

<u>Moisture in concrete roof decks</u>



























2009 bulletin

"...SDI does not recommend the use of roofing membranes attached to the steel deck using line patterns with large spacing unless a structural engineer has reviewed the adequacy of the steel deck and the structural supports to resist to wind uplift loads transmitted along the lines of attachment. Those lines of attachment shall only be perpendicular to the flutes of the deck."





			FM G	lohal									
			Prope	rty Los	s Preve	ntion D	ata She	ets		1-29			
						(0.0			~ ~				
Table 1C. Maximum Steel Deck Span (ft) for 11/2 in. (38 mm) Deep, Wide Rib (Type B) Steel Deck with an Adhered Root Covor, for Wind Patings from 50 to 225 ocf (2.0 to 10.9 kPa)													
(NOTE:	Cover, for wind Hatings from 60 to 225 psf (2.9 to 10.8 kPa) F: Use this table when the distance between rows of roof cover fasteners is one-half the deck span or less. Green												
			fon	t indicate	s that de	oflection	governs	over ber	ding stre	955.)			
Yield					UI	timate W	ind Ratir	g per R	oofNav (p	osf)			
Stress	Deck					1	Maximum	Span (f	t)				
psi	Gauge	60	75	90	105	120	135	150	165	180	195	210	225
33,000	22	7.10	7.10	7.10	7.10	7.07	6.67	6.33	6.03	5.78	5.55	5.35	5.17
	20	7.78	7.78	7.78	7.78	7.78	7.43	7.05	6.72	6.44	6.18	5.96	5.76
	18	9.08	9.08	9.08	9.08	9.08	8.66	8.22	7.84	7.50	7.21	6.95	6.71
	16	10.36	10.36	10.36	10.36	10.36	9.89	9.38	8.94	8.56	8.23	7.93	7.66
40,000	22	7.10	7.10	7.10	7.10	7.10	7.10	6.96	8.64	6.35	6.10	5.88	5.68
	20	7.78	7.78	7.78	7.78	7.78	7.78	7.76	7.40	7.08	6.80	6.56	6.33
	18	9.08	9.08	9.08	9.08	9.08	9.08	9.04	8.62	8.25	7.93	7.64	7.38
	16	10.36	10.36	10.36	10.36	10.36	10.36	10.32	9.84	9.42	9.05	8.72	8.43
45,000	22	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.04	6.74	6.48	6.24	6.03
	20	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.51	7.22	6.95	6.72
	18	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	8.76	8.41	8.11	7.83
	16	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	9.99	9.60	9.25	8.94
50,000	22	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	6.93	6.66	6.42	6.20
	20	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.72	7.42	7.15	6.91
	18	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.00	8.65	8.33	8.05
	16	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.28	9.87	9.51	9.19
55,000	22	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	6.90	6.67
	20	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.69	7.43
	18	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	8.97	8.66
	16	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.24	9.89
60,000	22	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	6.97
+	20	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.77
	18	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.06
	16	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.34
			Green	font indi	cates that	at deflect	ion gove	rns over	bending	stress.			
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Technical issues posing liability risks for your business



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LegalCo Rosemont, IL

Technical issues posing liability risks for your business















	ĪĪ.	Technical Note - No. 7	
	The steel deck bending and shear streng fasteners attaching the deck to the supp Specification for the Design of Cold-Form Standard for Steel Roof Deck (ANSI/SDI RI the specified minimum mechanical prog strength) for the roof deck, and should 1 testing. Results of field-tests utilized to co mechanical properties of the steel deck, through deck, must recognize the proge limits required by the steel specification	gth (resistance) and strength (resistance) of the ports are calculated using the <i>North American</i> <i>ed Sett Structural Members</i> (NAIS 1500-16) and the ID-2017). These design strengths are dependent on perities (i.e. base steel thickness yield and ultimate be lower than the strength determined by field- determine strengths which are dependent on the such as pull-out or pull-over of a scower fastemed erties of the delivered steel may exceed the minimum . Therefore, field-strengths.	
SDI Recom	mendations		
1. 7 5 2. V 3. 7 4. [6 6 6 6 6 6 6 6 6	The SDI does not recommend the deck using line patterns with larg span) unless a structural enginee and the structural supports to res- of attachment. When existing buildings with stee mechanically attached membran- engaged to determine the limitat The lines of attachment for mech- perpendicular to the ribs of the d ines of fasteners parallel to the d- Designers should require pre-con ensure that the lines of fasteners design assumptions. Determinati option of field crews.	e use of roofing membranes attack ge spacing (spacing greater than 1 er has reviewed the adequacy of th sist wind uplift loads transmitted a el roof deck are recovered or reroof to, a competent structural engineer tions imposed by the existing steel hanically attached membranes shal leck. Membranes should not be att leck ribs. nstruction submittals of membrane (direction and spacing) comply wit ion of membrane layouts should not	hed to the steel /2 of the deck he steel deck along the lines fed with a r should be I deck. I only be tached with e layouts to th structural ot be left to the











