



Fall Education Seminar
October 4, 2018

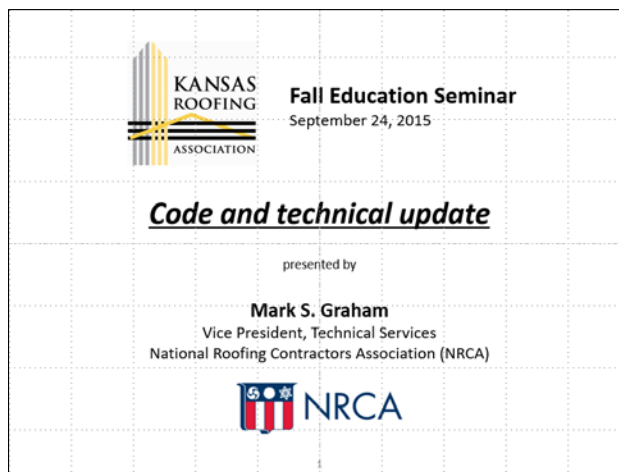
Code and technical issues update

presented by

Mark S. Graham
Vice President, Technical Services
National Roofing Contractors Association (NRCA)




2015 I-codes



<http://www.marksgraham.com/presentations.html>

2018 I-codes




**KANSAS
ROOFING
ASSOCIATION**

Fall Education Conference
September 21, 2017

Covering the codes (and technical update)

presented by

Mark S. Graham
Vice President, Technical Services
National Roofing Contractors Association (NRCA)

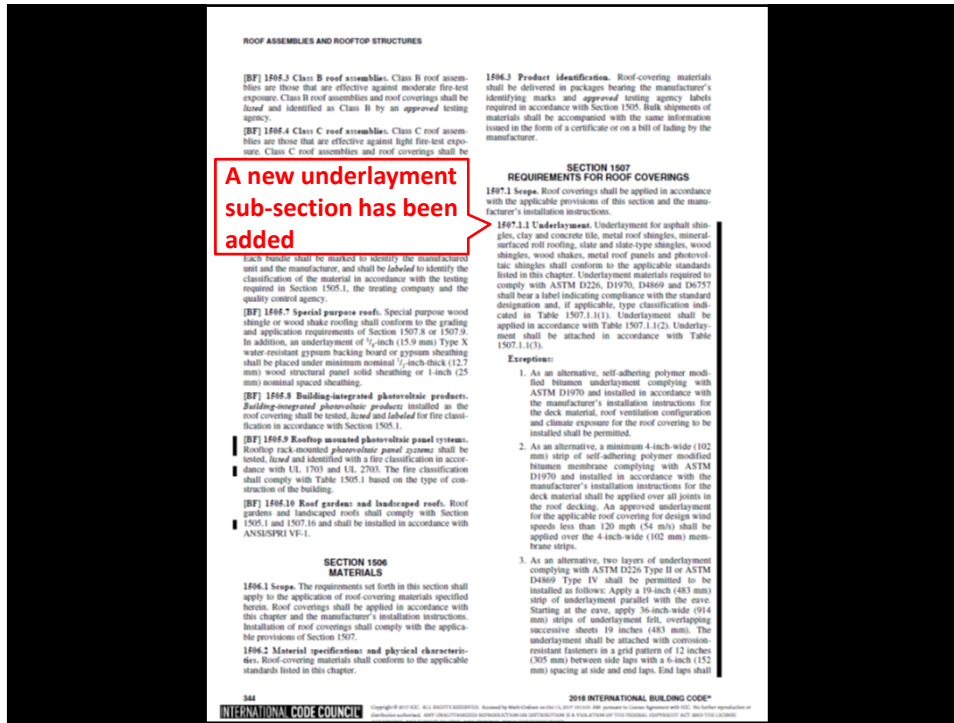


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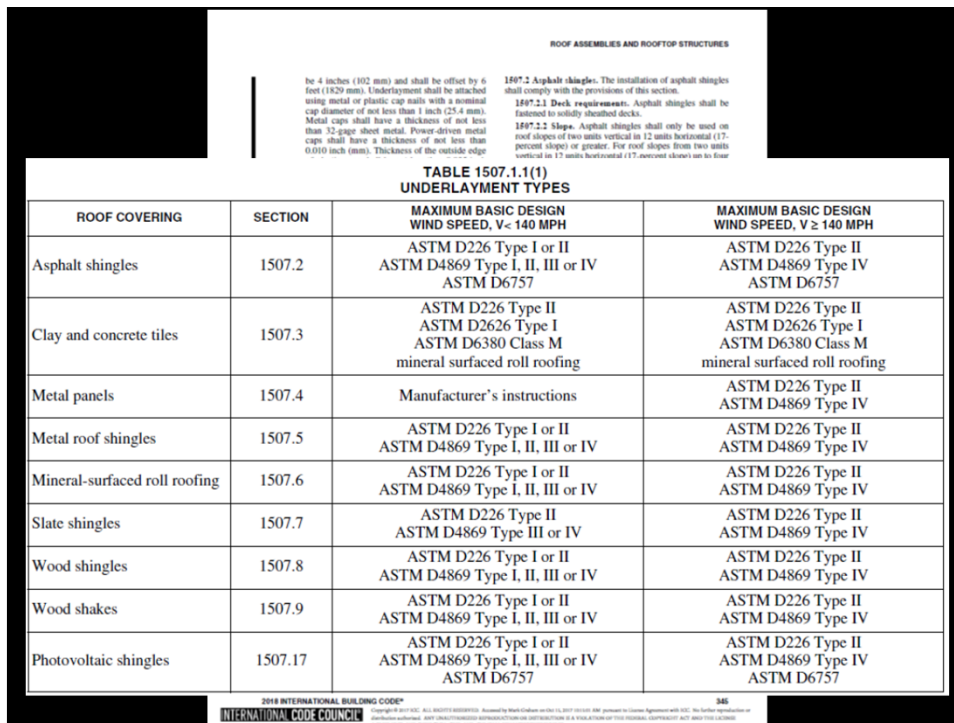
Topics

- 2018 I-code overview
- ASCE 7-16 (wind design)
- Roof drain concerns
- Moisture in concrete roof decks
- Steel roof deck concerns
- FM VSH (hail)
- Attic ventilation
- Questions (and answers)



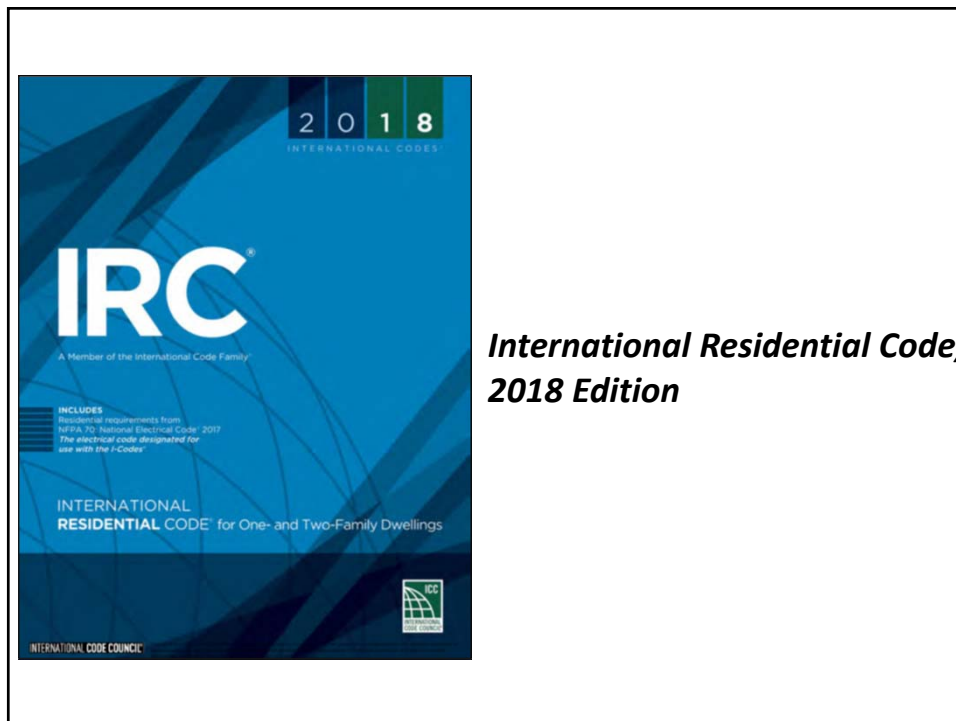
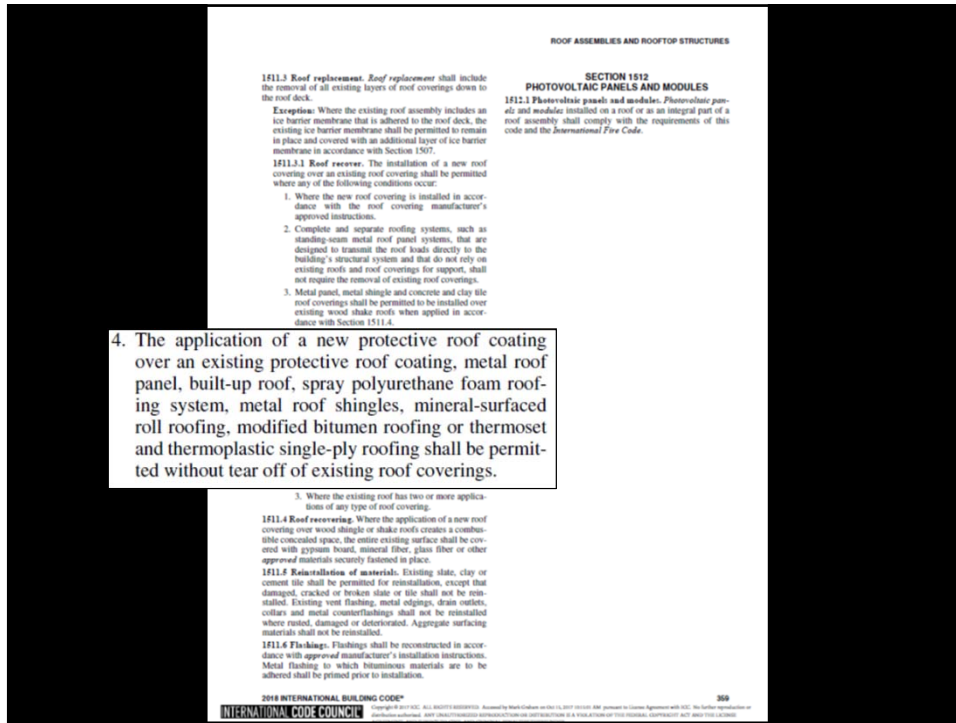


