



**2025 Winter Technical Session**  
Troy, Michigan – February 27, 2025

**Wind design/ASCE 7-22**

presented by

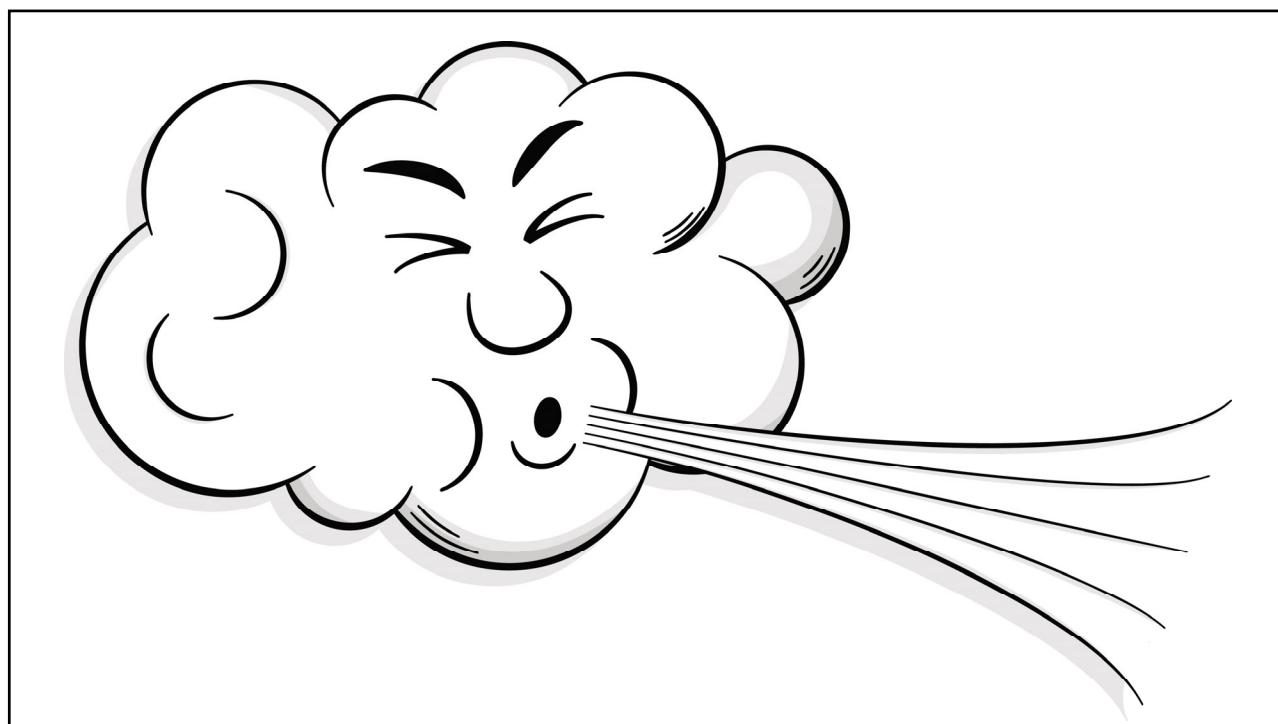
**Mark S. Graham**  
Vice President, Technical Services  
National Roofing Contractors Association (NRCA)



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**Wind design... high winds, hurricanes and tornados**

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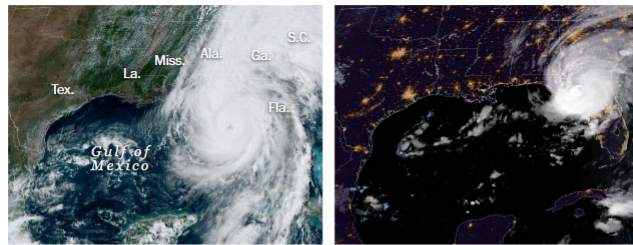
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### Beaufort wind scale

Force	Wind Speed (mph)	Description	Characteristics
0	0-1	Calm	Smoke rises vertically
1	1-3	Light air	Direction of smoke drift
2	4-7	Light breeze	Wind felt of face; leaves rustle
3	8-12	Gentle breeze	Wind extends a light flag
4	13-18	Moderate breeze	Small branches are moved
5	19-24	Fresh breeze	Small trees in leaf begin to sway
6	25-31	Strong breeze	Large branches in motion
7	32-38	Near gale	Whole trees in motion
8	39-46	Gale	Breaks twigs off trees
9	47-54	Severe gale	Slight structural damage occurs
10	55-63	Storm	Trees uprooted; structural damage
11	64-72	Violent storm	Wide-spread damage
12	73-83	Hurricane	See Saffir-Simpson Hurricane Scale

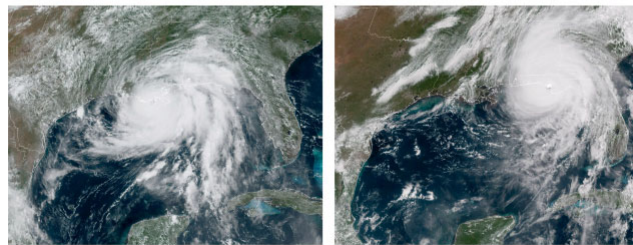
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## Hurricanes



**HELENE** (Sept. 26)  
420 miles wide

**IDALIA** (2023)  
219 miles



**IDA** (2021)  
247 miles

**MICHAEL** (2018)  
272 miles

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## Saffir-Simpson Hurricane Wind Scale

Category	Wind Speed (mph)	Characteristics
1	74-95	Very dangerous winds produce some damage
2	96-110	Extremely dangerous winds will cause extensive damage
3	111-129	Devastating damage will occur
4	130-156	Catastrophic damage will occur
5	157 and higher	Catastrophic damage will occur

