ADDED	BC	02/03/10

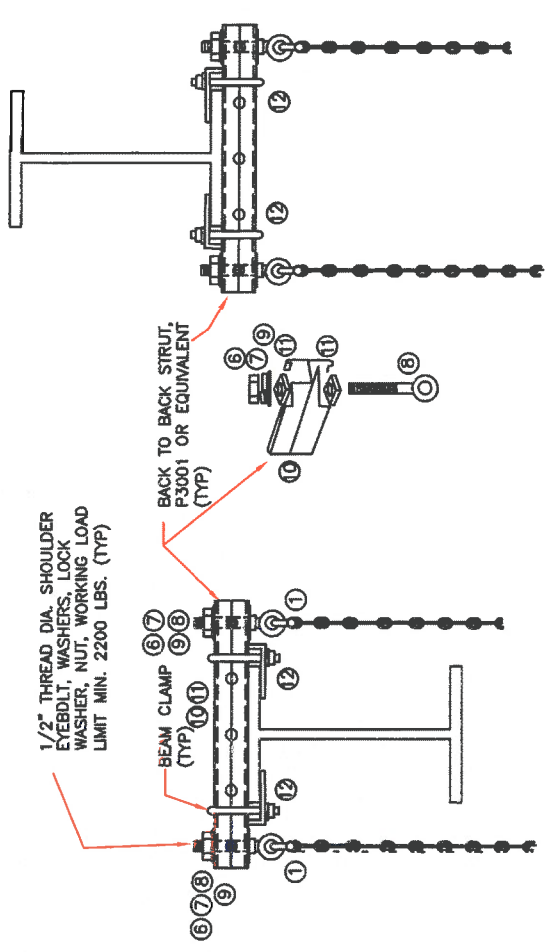
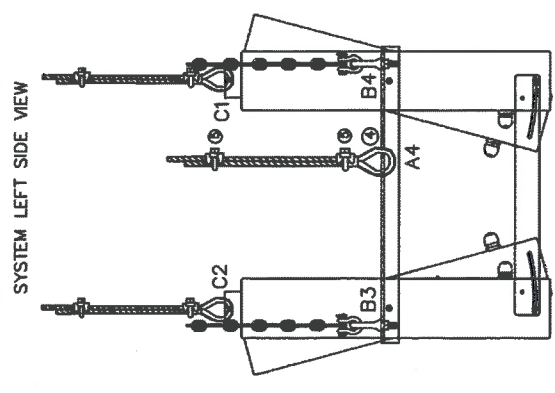
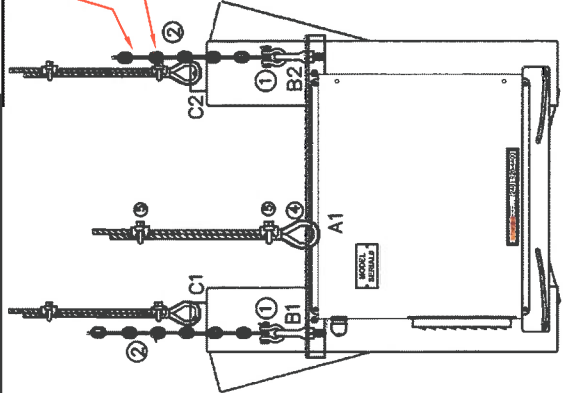
5/16" GRADE 80 CHAIN WITH (2 TOP & BOTTOM)  
3/8" GALV BOLT NUT & COTTER ANCHOR  
SHACKLE-(3000 LB WLL)

SUPPORT FROM EACH EYEBOLT  
WITH EQUAL CHAIN LENGTHS.

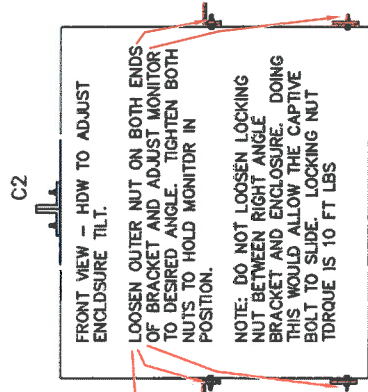
CHAIN AND UPPER AND LOWER  
SHACKLES SHALL BE OF  
CORROSION RESISTANT MATERIAL  
AND BE RATED FOR OVERHEAD  
LIFTING WITH A WORKING LOAD  
LIMIT OF 3000 LBS.  
VERTICAL CHAIN LOADING ONLY.

MINIMUM CLEARANCES BETWEEN BOARD  
AND NEARBY SURFACES:  
TOP: 6"  
BOTTOM: 12"  
SIDES: 36"  
FACE: 36"

DO NOT MOUNT BOARD ABOVE  
EQUIPMENT WHICH GENERATES HEAT.



TYPICAL ATTACHMENT  
OF BOARD SUPPORT CHAIN  
TO BUILDING STEEL



MONITOR FRONT VIEW

FRONT VIEW - HDW TO ADJUST  
ENCLOSURE TILT.

LOOSEN OUTER NUT ON BOTH ENDS  
OF BRACKET AND ADJUST MONITOR  
TO DESIRED ANGLE. TIGHTEN BOTH  
NUTS TO HOLD MONITOR IN  
POSITION.

NOTE: DO NOT LOOSEN LOCKING  
NUT BETWEEN RIGHT ANGLE.  
BRACKET AND ENCLOSURE. DOING  
THIS WOULD ALLOW THE CAPTIVE  
BOLT TO SLIDE. LOCKING NUT  
TORQUE IS 10 FT LBS

STATIC CONTROLS 990 FLEXIBLE ANDON BOARD MOUNTING  
(NOT TO SCALE)

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Installation contractor responsible for all local practices/codes  
and structural load verification

**SOC**  
Static Controls Corporation

30460 WIXOM ROAD  
WIXOM, MI 48196  
(248) 936-4400  
FAX (248) 936-4412

Customer Approved By: MT  
App: App  
Date: 01/28/10  
Approved For Prod: MT  
Job No: N/A  
Project: N/A  
Sheet: 990-INST-MOD

This FLEXIBLE ANDON BOARD  
SAFETY CABLE  
MODIFICATION DRAWING  
Issued: 10/1/09  
Page 1 of 3