A new underlayment sub-section has been added



| ROOF ASSEMBLIES AND ROOFTOP STRUCTURES | | | | | | | | | | | | | | | | | | | | | | | |
|--|---------|--|--|----------|---------|--|---|----------------|--------|--|--|-------------|--------|--|--|---------------|--------|--|--|-----------------------|---------|--|--|
| TABLE 1507.1.1(2) UNDERLAYMENT APPLICATION | | | | | | | | | | | | | | | | | | | | | | | |
| ROOF COVERING | SECTION | MAXIMUM BASIC DESIGN WIND SPEED, $V < 140$ MPH | MAXIMUM BASIC DESIGN WIND SPEED, $V \geq 140$ MPH | | | | | | | | | | | | | | | | | | | | |
| Asphalt shingles | 1507.2 | <p>For roof slopes from two units vertical in 12 units horizontal (2:12), up to four units vertical in 12 units horizontal (4:12), underlayment shall be two layers applied as follows: Apply a 19-inch strip of underlayment felt parallel to and starting at the eaves. Starting at the eave, apply 36-inch-wide sheets of underlayment, overlapping successive sheets 19 inches. End laps shall be 4 inches and shall be offset by 6 feet. Distortions in the underlayment shall not interfere with the ability of the shingles to seal.</p> <p>For roof slopes of four units vertical in 12 units horizontal (4:12) or greater, underlayment shall be one layer applied as follows: Underlayment shall be applied shingle fashion, parallel to and starting from the eave and lapped 2 inches. Distortions in the underlayment shall not interfere with the ability of the shingles to seal. End laps shall be 4 inches and shall be offset by 6 feet.</p> | Same as Maximum Basic Design Wind Speed, $V < 140$ mph except all laps shall be not less than 4 inches | | | | | | | | | | | | | | | | | | | | |
| <table border="1"> <thead> <tr> <th>COVERING</th> <th>SECTION</th> <th>MAXIMUM BASIC DESIGN WIND SPEED, $V < 140$ MPH</th> <th>MAXIMUM BASIC DESIGN WIND SPEED, $V \geq 140$ MPH</th> </tr> </thead> <tbody> <tr> <td>Slate shingles</td> <td>1507.7</td> <td></td> <td></td> </tr> <tr> <td>Wood shakes</td> <td>1507.8</td> <td></td> <td></td> </tr> <tr> <td>Wood shingles</td> <td>1507.9</td> <td></td> <td></td> </tr> <tr> <td>Photovoltaic shingles</td> <td>1507.17</td> <td></td> <td></td> </tr> </tbody> </table> <p>For 3/8 inch = 25.4 mm, 1 foot = 304.8 mm, 1 mile per hour = 0.447 m/s.</p> | | | | COVERING | SECTION | MAXIMUM BASIC DESIGN WIND SPEED, $V < 140$ MPH | MAXIMUM BASIC DESIGN WIND SPEED, $V \geq 140$ MPH | Slate shingles | 1507.7 | | | Wood shakes | 1507.8 | | | Wood shingles | 1507.9 | | | Photovoltaic shingles | 1507.17 | | |
| COVERING | SECTION | MAXIMUM BASIC DESIGN WIND SPEED, $V < 140$ MPH | MAXIMUM BASIC DESIGN WIND SPEED, $V \geq 140$ MPH | | | | | | | | | | | | | | | | | | | | |
| Slate shingles | 1507.7 | | | | | | | | | | | | | | | | | | | | | | |
| Wood shakes | 1507.8 | | | | | | | | | | | | | | | | | | | | | | |
| Wood shingles | 1507.9 | | | | | | | | | | | | | | | | | | | | | | |
| Photovoltaic shingles | 1507.17 | | | | | | | | | | | | | | | | | | | | | | |

| ROOF ASSEMBLIES AND ROOFTOP STRUCTURES | |
|---|---|
| <p>wood complying with Section 2303.2 for exterior installation.</p> <p>3. Where exterior wall covering panels are used, the panels shall have a flame spread index of 25 or less when tested in the minimum and maximum thicknesses intended for use, with each face tested independently in accordance with ASTM E84 or UL 723. The panels shall be tested in the minimum and maximum thicknesses intended for use in accordance with, and shall comply with the acceptance criteria of, NFPA 285 and shall be installed as tested. Where the panels are tested as part of an exterior wall assembly in accordance with NFPA 285, the panels shall be installed on the face of the mechanical equipment screen supporting structure in the same manner as they were installed on the tested exterior wall assembly.</p> <p>[BG] 1510.6.3 Type V construction. The height of mechanical equipment screens located on the roof decks of buildings of Type V construction, as measured from grade plane to the highest point on the mechanical equipment screen, shall be permitted to exceed the maximum building height allowed for the building by other provisions of this code where complying with any one of the following limitations, provided that the fire separation distance is greater than 5 feet (1524 mm):</p> <ol style="list-style-type: none"> 1. Where the fire separation distance is not less than 20 feet (6096 mm), the height above grade plane of the mechanical equipment screen shall not exceed 4 feet (1219 mm) more than the maximum building height allowed. 2. The mechanical equipment screen shall be constructed of noncombustible materials. 3. The mechanical equipment screen shall be constructed of fire-retardant-treated wood complying with Section 2303.2 for exterior installation. 4. Where the fire separation distance is not less than 20 feet (6096 mm), the mechanical equipment screen shall be constructed of materials having a flame spread index of 25 or less when tested in the minimum and maximum thicknesses intended for use with each face tested independently in accordance with ASTM E84 or UL 723. <p>[BG] 1510.7 Photovoltaic panels and modules. Rooftop-mounted photovoltaic panels and modules shall be designed in accordance with this section.</p> <p>[BG] 1510.7.1 Fire classification. Rooftop-mounted photovoltaic panels and modules shall have the fire classification in accordance with Section 1505.9.</p> <p>[BG] 1510.7.2 Photovoltaic panels and modules. Rooftop-mounted photovoltaic panels and modules shall be listed and labeled in accordance with UL 1703 and shall be installed in accordance with the manufacturer's instructions.</p> <p>[BG] 1510.8 Other rooftop structures. Rooftop structures not regulated by Sections 1510.2 through 1510.7 shall comply with Sections 1510.8.1 through 1510.8.5, as applicable.</p> | <p>[BG] 1510.8.1 Aerial supports. Aerial supports shall be constructed of noncombustible materials.</p> <p>Exception: Aerial supports not greater than 12 feet (3658 mm) in height as measured from the roof deck to the highest point on the aerial supports shall be permitted to be constructed of combustible materials.</p> <p>[BG] 1510.8.2 Bulkheads. Bulkheads used for the shelter of mechanical or electrical equipment or vertical shaft openings in the roof assembly shall comply with Section 1510.2 as penoblasts. Bulkheads used for any other purpose shall be considered as an additional story of the building.</p> <p>[BG] 1510.8.3 Dormers. Dormers shall be of the same type of construction as required for the roof in which such dormers are located or the exterior walls of the building.</p> <p>[BG] 1510.8.4 Fences. Fences and similar structures shall comply with Section 1510.6 as mechanical equipment screens.</p> <p>[BG] 1510.8.5 Flagpoles. Flagpoles and similar structures shall not be required to be constructed of noncombustible materials and shall not be limited in height or number.</p> <p>[BG] 1510.9 Structural fire resistance. The structural frame and roof construction supporting loads imposed upon the roof by any rooftop structure shall comply with the requirements of Table 601. The fire-resistance reduction permitted by Table 601, Note a, shall not apply to roofs containing rooftop structures.</p> <p>SECTION 1511 REROOFING</p> <p>1511.1 General. Materials and methods of application used for recovering or replacing an existing roof covering shall comply with the requirements of Chapter 15.</p> <p>Exceptions:</p> <ol style="list-style-type: none"> 1. Roof replacement or roof removal of existing low-slope roof coverings shall not be required to meet the minimum design slope requirement of one-quarter unit vertical in 12 units horizontal (2-percent slope) in Section 1507 for roofs that provide positive roof drainage. 2. Recovering or replacing an existing roof covering shall not be required to meet the requirement for secondary (emergency overflow) drains or scuppers in Section 1503.4 for roofs that provide for positive roof drainage. For the purposes of this exception, existing secondary drainage or scupper systems required in accordance with this code shall not be removed unless they are replaced by secondary drains or scuppers designed and installed in accordance with Section 1503.4. <p>1511.2 Structural and construction loads. Structural roof components shall be capable of supporting the roof-covering system and the material and equipment loads that will be encountered during installation of the system.</p> |