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## Tornados



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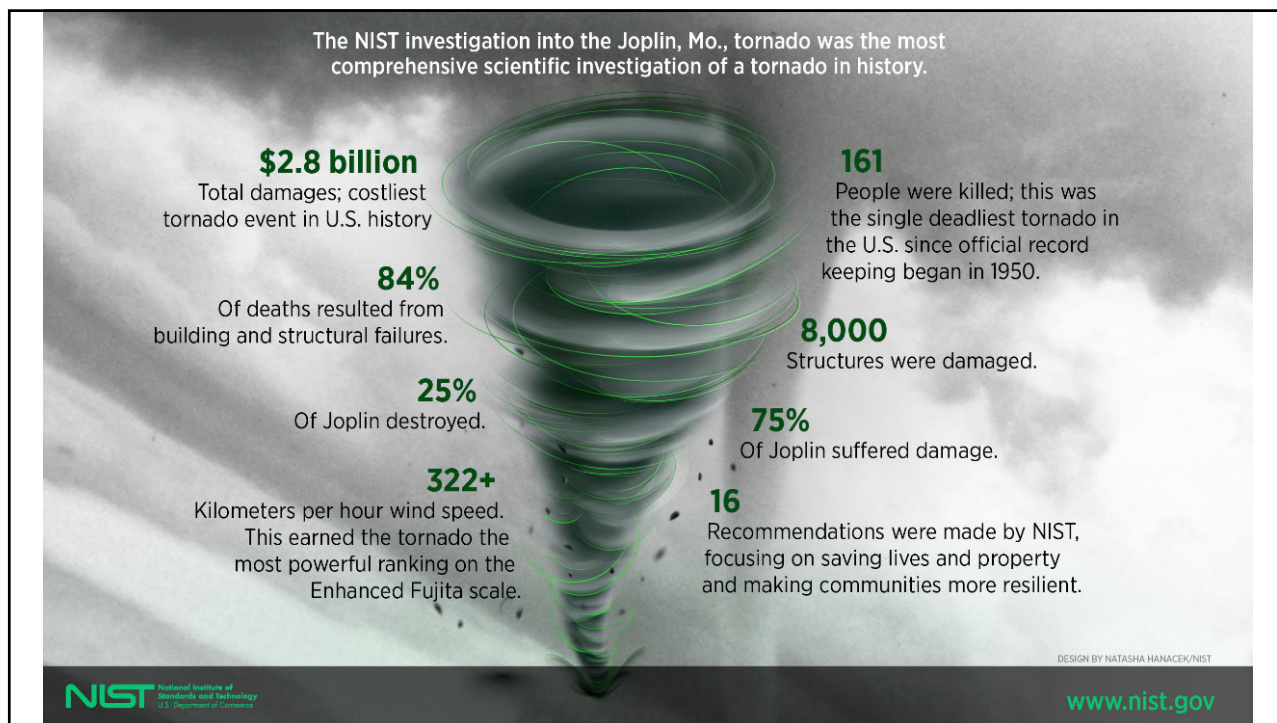
## Enhanced Fujita Scale (EF scale)

Category	Wind Speed (mph)
0	65-85
1	86-110
2	111-135
3	136-165
4	166-200
5	Over 200

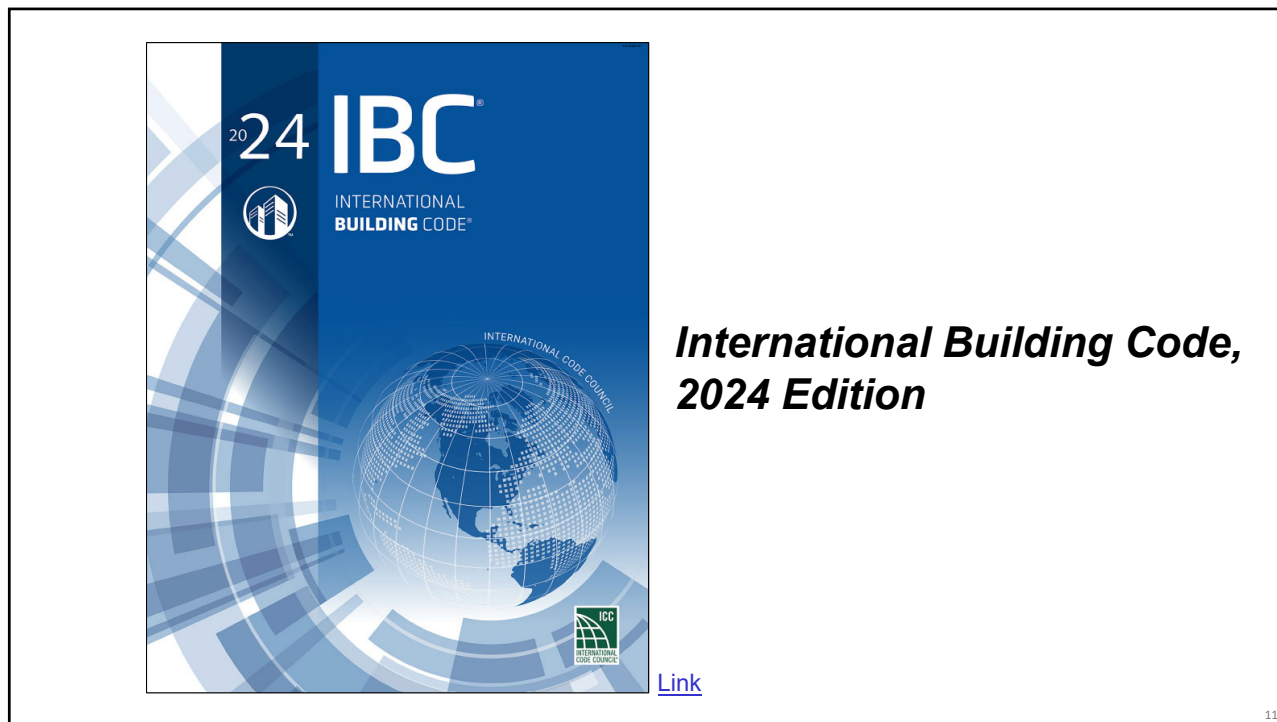
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**STRUCTURAL DESIGN**

6. Design load-bearing values of soils.

7. Rain load data.

**1603.1.1 Floor live load.** The uniformly distributed, concentrated and impact floor live load used in the design shall be indicated for floor areas. Use of live load reduction in accordance with Section 1607.1.3 shall be indicated for each type of live load used in the design.

**1603.1.2 Roof live load.** The roof live load used in the design shall be indicated for roof areas.

**1603.1.3 Roof snow load data.** The ground snow load,  $p_g$ , shall be indicated. In areas where the ground snow load,  $p_g$ , exceeds 15 pounds per square foot (psf) (0.72 kN/m<sup>2</sup>), the following additional information shall also be provided, regardless of whether snow loads govern the design of the roof:

1. Flat-roof snow load,  $p_s$ .
2. Snow exposure factor,  $C_e$ .
3. Risk category.
4. Thermal factor,  $C_t$ .
5. Slope factor(s),  $C_s$ .
6. Drift surcharge load(s),  $p_d$ , where the sum of  $p_d$  and  $p_s$  exceeds 30 psf (1.44 kN/m<sup>2</sup>).
7. Width of snow drift(s),  $w$ .
8. Winter wind parameter for snow drift,  $W_e$ .

**1603.1.4 Wind and tornado design data.** The following information related to wind loads and, where required by Section 1609.5, tornado loads shall be shown, regardless of whether wind or tornado loads govern the design of the lateral force-resisting system of the structure:

1. Basic wind speed,  $V$ , mph (m/s), tornado speed,  $V_T$ , mph (m/s), and allowable stress design wind speed,  $V_{asd}$ , mph (m/s), as determined in accordance with Section 1609.3.1.
2. Risk category.
3. Effective plan area,  $A_e$ , for tornado design in accordance with Chapter 32 of ASCE 7.
4. Wind exposure. Applicable wind direction if more than one wind exposure is utilized.
5. Applicable internal pressure coefficients, and applicable tornado internal pressure coefficients.
6. Design wind pressures and their applicable zones with dimensions to be used for exterior component and cladding materials not specifically designed by the registered design professional responsible for the design of the structure, pounds per square foot (kN/m<sup>2</sup>). Where design for tornado loads is required, the design pressures shown shall be the maximum of wind or tornado pressures.