Who in your company "accepts" steel roof deck?

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The roofing industry needs to re-think the concept of "deck acceptance."

Deck acceptance should be limited to:

- Its physical presence
- Top surface is visually dry
- Surface is broom clean

If we do not limit deck acceptance, we do nothing other than incur someone else's liability (and not get paid for it).

New FM Global Loss Prevention Data Sheets

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Significant changes in FM 1-28, Feb. 2020

- Wind load determination tables have been removed from FM 1-28; now use the ratings calculator in RoofNav
- FM 1-28 now uses ASCE 7-16's pressure coefficients and zones
- FM 1-28 still uses ASCE 7-05's 100-year MRI maps
- FM 1-28 still uses the allowable strength design (ASD) method
- FM 1-28 uses (adds) an Importance Factor of 1.15

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Example: A lo building is an located in an	ow-rise office build enclosed structure open terrain area	ing (Risk Catego e with a mean ro that can be cate	ry II) is located oof height of 60 gorized as Expo	in Chicago, IL. ⁻) ft. The buildin osure Category	Гhe g is C.
Document	speed (mph)	Zone 1'	Zone 1	Zone 2	Zone 3
ASCE 7-05	V _{ASD} = 90		24	40	58
FM 1-28 (old)	V _{ASD} = 90		27	FM 1-60	69
FM 1-28 (new)	V _{ASD} = 90	24	43	FM 1-90	77
ASCE 7-10 Ult.	V _{ULT} = 115		39	65	97
ASCE 7-10 ASD	V _{ASD} = 90		23	39	58
ASCE 7-16 Ult.	V _{ULT} = 105	30	51	67	92
ASCE 7-16 ASD	V _{ASD} = 90	18	31	41	55

Comparing ASCE 7-05, FM 1-28, ASCE 7-10 and ASCE 7-16

Example: A high-rise office building (Risk Category II) is located in Chicago, IL. The building is an enclosed structure with a mean roof height of 150 ft. The building is located in an open terrain area that can be categorized as Exposure Category C.

Document	Basic wind	Design wind pressure (psf)							
	speed (mph)	Zone 1' (Center)	Zone 1 (Field)	Zone 2 (Perimeter)	Zone 3 (Corners)				
ASCE 7-05	V _{ASD} = 90		38	60	82				
FM 1-28 (old)	V _{ASD} = 90		44	69	94				
FM 1-28 (new)	V _{ASD} = 90		44	FM 1-90	94				
ASCE 7-10 (Ult.)	V _{ULT} = 115		63	98	134				
ASCE 7-10 ASD	V _{ASD} = 90		38	59	80				
ASCE 7-16 Ult.	V _{ULT} = 105		52	82	112				
ASCE 7-16 ASD	V _{ASD} = 90		31	49	67				

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The values derived from FM 1-28 are not consistent with ASCE 7-16's ASD values (IBC 2018). Using FM 1-28 typically results in higher design wind loads.

Complying with the code is a minimum legal requirement.

- Where FM 1-28 is lower, use the code's required wind loads
- Where the codes values are lower, FM 1-28's values may be a project-specific contract requirement

FM Global intends FM 1-28 to be effective immediately (i.e., as of February 26, 2020) upon publication

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