CHAPTER 9
ROOF ASSEMBLIES

User note:

About this chapter: Chapter 9 addresses the design and construction of roof assemblies. A roof assembly includes the roof deck, substrate or thermal barrier, insulation, vapor retarder and roof covering. This chapter provides the requirement for wind resistance of roof coverings. The types of roof covering materials and installation addressed by Chapter 9 are asphalt shingles, clay and concrete tile, metal roof shingles, manufactured tile roofing, slate and stone-type shingles, wood shakes and shingles, built-up roofs, metal roof panels, modified bitumen roofing, thermoset and thermoplastic single-ply roofing, sprayed polyurethane foam roofing, liquid applied coatings and photovoltaic shingles. Chapter 9 also provides requirements for roof drainage, flashing, above-deck thermal insulation, rooftop-mounted photovoltaic systems and re-roofing or replacing an existing roof covering.

IRC 2018 Ch. 9 changes are similar to those of IBC 2018 Ch. 15 except:

- ASCE 7-10's wind maps apply
- Some rooftop PV reformatting:
 - New Sec. R324-Solar Energy Systems
- New Sec. R905.17 (BIPV applied directly to the roof deck)

Impregnation with chemicals by the full-cell vacuum-pressure process, in accordance with AWPA C1. Each bundle shall be marked to identify the manufacturer and the manufacturer, and shall be labeled to identify the classification of the material in accordance with the testing required in Section R902.1, the testing company and the quality control agency.

R902.3 Building-integrated photovoltaic product. Building-integrated photovoltaic products installed as the roof covering shall be tested, listed and labeled for fire classification in accordance with Section R902.1.

R902.4 Rooftop-mounted photovoltaic panel systems. Rooftop-mounted photovoltaic panel systems installed on or

R903.2.2 Crickets and saddles. A cricket or saddle shall be installed on the ridge side of any chimney or penetration more than 30 inches (762 mm) wide as measured perpendicular to the slope. Cricket or saddle coverings shall be sheet metal or of the same material as the roof covering.


Exception: Unit skylights installed in accordance with Section R308.6 and flashed in accordance with the manufacturer's instructions shall be permitted to be installed without a cricket or saddle.

R903.3 Coping. Parapet walls shall be properly coped with noncombustible, weatherproof materials of a width not less than the thickness of the parapet wall.

2018 INTERNATIONAL RESIDENTIAL CODE®

INTERNATIONAL CODE COUNCIL

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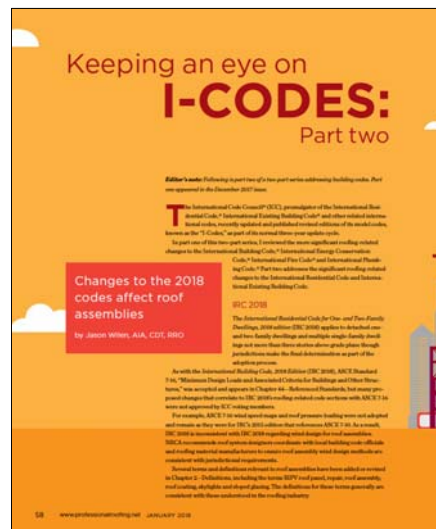
International Energy Conservation Code, 2018 Edition

IECC 2018's roofing-related requirements

- No substantive changes from IECC 2015
 - R-value
 - Roof reflectivity and emissivity
 - Air barriers
- ASHRAE 90.1-16 alternative
 - ASHRAE 90.1-12 referenced in IECC 2015

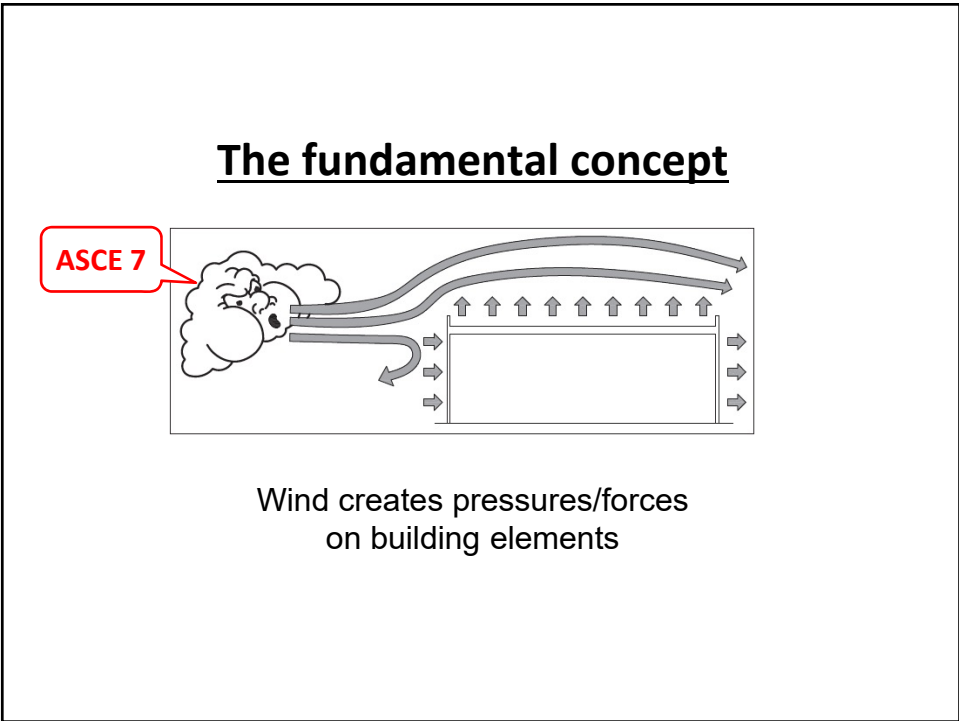


Professional Roofing, December 2017
[Link to access this article](#)



Professional Roofing, January 2018
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ASCE 7-16
Design wind uplift



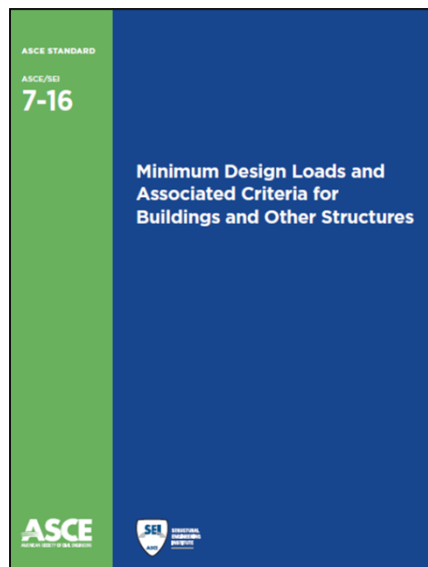
Fundamental concept -- continued

Adhesion or attachment \geq Uplift pressure

FM rating

UL classification \geq ASCE 7

Engineering



American Society of Civil Engineers Standard 7, “Minimum Design Loads and Associated Criteria for Buildings and Other Structures” (ASCE 7-16)

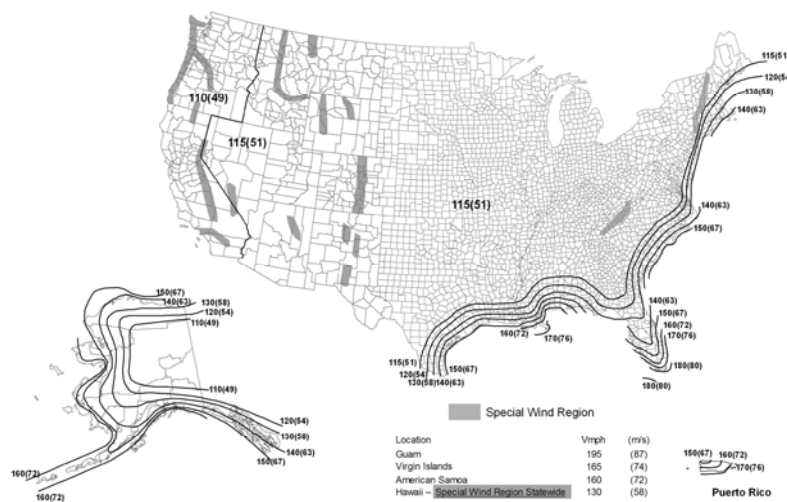
Noteworthy changes in ASCE 7-16

Compared to ASCE 7-10

- Revised basic wind speed map
- Changes (and new) pressure coefficients
- Revised perimeter and corner zones

ASCE 7-10 basic wind speed map

Fig. 1607A-- V_{ult} for Risk Category II Buildings



ASCE 7-16 basic wind speed map

Risk Category II Buildings (MRI = 700 years)