**1603.1.5 Flood design data.** For buildings located in areas or in part in flood hazard areas as designated in Section 1612.2, the documentation pertaining to design, if required in Section 1612.4, shall be included and the following information, referenced to the datum on the community's Flood Insurance Rate Map (FIRM), shall be shown, regardless of whether flood loads govern the design of the building:

1. Flood design class assigned according to ASCE 24.
2. In flood hazard areas other than coastal high hazard areas or coastal A zones, the elevation of the proposed lowest floor, including the basement.
3. In flood hazard areas other than coastal high hazard areas or coastal A zones, the elevation to which any nonresidential building will be dry floodproofed.
4. In coastal high hazard areas and coastal A zones, the proposed elevation of the bottom of the lowest horizontal structural member of the lowest floor, including the basement.

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STRUCTURAL DESIGN

1608.2.1 Ground snow conversion. Where required, the ground snow loads,  $p_g$ , of Figures 1608.2(1) through 1608.2(4) and Table 1608.2 shall be converted to allowable stress design ground snow loads,  $p_{gsd}$ , using Equation 16-17.

Equation 16-17  $p_{gsd} = 0.75 p_g$

where:  
 $p_{gsd}$  = Allowable stress design ground snow load.

SECTION 1609—WIND LOADS

**1609.1 Applications.** Buildings, structures and parts thereof shall be designed to withstand the minimum wind loads prescribed herein. Decreases in wind loads shall not be made for the effect of shielding by other structures.

**1609.1.1 Determination of wind loads.** Wind loads on every building or structure shall be determined in accordance with Chapters 26 to 30 of ASCE 7. The type of opening protection required, the basic wind speed,  $V$ , and the exposure category for a site is permitted to be determined in accordance with Section 1609 or ASCE 7. Wind shall be assumed to come from any direction and wind pressures shall be assumed to act normal to the surface considered.

**Exceptions:**

1. Subject to the limitations of Section 1609.1.1.1, residential structures using the provisions of applicable Group R-2 and AWC WFCM.
2. Subject to the limitations of Section 1609.1.1.1, residential structures using the provisions of AWC WFCM.
3. Subject to the limitations of Section 1609.1.1.1, residential structures using the provisions of AISI S230.
4. Designs using NAAMM FP 1001.
5. Designs using TIA-222 for antenna-supporting structures and antennas, provided that the horizontal extent of Topographic Category 2 escarpments in Section 2.6.6.2 of TIA-222 shall be 16 times the height of the escarpment.
6. Wind tunnel tests in accordance with ASCE 49 and Sections 31.4 and 31.7 of ASCE 7.
7. Temporary structures complying with Section 3103.6.1.2.

The wind speeds in Figures 1609.3(1) through 1609.3(4) are basic wind speeds,  $V$ , and shall be converted in accordance with Section 1609.3.1 to allowable stress design wind speeds,  $V_{asd}$ , when the provisions of the standards referenced in Exceptions 4 and 5 are used.

IBC 2024 Ch. 35-References Standards identifies ASCE 7-22's edition as being applicable

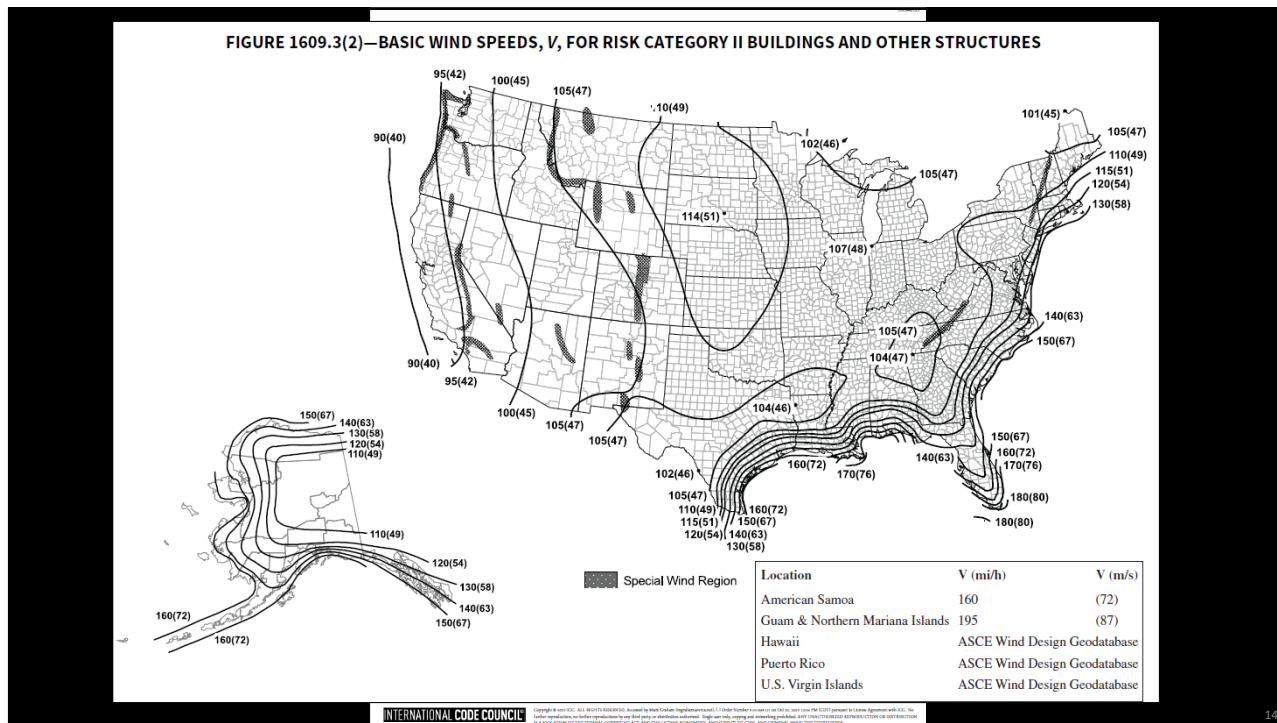
Table 1609.2 with corrosion-resistant attachment hardware provided and anchors permanently installed on the building is permitted for buildings with a mean roof height of 45 feet (13 716 mm) or less where  $V_{sd}$  determined in accordance with Section 1609.3.1 does not exceed 140 mph (63 m/s).

2. Glazing in Risk Category I buildings, including greenhouses that are occupied for growing plants on a production or research basis, without public access shall be permitted to be unprotected.