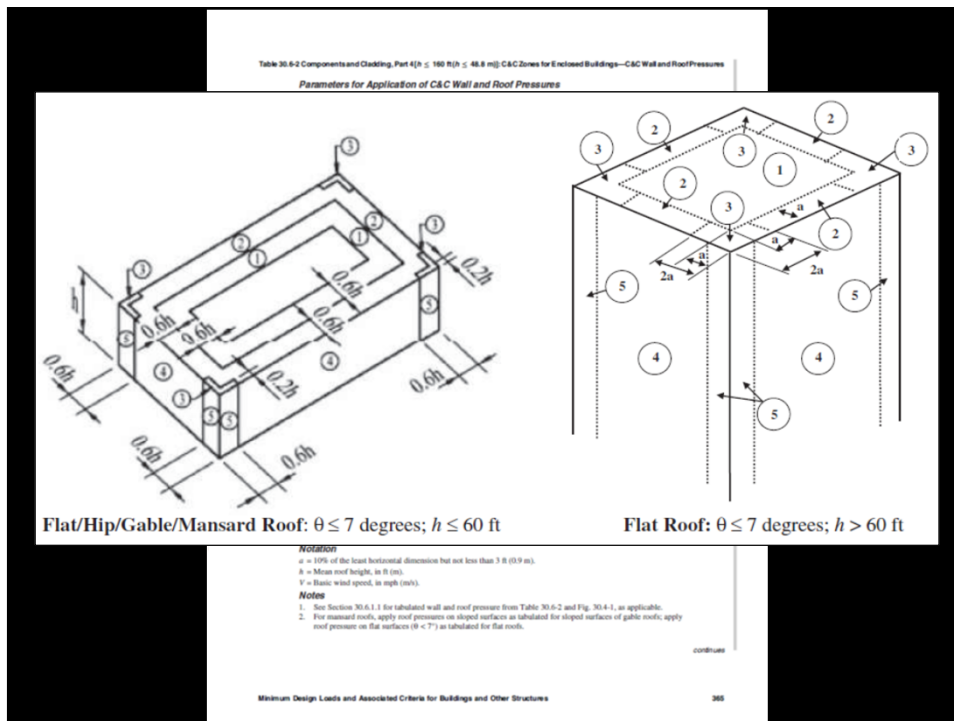
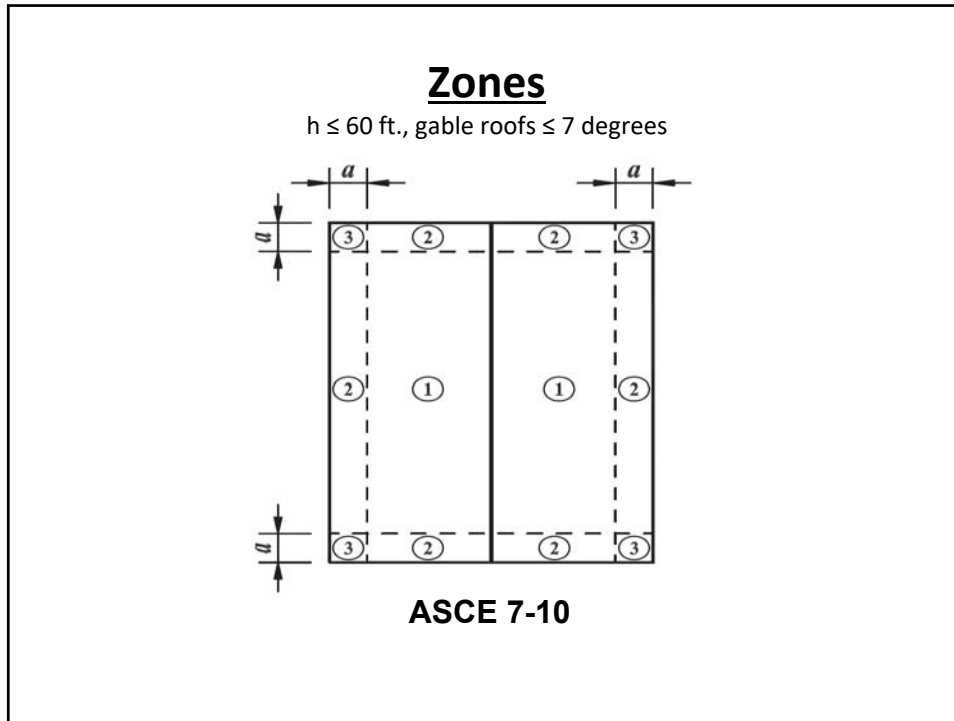
| MRI | | |
|--------------------------|------------|------------|
| Risk Category | ASCE 7-10 | ASCE 7-16 |
| I (Low) | 300 yrs. | 300 yrs. |
| II (not I, II or IV) | 700 yrs. | 700 yrs. |
| Category III (High risk) | 1,700 yrs. | 1,700 yrs. |
| Category IV (Essential) | 1,700 yrs. | 3,000 yrs. |

Selection of the correct Risk Category/map (i.e., wind speed) is essential

Comparing GC_p pressure coefficients

h ≤ 60 ft., gable roofs ≤ 7 degrees

| Zone | ASCE 7-10 | ASCE 7-16 | Change |
|---------------|-----------|-----------|--------|
| 1' | n/a | 0.9 | -10% |
| 1 (field) | -1.0 | -1.7 | +70% |
| 2 (perimeter) | -1.8 | -2.3 | +28% |
| 3 (corners) | -2.8 | -3.2 | +14% |



Noteworthy changes in ASCE 7-16

Compared to ASCE 7-10

- Revised basic wind speed map
- Changes (and new) pressure coefficients
- Revised perimeter and corner zones

While center field pressures may be slightly lower, field, perimeter and corner uplift pressures will generally be greater

How the roofing industry will adapt to ASCE 7-16 remains to be seen....

FM Global has indicated they will update their FM 1-28 to be based on ASCE 7-16 (with modifications) in mid-2019.

An example...

Comparing ASCE 7-05, ASCE 7-10 and ASCE 7-16

Example: A office building (Risk Category II) is located in Omaha, Nebraska. The building is an enclosed structure with a mean roof height of 40 ft. The building is located in an open terrain area that can be categorized as Exposure Category C. An adhered, membrane roof systems is to be installed.

| Document | Basic wind speed (mph) | Design wind pressure (psf) | | | |
|-------------------|------------------------|----------------------------|----------------|--------------------|------------------|
| | | Zone 1' (Center) | Zone 1 (Field) | Zone 2 (Perimeter) | Zone 3 (Corners) |
| ASCE 7-05 | 90 | -- | 21.8 | 36.4 | 54.8 |
| ASCE 7-10 Ult. | 115 | -- | 35.5 | 59.5 | 89.5 |
| ASCE 7-10 ASD | 89 | -- | 21.3 | 35.7 | 53.4 |
| ASCE 7-16 Ult. | 110 | 29.7 | 51.7 | 68.1 | 92.8 |
| ASCE 7-16 ASD | 85 | 17.8 | 31.8 | 40.9 | 55.7 |

This comparison illustrates why it is important for Designers to include wind design loads in their Construction Documents (per IBC Sec. 1603.1)...

...It also illustrates why specifying a wind warranty can create an uneven playing field. Unless the Designer indicates the wind design loads, which design method will the manufacturer use (e.g., in a competitive environment)?



Specifying wind design

Many roof system designers inadequately address wind loads in contract documents
by Mark S. Graham

Specifying wind speed warranties is not a substitute for code-required wind design data

NBCA is receiving an increasing number of reports indicating project drawings and specifications incompletely, inadequately or inaccurately address proper wind design for low-slope membrane roof systems. Some designers, according to reports, only include a specification requirement for the roof system manufacturer to provide a wind warranty. But there are minimum requirements for proper wind design of low-slope membrane roof systems.

Code requirements

Building codes typically provide specific requirements for specifying design wind loads, including wind design data, in contract documents.

The International Building Code, 2012 Edition (IBC, 2012), Chapter 16-Structural Design, Section 1603-Contract Documents, indicates contract documents need to include a roof system's low wind speed design data and any special loads.

Required wind design data includes identifying the ultimate design wind speed, nominal design wind speed, risk category wind exposure and applicable internal pressure coefficients. For component and cladding systems that are not specifically designed by a registered design professional, design wind pressures in terms of psf (pounds per square foot) also are required. Roof systems typically are considered component and cladding systems. Design wind pressures in the field, perimeter and corner regions

of roof areas should be noted in contract documents.

IBC's previous editions include similar contract document requirements.

For new construction projects, design loads more commonly will be identified on structural drawings in the project drawing set. For projects without specific structural drawings, design loads may be provided on architectural drawings or drawing sets or in project specifications.

ANSI/SPRI ES-1

ANSI/SPRI ES-1, "Wind Design Standard for Edge Systems Used with Low-Slope Roofing Systems," which is referenced in IBC 2012, includes two primary document determinations of design wind loads at roof edges (flats, copings) and eaves for membrane loads of copings and flats.

Designers should not simply specify compliance with ANSI/SPRI ES-1 in project specifications; they should determine and clearly include design wind loads at roof edges in contract documents.

IBC 2012 includes in Section 1504.5-Edge Systems for Low-Slope Roof-Design wind loads should be determined using the ultimate design wind speed and IBC 2012's Chapter 16, which is based on ASCE 7-10, "Minimum Design Loads for Buildings and Other Structures."