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**TABLE 1604.5—RISK CATEGORY OF BUILDINGS AND OTHER STRUCTURES**

RISK CATEGORY	NATURE OF OCCUPANCY
I	Buildings and other structures that represent a low hazard to human life in the event of failure, including but not limited to: <ul style="list-style-type: none"> <li>Agricultural facilities.</li> <li>Certain temporary facilities.</li> <li>Minor storage facilities.</li> </ul>
II	Buildings and other structures except those listed in Risk Categories I, III and IV.
III	Buildings and other structures that represent a substantial hazard to human life in the event of failure, including but not limited to: <ul style="list-style-type: none"> <li>Buildings and other structures whose primary occupancy is public assembly with an occupant load greater than 300.</li> <li>Buildings and other structures containing one or more public assembly spaces, each having an occupant load greater than 300 and a cumulative occupant load of these public assembly spaces of greater than 2,500.</li> <li>Buildings and other structures containing Group E or Group I-4 occupancies or combination thereof, with an occupant load greater than 250.</li> <li>Buildings and other structures containing educational occupancies for students above the 12th grade with an occupant load greater than 500.</li> <li>Group I-3, Condition 1 occupancies.</li> <li>Any other occupancy with an occupant load greater than 5,000.<sup>a</sup></li> <li>Power-generating stations with individual power units rated 75 MW<sub>e</sub> (megawatts, alternating current) or greater, water treatment facilities for potable water, wastewater treatment facilities and other public utility facilities not included in Risk Category IV.</li> <li>Buildings and other structures not included in Risk Category IV containing quantities of toxic or explosive materials that:                             <ul style="list-style-type: none"> <li>Exceed maximum allowable quantities per control area as given in Table 307.1(1) or 307.1(2) or per outdoor control area in accordance with the International Fire Code; and</li> <li>Are sufficient to pose a threat to the public if released.<sup>b</sup></li> </ul> </li> </ul>
IV	Buildings and other structures designated as essential facilities and buildings where loss of function represents a substantial hazard to occupants or users, including but not limited to: <ul style="list-style-type: none"> <li>Group I-2, Condition 2 occupancies.</li> <li>Ambulatory care facilities having emergency surgery or emergency treatment facilities.</li> <li>Group I-3 occupancies other than Condition 1.</li> <li>Fire, rescue, ambulance and police stations and emergency vehicle garages</li> <li>Designated earthquake, hurricane or other emergency shelters.</li> <li>Designated emergency preparedness, communications and operations centers and other facilities required for emergency response.</li> <li>Public utility facilities providing power generation, potable water treatment, or wastewater treatment.</li> <li>Power-generating stations and other public utility facilities required as emergency backup facilities for Risk Category IV structures.</li> <li>Buildings and other structures containing quantities of highly toxic materials that:                             <ul style="list-style-type: none"> <li>Exceed maximum allowable quantities per control area as given in Table 307.1(2) or per outdoor control area in accordance with the International Fire Code; and</li> <li>Are sufficient to pose a threat to the public if released.<sup>b</sup></li> </ul> </li> <li>Aviation control towers, air traffic control centers and emergency aircraft hangars.</li> <li>Buildings and other structures having critical national defense functions.</li> <li>Water storage facilities and pump structures required to maintain water pressure for fire suppression.</li> </ul>

a. For purposes of occupant load calculation, occupancies required by Table 1604.5 to use gross floor area calculations shall be permitted to use net floor areas to determine the total occupant load. The floor area for vehicular drive aisles shall be permitted to be excluded in the determination of net floor area in parking garages.

b. Where approved by the building official, the classification of buildings and other structures as Risk Category III or IV based on their quantities of toxic, highly toxic or explosive materials is permitted to be reduced to Risk Category II, provided that it can be demonstrated by a hazard assessment in accordance with Section 1.5.3 of ASCE 7 that a release of the toxic, highly toxic or explosive materials is not sufficient to pose a threat to the public.

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## ASCE Hazard Tool

www.ASCEHazardTool.org

### ASCE HAZARD TOOL

Enter Structure Information

Enter Location  Snap to Address

ADDRESS LAT/LONG FIND ON MAP

2975 E Maple Rd, Troy, Mich X

Requested Data

Standard Version  NEW ASCE/SEI 41 now available

Risk Category  Select Risk  Site Soil Class  Default

Measurements  Customary  SI

Load Types  Select all

Wind  Seismic

Ice  Snow

Rain  Flood

Tsunami  Tornado

All data are per the requirements of published ASCE standards; local requirements may vary.

**ASCE**

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#### REPORT SUMMARY

Site Information

Address:	2975 E Maple Rd, Troy, Michigan, 48083
Elevation:	632 ft (NAVD 88)
Lat:	42.550635
Long:	-83.089123
Standard:	ASCE/SEI 7-22
Risk Category:	II
Soil Class:	Default

Wind

Wind Speed	108 Vmph
10-year MRI	74 Vmph
25-year MRI	80 Vmph
50-year MRI	85 Vmph
100-year MRI	91 Vmph
300-year MRI	101 Vmph
700-year MRI	108 Vmph
1,700-year MRI	115 Vmph
3,000-year MRI	119 Vmph
10,000-year MRI	130 Vmph
100,000-year MRI	149 Vmph
1,000,000-year MRI	169 Vmph

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STRUCTURAL DESIGN

**FIGURE 1609.3(4)—BASIC WIND SPEEDS, V, FOR RISK CATEGORY IV BUILDINGS AND OTHER STRUCTURES**

**1609.3.1 Wind speed conversion.** Where required, the basic wind speeds of Figures 1609.3(1) through 1609.3(4) shall be converted to *allowable stress design* wind speeds,  $V_{ASD}$ , using Table 1609.3.1 or Equation 16-18.

**Equation 16-18**  $V_{ASD} = V\sqrt{0.6}$  i.e.,  $V_{ASD} = V \times 0.78$

where:

$V_{ASD}$  = Allowable stress design wind speed applicable to methods specified in Exceptions 4 and 5 of Section 1609.1.1.

V = Basic wind speeds determined from Figures 1609.3(1) through 1609.3(4).

V	100	110	120	130	140	150	160	170	180	190	200
$V_{ASD}$	78	85	93	101	108	116	124	132	139	147	155

For SI: 1 mile per hour = 0.44 m/s.

a. Linear interpolation is permitted.

b.  $V_{ASD}$  = allowable stress design wind speed applicable to methods specified in Exceptions 1 through 5 of Section 1609.1.1.

c. V = basic wind speeds determined from Figures 1609.3(1) through 1609.3(4).

**1609.4 Exposure category.** For each wind direction considered, an exposure category that adequately reflects the characteristics of ground surface irregularities shall be determined for the site at which the building or structure is to be constructed. Account shall be taken of variations in ground surface roughness that arise from natural topography and vegetation as well as from constructed features.