IBC 2012 references ANSI/SPRI ES-1-03, ANSI/SPRI ES-1-03 is based upon ASCE 7-10, which is not an ultimate design wind speed based method. Therefore, the design wind load determination method contained in ANSI/SPRI ES-1 does not satisfy IBC 2012's requirements for design wind loads at roof edges.

Design wind loads at roof edges should be determined using IBC 2012's Chapter 16 and be clearly noted in contract documents.

Responsibilities

Designers should not place the responsibility for determining roof system or individual component design wind loads on manufacturers, component suppliers or installers, or roofing contractors.

Also, designers' sole reliance on specifying wind speed warranties is not a substitute for site-specific wind design data. Such warranties typically do not address combination of ultimate and nominal design wind speeds, building height, risk category, wind exposure and internal pressure coefficients applicable to the specific building necessary for properly determining roof system design wind loads.

Responsibility for properly determining and clearly identifying wind design data, including design wind loads for roof systems, is required by the building code and is clearly that of roof system designers. Designers may retain a structural engineer or qualified consultant to help them fulfill their design responsibilities.

To help designers determine wind loads for commonly encountered low-slope roof systems, NBCA, the National Roofing Contractors Association and National Roofing Contractors Association have developed and offer a free online application, Roof Wind Designer. Roof Wind Designer is a web application that allows users to determine design wind loads using ASCE 7's, "Minimum Design Loads for Buildings and Other Structures," 2005 or 2010 edition.

Roof Wind Designer is accessible at www.nrcanet.org/roofs.

MARK S. GRAHAM is NBCA's executive vice president of technical services.

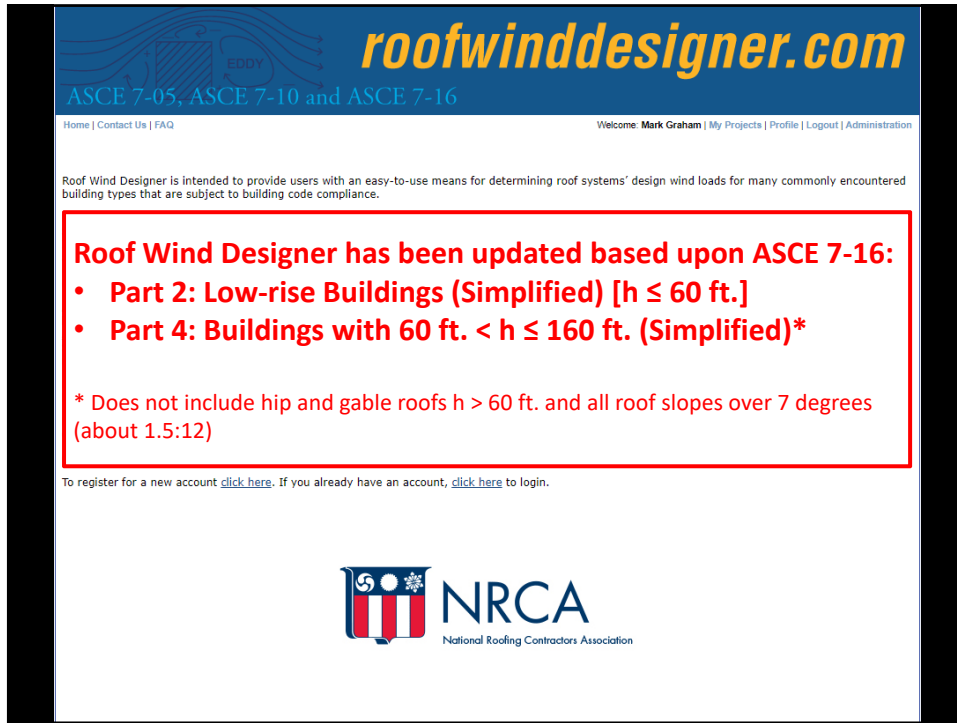
16 www.professionalroofing.net MARCH 2014

[Link](#)

Professional Roofing
March 2014

Fall Education Seminar
Kansas Roofing Association

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The screenshot shows the website **roofwinddesigner.com** with a blue header. Below the header, there is a navigation bar with links for Home, Contact Us, and FAQ. A welcome message for Mark Graham is visible. The main content area features a red-bordered box with the following text:

Roof Wind Designer has been updated based upon ASCE 7-16:

- **Part 2: Low-rise Buildings (Simplified) [h ≤ 60 ft.]**
- **Part 4: Buildings with 60 ft. < h ≤ 160 ft. (Simplified)***

* Does not include hip and gable roofs h > 60 ft. and all roof slopes over 7 degrees (about 1.5:12)

Below the box, there is a registration notice: "To register for a new account [click here](#). If you already have an account, [click here](#) to login."

At the bottom of the page, the NRCA logo is displayed, which includes a shield with a sun, a moon, and a star, and the text "NRCA National Roofing Contractors Association".

Roof drain concerns

Roof drainage

SECTION 1502 ROOF DRAINAGE

[P] 1502.1 General. Design and installation of roof drainage systems shall comply with Section 1502 of this code and Sections 1106 and 1108, as applicable, of the *International Plumbing Code*.

[P] 1502.2 Secondary (emergency overflow) drains or scuppers. Where roof drains are required, secondary (emergency overflow) roof drains or scuppers shall be provided where the roof perimeter construction extends above the roof in such a manner that water will be entrapped if the primary drains allow buildup for any reason. The installation and sizing of secondary emergency overflow drains, leaders and conductors shall comply with Sections 1106 and 1108, as applicable, of the *International Plumbing Code*.

1502.3 Scuppers. Where scuppers are used for secondary (emergency overflow) roof drainage, the quantity, size, location and inlet elevation of the scuppers shall be sized to prevent the depth of ponding water from exceeding that for which the roof was designed as determined by Section 1611.1. Scuppers shall not have an opening dimension of less than 4 inches (102 mm). The flow through the primary system shall not be considered when locating and sizing scuppers.

1502.4 Gutters. Gutters and leaders placed on the outside of buildings, other than Group R-3, private garages and buildings of Type V construction, shall be of noncombustible material or not less than Schedule 40 plastic pipe.

CHAPTER 11 STORM DRAINAGE

Over note:
About this chapter: Detailed roof building must be reviewed and checked to ensure that an appropriate storm water Chapter 11 code flow the design needed exist for the particular area and provide sizing methods for piping and gutter systems to remove the storm water away from the building. Included in this chapter are regulations for piping materials and related drainage systems.

SECTION 1105 ROOF DRAINS

1105.1 General. Roof drains shall be installed in accordance with the manufacturer's instructions. The inside opening for the roof drain shall not be obstructed by the roofing membrane material.

1105.2 Roof drain flow rate. The published roof drain flow rate, based on the head of water above the roof drain, shall be used to size the storm drainage system in accordance with Section 1106. The flow rate used for sizing the storm drainage piping shall be based on the maximum anticipated ponding at the roof drain.

SECTION 1106 SIZE OF CONDUCTORS, LEADERS AND STORM DRAINS

1106.1 General. The size of the vertical conductors and leaders, building storm drains, building storm sewers and any horizontal branches of such drains or sewers shall be based on the 100-year hourly rainfall rate indicated in Figure 1106.1 or on other rainfall rates determined from approved local weather data.



Primary roof drain



Retrofit roof drain insert


NRCA recommendations

Roof drainage concerns

- Be cautious of roof drain issues, particularly in reroofing situations
 - IBC 2009 adds secondary drainage
 - IBC 2015 provides exception
 - IPC 2015 and IPC 2018 changes
- Assure membrane opening is larger than drain outlet/piping opening
- Be cautious of retrofit drain inserts
- Consider proposal/contract language

Moisture in concrete roof decks

NRCA Industry Issue Update, August 2013



INDUSTRY ISSUE UPDATE
NRCA Member Benefit

Moisture in Lightweight Structural Concrete Roof Decks

Concrete Moisture Presents Challenges for Roofing Contractors

NRCA's Technical Services Section is receiving an increasing number of inquiries relating to the application of roof systems over concrete roof decks. These inquiries can be separated into two general questions: When is a concrete roof deck dry enough to apply a roof covering? And why is a roof system applied over a concrete roof deck showing signs of moisture infiltration when the roof covering is leaking?

CONCRETE BASICS
There are three general types of concrete: normal-weight structural concrete, lightweight structural concrete and lightweight insulating concrete.

Normal-weight structural concrete is what most people think of as concrete; it has a density of about 150 pounds per cubic foot (pcf). Lightweight structural concrete has structural load-carrying capabilities similar to normal-weight structural concrete; it has a density in the range of 85 to 120 pcf. Lightweight insulating concrete, which many roofing professionals are familiar with as an insulating, slope-to-drain deck topping, typically has a density in the range from 20 to 40 pcf.

Structural concrete—normal-weight structural concrete and lightweight structural concrete—is produced by mixing large and small aggregates, Portland cement, water and, in some instances, admixtures such as fly ash or various chemical additives. Admixtures can add entrained air to the concrete, accelerate concrete's setting, retain concrete's excess moisture and/or lengthen concrete's finishing time. Use of admixtures typically is not visually identifiable in the field; microscopic analysis usually is needed for post-application identification of admixtures.

The primary difference in the composition of normal-weight structural concrete and lightweight structural concrete is the large aggregate type. Normal-weight structural concrete contains normal-weight aggregates such as stone or crushed gravel, which are dense and typically will absorb no more moisture than about 2 percent by weight. Lightweight structural concrete uses lightweight,

porous aggregates such as expanded shale, which will absorb about 5 to 25 percent moisture by weight. Lightweight aggregate needs to be saturated with moisture—it often soaks in ponds—before mixing. As a result, lightweight structural concrete inherently contains much more water than normal-weight structural concrete.

Lightweight structural concrete is used in roofing-related applications for cast-in-place concrete roof decks using removable form composite roof decks where a metal form deck remains in place and as a deck topping material, such as a concrete topping surface over precast concrete planks or slabs.

Once poured, lightweight structural concrete typically cannot be easily distinguished from normal-weight structural concrete.

Visual identification is possible using magnification, typically a microscope used by a trained technician.

REPORTED PROBLEMS
The problems reported to NRCA associated with lightweight structural concrete roof decks include the following:

- **Moisture accumulation.** Excessive moisture from a concrete deck can be pressure-differential driven into and condensed within a roof system.
- **Adhesive del.** The presence of moisture can result in deterioration of moisture-sensitive roofing materials and adhesive bond loss between adhered material layers.
- **Adhesive issues with some-Armed and One-Adhesive organic compounds.** Excessive moisture can affect adhesive curing and drying rates. Also, moisture can result in adhesive "rewetting," resulting in bond strength loss.
- **Metal fastener corrosion.** Excessive moisture can contribute to and accelerate metal component corrosion, including fastener corrosion.
- **Insulation R-value del.** The accumulation and presence of moisture in most insulation products will result in reduced thermal performance (lower effective R-value).
- **Microbial growth.** The presence of prolonged high-moisture

[Link](#)

Concrete Floors and Moisture, 2nd Edition

Howard M. Kanare, CTL Group

75% internal RH can be achieved:

- Normal weight structural concrete
 - Less than 90 days
- Lightweight structural concrete
 - Almost 6 months

Conclusions

- Concrete roof decks – normal weight and light-weight structural – present challenging moisture-related considerations.
- Further complicated by the use of admixtures and method of finishing.
- NRCA does not support the 28-day drying period or the plastic sheet test


Conclusions - continued

- Roofing contractors can only visually assess the dryness of the concrete's top surface
- Roofing contractors cannot readily assess any remaining free moisture within concrete or its likely release

Roofing contractors are not privy to and may not be knowledgeable about the information necessary to make "...when to roof..." decisions

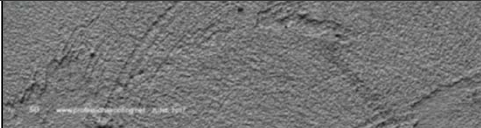
Professional Roofing

June 2017





| ASTM E96 calculated perm | | | | |
|---------------------------------|---------|---------|------------------------|---------|
| Lightweight structural concrete | | | Normal weight concrete | |
| Age | Wet cup | Dry cup | Wet cup | Dry cup |
| 28 days | 1.48 | 0.78 | 3.42 | 1.05 |
| 60 days | 1.45 | 0.47 | 2.03 | 1.13 |

The figure shows results of ASTM E96 water vapor transmission testing. Note the lightweight structural concrete has about half of the permeability of regular weight concrete. Considering lightweight structural concrete arrives with more than twice the evaporable water of regular weight concrete, this explains why lightweight structural concrete retains moisture for so long.



[Link](#)

Moisture on concrete roof decks

Moisture in concrete roof decks
Normal-weight and lightweight structural concrete cause some concern
by Mark S. Givens

NISCA continues to receive a significant number of reports of moisture-related problems associated with concrete roof decks. Following years of background information and NISCA best recommendations for addressing the issue.

What's happened?
The issue of moisture in concrete roof decks is not new. Since 2000, NISCA has received numerous reports of moisture-related problems with roof systems installed on concrete roof decks. Such lightweight structural and normal weight structural concrete. Significant problems include roof system moisture accumulation, excessive heat, excessive steam with water-based and low-volatility organic compound emissions, mold and bacteria growth, moisture to vapor rise and structural damage.

Since the 2005 publication of the NISCA Building and Roofing Manual, Fifth Edition, NISCA no longer considers the plastic sheet use method as a viable assessment to determine a concrete roof deck dry-ness before roof system application. Also, there is little to no correlation between concrete 28-day curing period and the "dryness."

20 www.professionalroofing.net SEPT/NOV 2017

Professional Roofing,
Sept. 2017

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Moisture vapor reduction admixtures (MVRAs)

Some examples:

- Barrier One
- ISE Logik MVRA 9000
- SPG VaporLock

NRCA has still not seen an MVRA perform successfully in concrete roof deck applications

The roofing industry needs to re-think the concept of concrete roof deck “acceptance”

NRLRC's Contract Provisions, Vol. III

“Roofing Contractor’s commencement of the roof installation indicates only that the Roofing Contractor has visually inspected the surface of the roof deck for visible defects and has accepted the surface of the roof deck. Roofing Contractor is not responsible for the construction, structural sufficiency, durability, fastening, moisture content, suitability, or physical properties of the roof deck or other trades’ work or design. Roofing Contractor is not responsible to test or assess moisture content of the deck or substrate.”

Steel roof deck concerns

Professional Roofing
 March 2017
www.professionalroofing.net

Structure magazine
 March 2017
www.structuremag.org

Steel roof deck design

- SDI Design Manual
- AISI S100, “Specifications for the Design of Cold-formed Steel structural Members”
- ANSI/SDI RD1.0-2006, “Standard for Steel Roof Deck”
- ANSI/SDI RD-2010, “Standard for Steel Roof Deck”
- *SDI Roof Deck Design Manual, First Edition* (Nov. 2012)

Steel roof deck design

Wind uplift resistance

- Minimum 30 psf uplift (uniform loading)
- Minimum 45 psf uplift (uniform loading) at roof overhangs

SDI bulletin

2009

STEEL DECK INSTITUTE
Position Statement

ATTACHMENT OF ROOFING MEMBRANES TO STEEL DECK

This document has been published by the Steel Deck Institute (SDI) as a position paper in response to discussions taking place in the roofing community about the screw attachment of roofing membranes to steel deck following line patterns with large spacing. The impetus for this paper is in response to testing carried out by the Special Interest Group for Dynamic Evaluation of Roofing Systems (SDIGERS) at the Institute for Research in Construction, National Research Council of Canada. The mandate of the SDIGERS joint research program is to carry out generic, peer competitive research on the performance of flat roofing systems subjected to dynamic wind loading. The objective is to develop improved roofing systems and design methods.

The SDIGERS research is looking at roofing systems that incorporate wide membrane sheets attached to the steel deck following line patterns spaced as up to 12 ft (3.66 m). While the membrane itself has the performance characteristics to accommodate this size of tributary loading, the existing design methods for steel deck under wind uplift are typically based on the uniform application of the wind suction to the deck. The large majority of the steel roof deck used for commercial buildings in North America is profiled with 1 1/4" DB metal flutes, with the structural supports usually spaced between 5' 0" (1.52 m) and 6' 0" (1.83 m). Under uplift conditions, the attachment of the roofing membrane along lines with large spacing could produce localized loads that can exceed the capacity of the deck, whereas those same loads applied uniformly on the surface of the deck would be acceptable.

The strength of screwed connection between the membrane and the steel deck, as well as the strength of screwed, nailed, or welded attachment of the steel deck to the structural supports can be computed according to the North American Specification for the Design of Cold-Formed Steel Structural Members. These design values are based on the specified minimum mechanical properties (i.e. base steel thickness and yield strength) specified for the steel sheet roof deck, and should be lower than the strength determined by field testing. The use of field test results for properties such as the pull-out strength of a screw into a steel deck needs to recognize that the properties of the steel deck can be higher than the minimum limits required by the steel specifications. Therefore, field testing results must be adjusted accordingly to account for the difference between the actual properties of the deck and the minimum properties of the steel according to the material specification used in design.

The screw fastening of wide roofing membranes (up to 12 ft) and the corresponding spacing of the lines of screws holding the membrane on the deck, will have a very different effect on the deck and structural supports than a membrane that is adhered over its entire surface. The screws will produce a line load along the deck instead of a uniform load of the entire deck surface. The line loads can be perpendicular or parallel to the deck flutes depending on the orientation of the membrane; each condition can have different implications of the loading that is applied to the deck.

If the roofing membrane seam is perpendicular to the flutes of the deck, as illustrated in Figure 1, there are two special conditions that need to be considered:

1. if the membrane seam occurs at the mid-span of the steel deck; and
2. if the membrane seam occurs at the structural support (joist).