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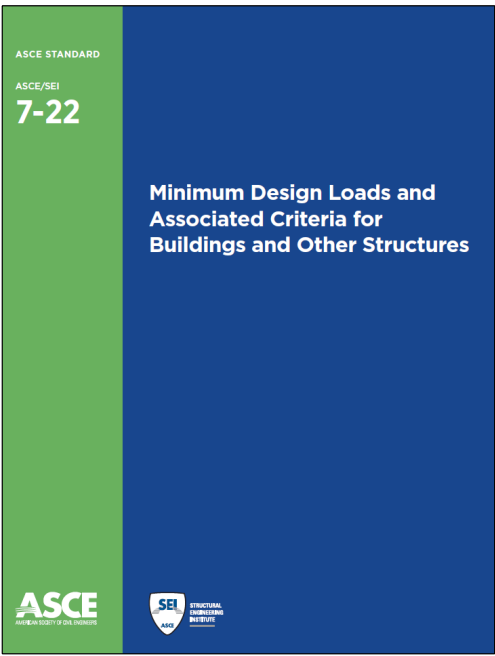
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## ASCE 7-22

- All loads on buildings and structures
- 482 pages + commentary (1046 pages total)
- 32 chapters
- 7 appendixes
- Referenced in IBC 2024 Ch. 16- Wind Design as the basis for wind design

[Link](#)

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**ASCE 7-22 on wind design**

- Ch. 26: Wind loads: General requirements
- Ch. 30: Wind loads: Components and cladding
- Ch. 31: Wind tunnel procedure
- Ch. 32: Tornado loads

*99 pages*

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**CHAPTER 26  
WIND LOADS: GENERAL REQUIREMENTS**

**26.1 PROCEDURES**

**26.1.1 Scope** Buildings and other structures, including the main wind force resisting system (MWFRS) and all components and cladding (C&C) thereof, shall be designed and constructed to resist the wind loads determined in accordance with Chapters 26 through 31.

Risk Category III and IV buildings and other structures, including the MWFRS and all C&C thereof, shall also be designed and constructed to resist tornado loads determined in accordance with Chapter 32, as applicable.

The provisions of this chapter define basic wind parameters for use with other provisions contained in this standard.

26.1.2.2 Components and Cladding Wind loads on C&C on all buildings and other structures shall be designed using one of the following procedures:

1. Analytical Procedures provided in Parts 1 through 5, as appropriate, of Chapter 30; or
2. Wind Tunnel Procedure as specified in Chapter 31.

26.1.3 Performance-Based Procedures Wind design of buildings and other structures using performance-based procedures shall be permitted subject to the approval of the Authority Having Jurisdiction. The performance-based wind design procedures used shall, at a minimum, conform to Section 1.3.1.3.

**26.2 DEFINITIONS**

The following definitions apply to the provisions of Chapters 26 through 31:

**APPROVED:** Acceptable to the Authority Having Jurisdiction.

**ASCE WIND DESIGN GEODATABASE:** The ASCE database (version 2022-1.0) of geocoded wind speed design data.

**User Note:** The ASCE Wind Design Geodatabase of geocoded wind speed design data is available at <https://asce7a-rsdbtool.onlinetool>.

**ATTACHED CANOPY:** A horizontal (maximum slope of 2%) patio cover attached to the building wall at any height; it is different from an overhang, which is an extension of the roof surface.

**BASIC WIND SPEED, V:** Three-second gust speed at 33 ft (10 m) above the ground in Exposure C (see Section 26.7.3) as determined in accordance with Section 26.5.1.

**BUILDING, ELEVATED:** A building supported on structural elements where wind can pass beneath the building.

**BUILDING, ENCLOSED:** A building that has the total area of openings in each wall that receives positive external pressure less than or equal to 4 ft<sup>2</sup> (0.37 m<sup>2</sup>) or 1% of the area of that wall, whichever is smaller. This condition is expressed for each wall by the following equation:

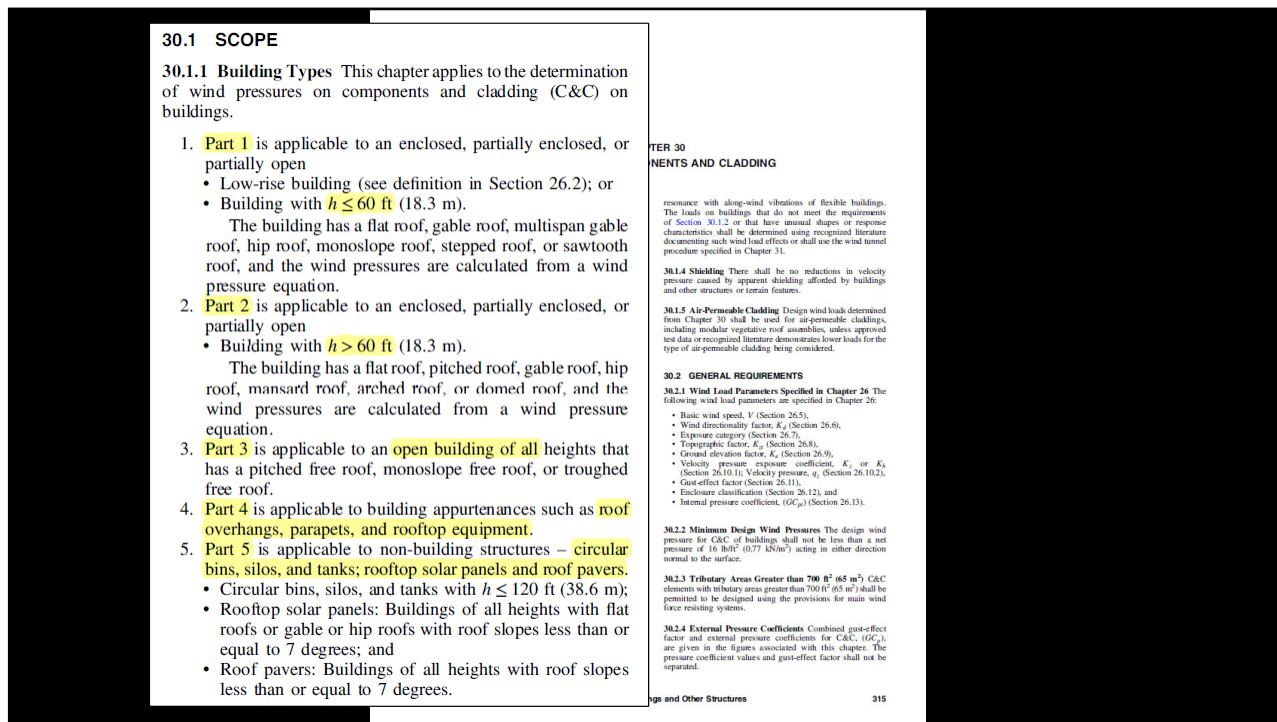
$$A_e < 0.01A_f \text{ or } 4 \text{ ft}^2 (0.37 \text{ m}^2), \text{ whichever is smaller,}$$

where  $A_e$  and  $A_f$  are as defined for Open Buildings.