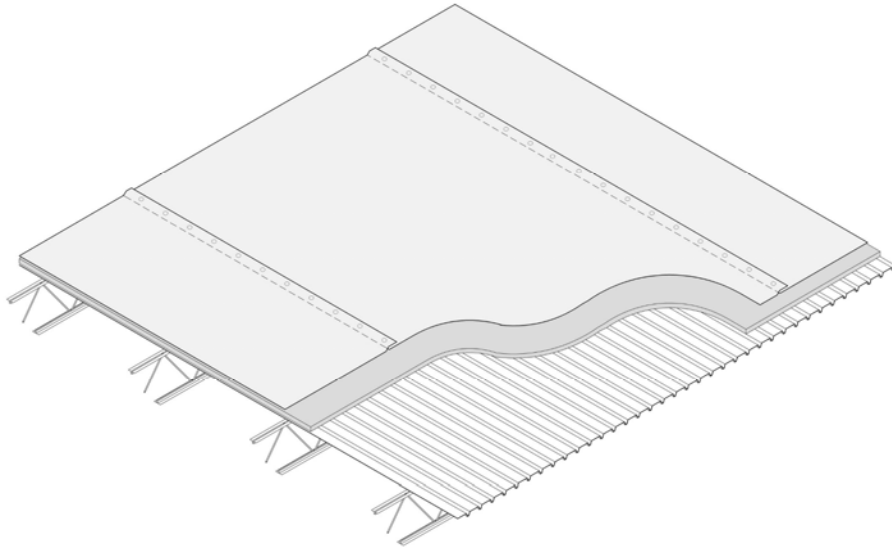
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- Decks designed for joist spacing between 5' and 6' 8" o.c.
- Decks designed for uniform loading
- Seam-fastened single-ply membranes are a concern

Membrane seams across deck flutes

SDI: 3.8 X moment (deck); 2 X load (joists)

Membrane seams in deck flute direction



SDI: 12 X bending moment and shear (deck)

SDI bulletin -- Conclusion

“...SDI does not recommend the use of roofing membranes attached to the steel deck using line patterns with large spacing unless a structural engineer has reviewed the adequacy of the steel deck and the structural supports to resist to wind uplift loads transmitted along the lines of attachment. Those lines of attachment shall only be perpendicular to the flutes of the deck.”

FM's guidelines

- FM 4451, 1978 edition (Steel roof deck)
- FM 4451, June 2012 edition (Steel roof deck)
 - Incorporates AISI S100-07
- FM 4470, June 2012 edition (Roof systems)



Changes reduce some FM classifications

FM 4470 has been revised, resulting in different uplift resistance criteria

by Mark S. Graham

FM Approvals has revised its criteria for determining the uplift resistance of membrane and liquid-applied roof assemblies. Because many roofing professionals rely on FM Approvals' classifications when designing and specifying low-slope roof assemblies, you should be aware of the changes made and their effect on specific roof assembly classifications.

FM 4470

FM 4470, "Approved Standard for Single-Ply, Polymer-Modified Bitumen, Sheet, Built-Up Roof (BTR) and Liquid Applied Roof Assemblies for use in Class 1 and Noncombustible Roof Deck Construction," is the basis for FM Approvals' determination of 1-60, 1-90, 1-120, etc., classifications used for low-slope membrane and liquid-applied roof assemblies.

In June 2012, FM Approvals revised FM 4470; the effective date of the new standard was Dec. 31, 2012. The revisions include adding NFPA 276, "Standard Method for the Test for Determining the Fire Release Rate of Roofing Assemblies with Combustible Above-Deck Roofing Components," to determine combustibility below the roof deck; changes to the conditions of acceptance for wind uplift and fatigue resistance testing; and adding an alternative test method for determining fastener corrosion resistance.

One of the most significant changes to FM 4470 is how roof decks are evaluated. With the revised standard, roof deck characteristics exceed the allowable stresses provided for in AISI S100, "North American Specification for the Design of Cold-Formed Steel Structural Members." The maximum allowable deflection for steel roof decks is based on a 200-pound point load per square foot, and 200-pound point load was used. Also, minimum designs of roof decks now are based on

a minimum 8.7-min-thick (slightly less than 22-gauge), 33-ksi yield strength steel. Previously, minimum 8.75-min-thick (22-gauge) steel complying with the ASTM International specification was used for evaluation.

The method of analyzing attachment of roof decks also has been revised. Check fasteners now are used for fastener "pull-out" (pull strength) of the deck material. Also, some calculations are performed on both roof decks and fastener heads, and the lower of the two values is used as the basis for classification.

FM 4470 also now includes additional provisions allowing for optional testing for dynamic pressure resistance of roof coverings, noncombustible core for roof insulation and solar reflectance of roof surfaces.

All products tested after Dec. 31, 2012, are required to satisfy the new standard's requirements. Products FM Approvals already approved under previous editions of FM 4470 also need to comply with the current edition by the effective date or fabric classification.

What this means

If a specific classified assembly meets its intended use and roof deck, FM Approvals has, upon consultation with the manufacturer, either changed the assembly parameters to compensate for the deck increase or reduced the assembly wind rating to a level where the deck no longer is overstressed. Assembly parameters likely changed include reducing the deck span and/or increasing the deck's roof thickness and/or yield strength (from 33 ksi to 80 ksi).

For assemblies where the wind rating has been reduced, the manufacturer's previous Roof-Near numbers have been withdrawn and new Roof-Near numbers issued to avoid confusion.

If you use the new version of FM 4470 for an allowed roof assembly applied to a 16-in.-thick, 22-gauge steel deck as a 6-foot maximum span, FM Approvals has indicated that classification is limited to 1-105 when using a 33-ksi steel deck and 1-300 when using an 80-ksi steel deck. For non-vented mechanically attached single-ply membrane assemblies, classifications will vary based on assembly parameters and span for new roof spacing, but generally classifications will be noticeably lower than with FM 4470's previous version.

Proceed cautiously

Roof system designers and specifiers need to be aware of FM 4470's revision and its effect on assembly parameters, uplift ratings and Roof-Near numbers for membrane and liquid-applied roof assemblies using steel decks.

For roofing projects designed before the implementation date but that will be installed after the implementation date, classification needs to be sought regarding which version of FM 4470 applies. If the current version applies, changes to the roof assembly specification may be necessary and allow a project team to compensate for the deck increase and specify and roofing contractors to work closely with manufacturers when determining changes to specific assembly parameters, uplift ratings and Roof-Near numbers. ■■■

MARK S. GRAHAM is FMCA's executive associate director of technical services.

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January 2013

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FM's guidelines

- FM 4451, 1978 edition (Steel roof deck)
- FM 4451, June 2012 edition (Steel roof deck)
 - Incorporates AISI S100-07
- FM 4470, June 2012 edition (Roof systems)
- FM 1-29, January/April 2016 (Securement)

FM 1-29 updated

www.fmglobalsdatasheets.com

| FM Global Property Loss Prevention Data Sheets | | 1-29 |
|--|------|------------------------------|
| | | January 2016 |
| | | Version: Revision April 2016 |
| | | Page 1 of 40 |
| ROOF DECK SECUREMENT AND ABOVE-DECK ROOF COMPONENTS | | |
| Note to Insuree of Factory Mutual Insurance Company: Contact the local FM Global office before beginning any roofing work. | | |
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New criteria for steel roof deck uplift:

- Uniformly-distributed loading
- Concentrated loading

An example

Hypothetical analysis using FM 1-29

- Adhered (uniform loading) roof system:
 - 6 ft. joist spacing → Class 165
- Seam-fastened (nonuniform, linear load) roof system:
 - 6 ft. seam spacing → Class 90 (33 ksi steel deck)
 - 9.5 ft. seam spacing → Class 90 (80 ksi steel deck)
 - 6 ft. seam spacing → Class 165 (80 ksi steel deck)

Seam spacing wider than joist spacing is problematic

NRCA's recommendations

Uniformly-loaded vs. non-uniform, linear pattern loaded steel roof decks

New construction:

- Structural engineer awareness of roof system design
 - Note load pattern and steel's yield strength on structural drawings and shop drawings
- Roof system designer awareness of steel roof deck design

NRCA's recommendations – cont.

Uniformly-loaded vs. non-uniform, linear pattern loaded steel roof decks

Reroofing:

- Realize steel roof decks are not likely designed to current SDI, FM Global and FM Approvals' standards
- If steel deck design cannot be verified:
 - Use narrow fastener row/seam spacing (rows/seams \leq joist spacing)
 - Use a uniform uplift loading roof system (BUR, MB, adhered single ply)

Fastener pull-out tests...


There is little correlation between fastener pull-out resistance and a steel roof deck's yield strength and uplift (bending) strength

Although roofing contractors sometimes are given the responsibility of inspecting and accepting steel roof decks to receive a new roof system, determining a roof deck's design adequacy is beyond the expertise of most roofing contractors.

This determination is best made during a project's design phase.

FM's very severe hail (VSH) classifications

RESEARCH+TECH



Understanding FM VSH
 FM has implemented a new impact-resistance classification
 by Mark S. Graham

Commercial and industrial owners FM Global and its code-approved testing agency subsidiary, FM Approvals, have implemented a Very Severe Hail (VSH) impact resistance classification that could affect some of the work you do.

FM Global guidelines
 FM Global traditionally has recommended its insured building owners use moderate hail (MO) or severe hail (SE) classified roof systems for buildings located in areas FM Global considers to be susceptible to moderate or severe hail impacts. FM Loss Prevention Data Sheet 1-14 (FM 1-14), "Hail Damage," provides some clarifying information.


In recent years, the U.S. insurance industry has experienced increases in losses from hail in terms of the number of claims reported and costs of those claims. A majority of the hail damage occurs in rural settings and often results in crop damage.

In the latest revision of FM 1-14, dated October 2014, FM Global has identified a new VSH region, encompassing Oklahoma, Kansas and some southern counties in Texas. FM 1-14 Table 1 identifies the specific southern Texas counties.