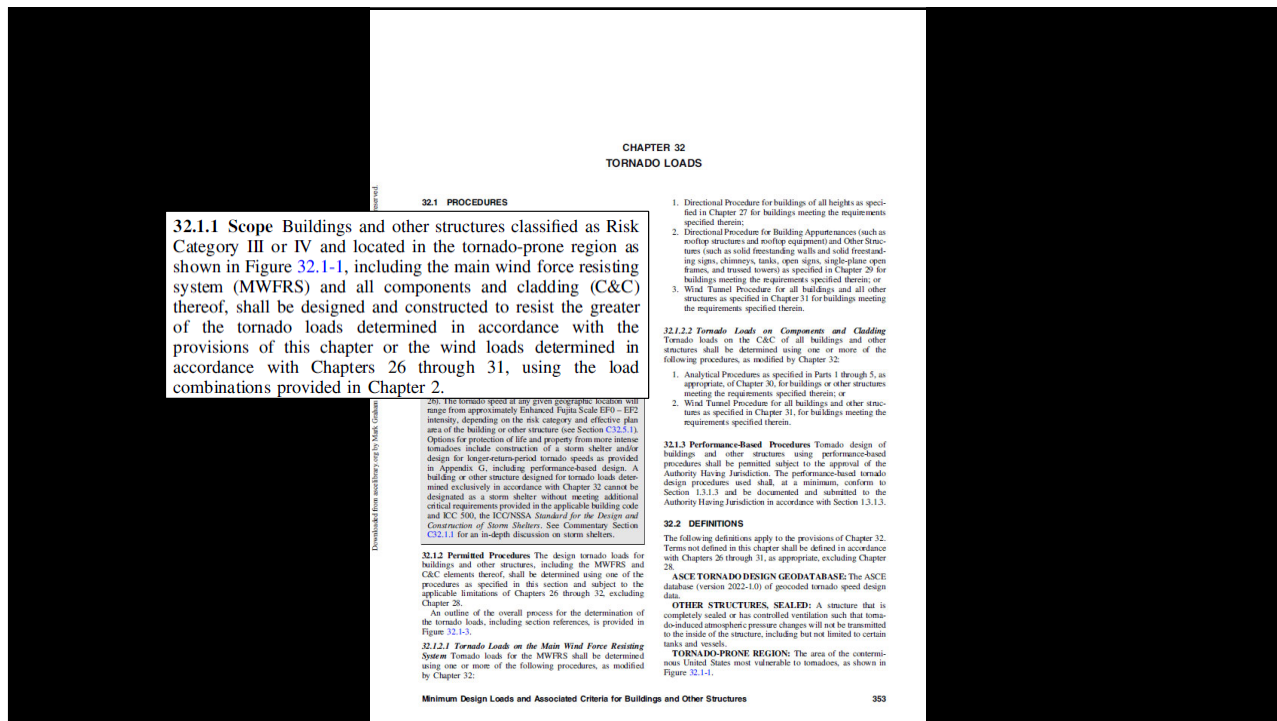
**BUILDING, LOW-RISE:** An enclosed, partially enclosed, or partially open building that complies with the following conditions:

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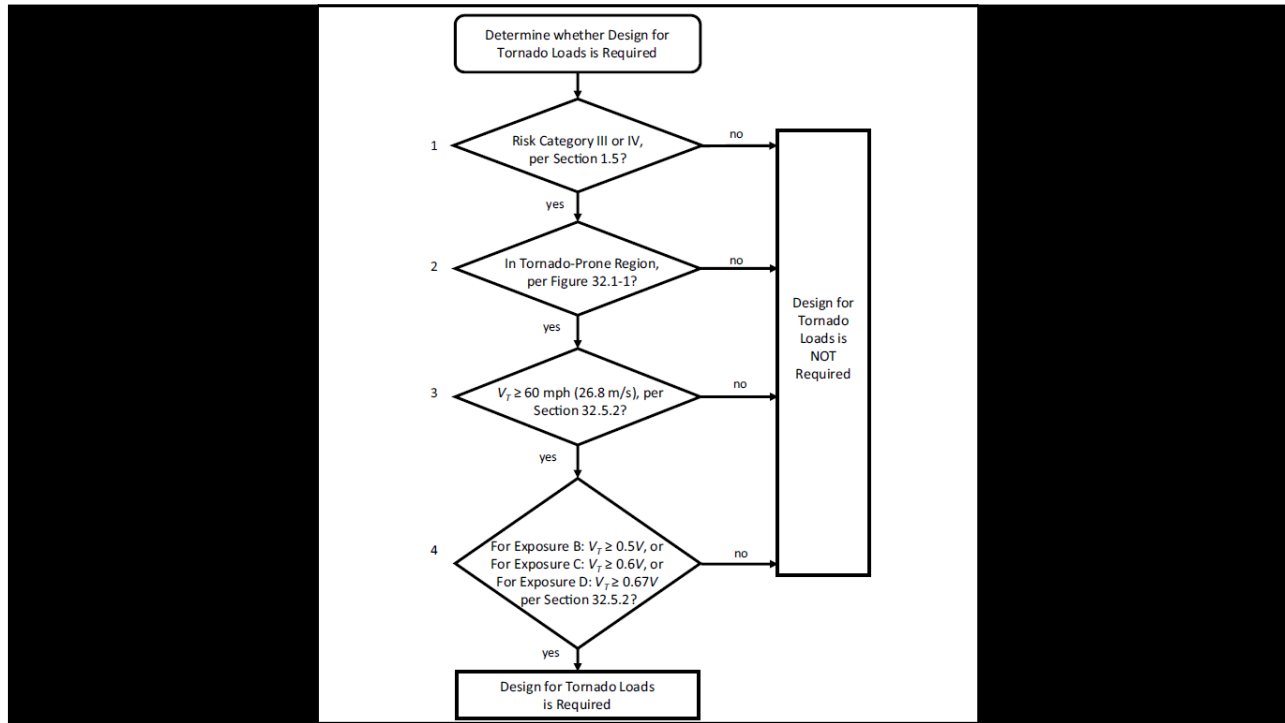
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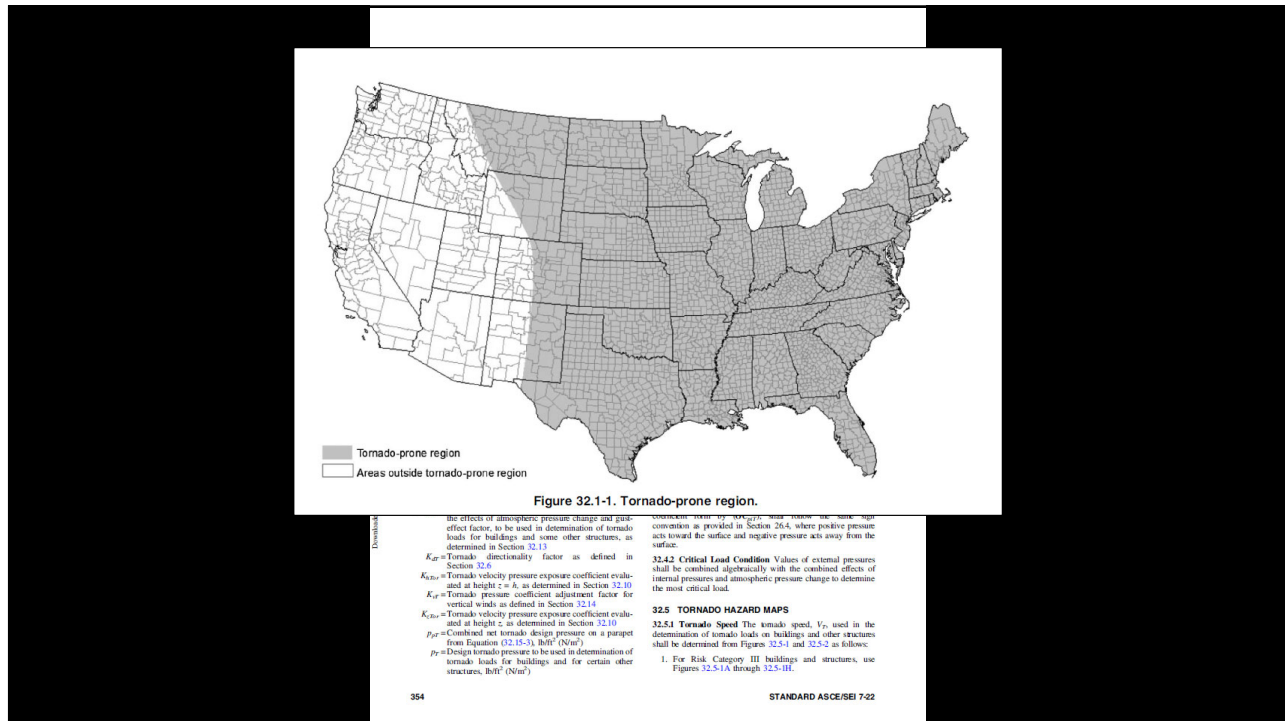
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FEMA/NIST Design Guide