To access FM Global Data Sheets, including FM 1-14, "Hail Damage," go to www.professionroofing.net

22 www.professionroofing.net DECEMBER 2017

RESEARCH+TECH



Designing for hail resistance
 Did you know FM Global has updated its hail design guidance?
 by Mark S. Graham

As March, property and building loss insurer FM Global updated its Property Loss Prevention Data Sheet 1-14, "Hail Damage" (FM 1-14). If you work on building interiors FM Global, you should be aware of its latest hail resistance guidelines and the effects they may have on roof system selection and design.

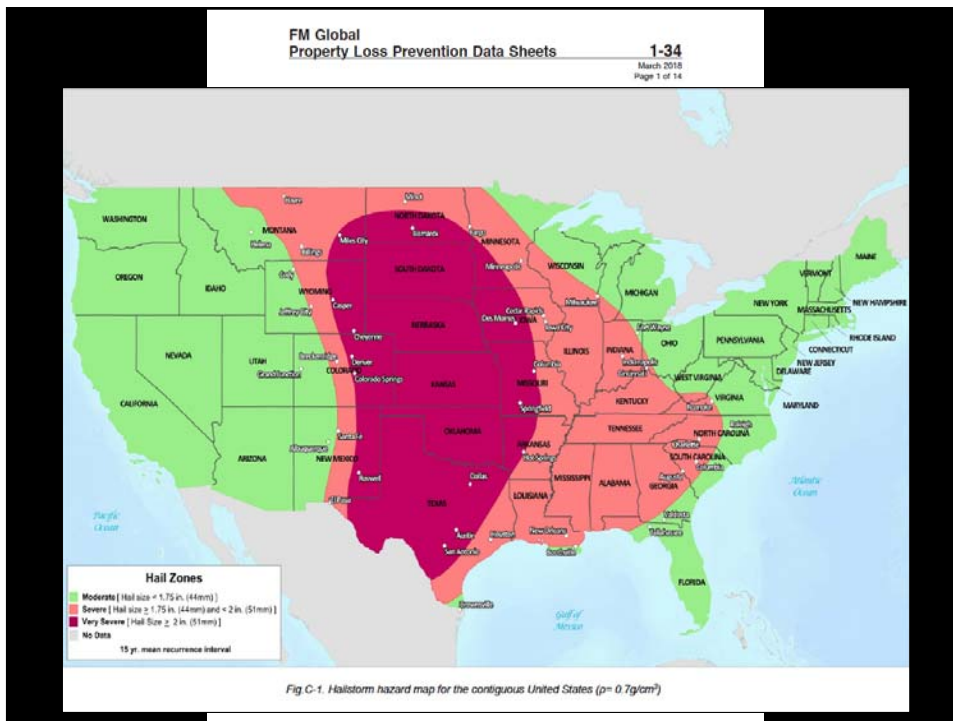
FM 1-14
 FM 1-14 provides loss prevention guidelines to minimize the potential for hail damage to buildings and associated equipment and other outdoor equipment. FM Global intends FM 1-14 and its other Property Loss Prevention Data Sheets to apply to the insured building. However, some designers use the Property Loss Prevention Data Sheets as design guidelines for buildings (and not systems) other than those insured by FM Global.

FM Global certainly believes in a well-thought-out design affecting every aspect of the world that can severely damage buildings' and systems, including HVAC units and skylights. Cooling towers and exposed glass and plastic components of outdoor equipment also can be

20 www.professionroofing.net MAY 2018

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Of the 894,252 roof assemblies in FM's RoofNav,
only 298 have a VSH classification

As of Oct. 4, 2018

Attic ventilation

RESEARCH+TECH



Clearing the air

Considerations for attic ventilation
by Mark S. Graham

Proper attic ventilation can be an important consideration when designing high-performance, energy-efficient roof assemblies. For example, with some asphalt-shingle products, proper attic ventilation may be a warranty requirement. Following is a review of code requirements and ICC-ES guidelines for attic ventilation in energy-efficient roof assemblies.

Code requirements

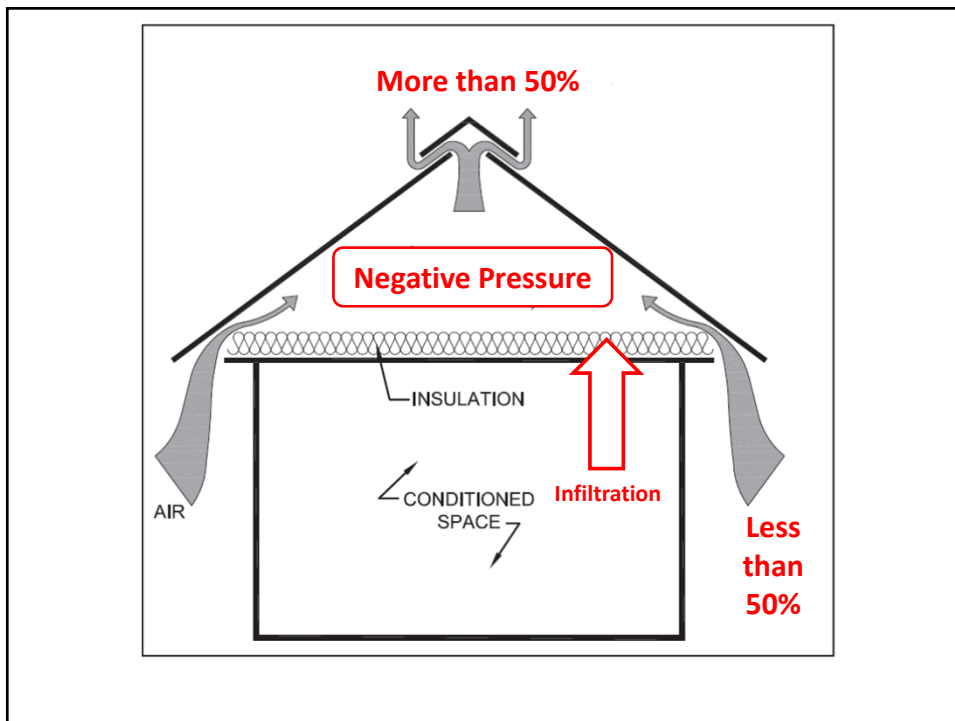
Code requirements for attic ventilation have varied between the International Building Code® (IBC) and International Residential Code® (IRC) and have changed with each edition up to the 2015 editions. Beginning with the IRC and IRC R-900 editions, both codes require the net free ventilating area (NFVA) to be at least a 1:300 ratio of the space being vented. Any blocking or sealing in attic recessed structures with air movement, and an air space of at least 1 inch must be provided between the bottom of the roof deck and any insulation. Vent openings must prohibit the exposure of ribs and studs and be installed according to manufacturer's installation instructions.

20 www.professionalroofing.net JULY 2018

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Be careful not to install excess amounts of ridge vents.... It can have undesirable consequences



April 3-4, 2019
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Recognition of expertise level of field workers

Launch in late-2018

www.nrca.net/NRCA-ProCertification

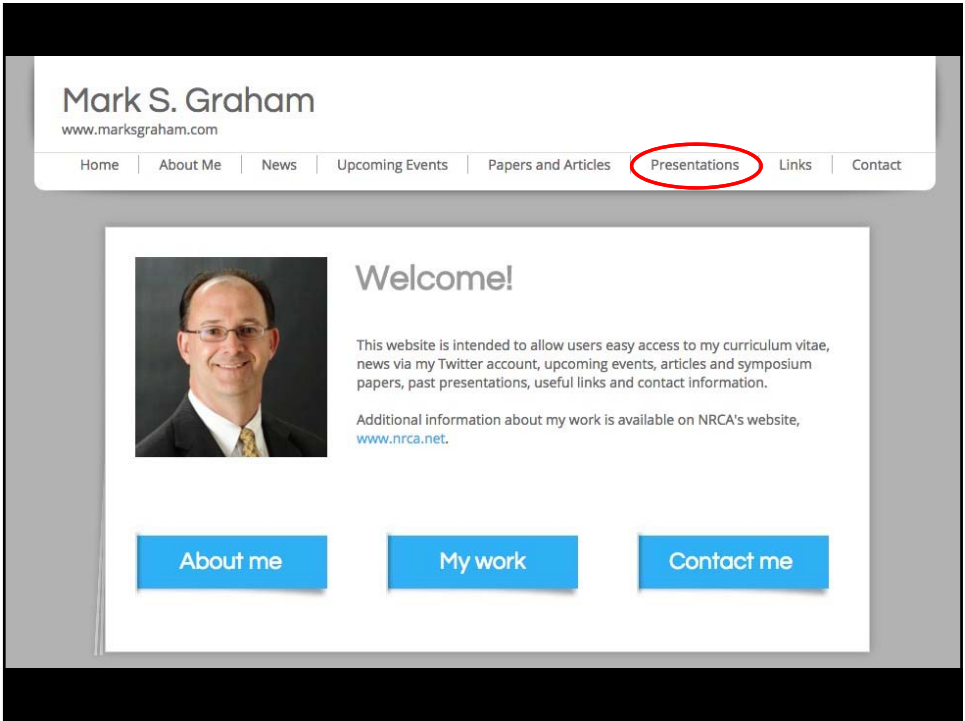
Questions... and other topics



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