## Design Guide for New Tornado Load Requirements in ASCE 7-22

### “Effective area” for tornado design purposes

**Smallest Convex Polygon Method**

**Simplified Rectangle Method**

Legend --- Building perimeter    Effective plan area

**Figure 5: Effective plan areas for buildings that are not essential facilities (Adapted from ASCE 7, Figure C32.5-1; used with permission from ASCE)**

**Smallest Convex Polygon Method**

**Simplified Rectangle Method**

Legend --- Building perimeter    Effective plan area

**Figure 6: Effective plan area for essential facilities (Adapted from ASCE 7, Figure C32.5-2; used with permission from ASCE)**

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4. Identify, coastal areas, and land boundaries outside the land contour shall use the list tornado speed contour.  
 5. Tornado speed correspond to approximately a 1% probability of exceedance in 50 years (annual exceedance probability = 0.00008, MRF = 1, 700 years).  
 6. Location-specific tornado speed is permitted to be determined using the ASCE Tornado Design Guidelines, available at the ASCE 7 Hazard Tool ([http://dx.doi.org/10.1890/1080-0603\(2014\)36:3;1-4](http://dx.doi.org/10.1890/1080-0603(2014)36:3;1-4)) or approved equivalent.

**Figure 32.5-1G (Continued). Tornado speeds for Risk Category III buildings and other structures, for effective plan area of 1,000,000 ft<sup>2</sup> (92,903 m<sup>2</sup>).**

**Separate tornado speed maps based on Risk Category III and IV, and effective plan areas of 1; 2,000; 10,000; 40,000; 100,000; 250,000; 1,000,000 and 4,000,000 sq. ft.**

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## ASCE Hazard Tool

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ASCE HAZARD TOOL
Measure Basemap Share

**Location**  
Tulsa, Oklahoma, ...

Elevation: 707 ft with respect to North American Vertical Datum of 1988 (NAVD 88)

Lat: 36.155327  
Long: -95.992083

Standard: ASCE/SEI 7-22

Risk Category: III

Soil Class: Default

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**Wind**

115 Vmph Overlay

DETAILS

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**Tornado**

See details for V<sub>1</sub> DETAILS

FULL REPORT SUMMARY

All data are per the requirements of published ASCE standards; local requirements may vary

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Query U.S. Environmental

Tornado Details

Effective Plan Area (ft²)		Tornado Speed (mph)	Tornado Speed (mph)	Tornado Speed (mph)	Tornado Speed (mph)	Tornado Speed (mph)
A <sub>1</sub> = 1	V <sub>1</sub> = 78	V <sub>1</sub> = 123	V <sub>1</sub> = 174	V <sub>1</sub> = 220	V <sub>1</sub> = 256	
A <sub>2</sub> = 2,000	V <sub>1</sub> = 80	V <sub>1</sub> = 125	V <sub>1</sub> = 175	V <sub>1</sub> = 222	V <sub>1</sub> = 259	
A <sub>3</sub> = 10,000	V <sub>1</sub> = 84	V <sub>1</sub> = 128	V <sub>1</sub> = 177	V <sub>1</sub> = 223	V <sub>1</sub> = 261	
A <sub>4</sub> = 40,000	V <sub>1</sub> = 89	V <sub>1</sub> = 132	V <sub>1</sub> = 183	V <sub>1</sub> = 226	V <sub>1</sub> = 265	
A <sub>5</sub> = 100,000	V <sub>1</sub> = 93	V <sub>1</sub> = 136	V <sub>1</sub> = 185	V <sub>1</sub> = 230	V <sub>1</sub> = 267	
A <sub>6</sub> = 250,000	V <sub>1</sub> = 99	V <sub>1</sub> = 142	V <sub>1</sub> = 191	V <sub>1</sub> = 234	V <sub>1</sub> = 270	
A <sub>7</sub> = 1,000,000	V <sub>1</sub> = 111	V <sub>1</sub> = 153	V <sub>1</sub> = 200	V <sub>1</sub> = 241	V <sub>1</sub> = 277	
A <sub>8</sub> = 4,000,000	V <sub>1</sub> = 124	V <sub>1</sub> = 164	V <sub>1</sub> = 211	V <sub>1</sub> = 251	V <sub>1</sub> = 286	

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**32.10 TORNADO VELOCITY PRESSURE**

**32.10.1 Tornado Velocity Pressure Exposure Coefficient** A tornado velocity pressure exposure coefficient,  $K_{z,Tor}$  or  $K_{R,Tor}$ , as applicable, shall be determined from Table 32.10-1.

**32.10.2 Tornado Velocity Pressure** Tornado velocity pressure,  $q_{z,T}$ , evaluated at height  $z$  above ground, shall be determined in accordance with the following equation:

$$q_{z,T} = 0.00256 K_{z,Tor} K_e V_T^2 \text{ (lb/ft}^2\text{); } V_T \text{ in mi/h} \quad (32.10-1)$$

$$q_{z,T} = 0.613 K_{z,Tor} K_e V_T^2 \text{ (N/m}^2\text{); } V_T \text{ in m/s} \quad (32.10-1.SI)$$

where

$K_{z,Tor}$  = Tornado velocity pressure exposure coefficient, see Section 32.10.1;

$K_e$  = Ground elevation factor, see Section 32.9;

$V_T$  = Tornado speed, see Section 32.5; and

$q_{z,T}$  = Tornado velocity pressure at height  $z$ .

The velocity pressure at mean roof height shall be computed as  $q_{h,T} = q_{z,T}$  evaluated from Equation (32.10-1) using  $K_{z,Tor}$  at mean roof height  $h$ .

**32.12 TORNADO ENCLOSURE CLASSIFICATION**

**32.12.1 General** For the purpose of determining internal pressure coefficients for tornadoes, buildings and other structures for which tornado internal pressure coefficients, ( $G_{C,tor}$ ), apply shall have an enclosure classification assigned in accordance with this section. If a building or other structure satisfies both the "open" and "partially enclosed" tornado enclosure classification definitions, it shall be classified as a "partially open" building or other structure.

**32.12.2 Openings** To assign the tornado enclosure classification, the amount of openings in the building envelope shall be determined by taking each wall of the building or other structure, assuming it functions as the windward wall, and summing the total area of openings present with respect to the area of the remaining building envelope. Buildings shall be classified as enclosed, partially enclosed, partially open, or open as defined in Section 26.2. Other structures shall be classified as sealed, as defined in Section 32.2, or enclosed, partially enclosed, partially open, or open as defined in Section 26.2.

Where not required by Section 32.12.3 to protect glazed openings, enclosed buildings and other structures shall either (1) be reevaluated for classification as partially enclosed, with all unprotected glazed openings on each assumed windward wall considered as openings; or (2) be protected in accordance with Section 32.12.3.1.

**32.12.3 Protection of Glazed Openings** Glazed openings shall be protected as specified in this section for Essential Facilities and for buildings and other structures required to maintain the functionality of Essential Facilities.

**32.12.3.1 Protection Requirements for Glazed Openings** Glazing in buildings requiring protection shall be protected with an impact-protective system or shall be impact-resistant glazing. Impact-protective systems shall be either (a) permanently affixed non-operable systems or (b) permanently affixed operable systems capable of being fully deployed from inside the building within five minutes and used in buildings that are staffed 24 hours per day.

Impact-protective systems and impact-resistant glazing shall be subjected to missile tests in accordance with ASTM E1996 using missile level D or E as described in Table 2 of ASTM E1996. Testing to demonstrate compliance with ASTM E1996 shall be in accordance with ASTM E1886. Impact-resistant glazing and impact-protective systems shall comply with the "Enhanced Protection" requirements of Table 1 of ASTM E1996, with tornado speed used in place of basic wind speed for determination of wind zone.

**EXCEPTION:** Other testing methods and/or performance criteria are permitted to be used where approved.

**32.13 TORNADO INTERNAL PRESSURE COEFFICIENTS**

Tornado internal pressure coefficients, ( $G_{C,23}$ ), shall be determined from Table 32.13-1 based on building and other structure enclosure classifications determined in accordance with Section 32.12.1.

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$$F_{rt} = q_{rt} K_{dt} K_{rt} (GC_p) A \quad (32.16-4)$$

$$F_{rt} = q_{rt} K_{dt} K_{rt} (GC_p) A \quad (32.16-4.S1)$$

where

$q_{rt}$  = Tornado velocity pressure from Section 32.10.2 evaluated at mean roof height  $h$ ,  $\text{lb/ft}^2$  ( $\text{N/m}^2$ );

$K_{dt}$  = Tornado directionality factor from Section 32.6;

$K_{rt}$  = Tornado pressure coefficient adjustment factor from Section 32.14;

$(GC_p)$  = Product of external pressure coefficient and gust-effect factor from Section 29.4.1, and

$A$  = Horizontal projected area of rooftop structure or equipment,  $\text{ft}^2$  ( $\text{m}^2$ ).

**32.16.3.3 Roofs of Isolated Circular Bins, Silos, and Tanks** Section 29.4.2.2 shall apply for determination of MWFRS loads on the roofs of isolated circular bins, silos, and tanks, as modified in this section. The net design tornado pressures shall be determined in accordance with the following equation, which replaces Equation (29.4.4):

$$p_r = q_{rt} [G_r K_{dt} K_{rt} C_p - (GC_{piT})] \quad (32.16-5)$$

$$p_r = q_{rt} [G_r K_{dt} K_{rt} C_p - (GC_{piT})] \quad (32.16-5.S1)$$

where

$q_{rt}$  = Tornado velocity pressure from Section 32.10.2 evaluated at mean roof height  $h$ ,  $\text{lb/ft}^2$  ( $\text{N/m}^2$ );

$G_r$  = Tornado gust-effect factor from Section 32.11;

$K_{dt}$  = Tornado directionality factor from Section 32.6;

$K_{rt}$  = Tornado pressure coefficient adjustment factor from Section 32.14;

$C_p$  = External pressure coefficient from Section 29.4.2.2, and

$(GC_{piT})$  = Tornado internal pressure coefficient from Section 32.13.

**32.16.3.4 Rooftop Solar Panels for Buildings of All Heights with Flat Roofs or Gable or Hip Roofs with Slopes Less Than 7 Degrees** Section 29.4.3 shall apply for determination of MWFRS loads on rooftop photovoltaic panels for buildings of all heights with flat roofs or gable or hip roofs with slopes less than 7 degrees, as modified in this section. The design tornado pressure,  $p_r$ , for rooftop photovoltaic panels shall be determined by the following equation, which replaces Equation (29.4.5):

$$p_r = q_{rt} K_{dt} (GC_{pi}) \quad (32.16-6)$$

$$p_r = q_{rt} K_{dt} (GC_{pi}) \quad (32.16-6.S1)$$

where

$q_{rt}$  = Tornado velocity pressure from Section 32.10.2 evaluated at mean roof height  $h$ ,  $\text{lb/ft}^2$  ( $\text{N/m}^2$ );

$K_{dt}$  = Tornado directionality factor from Section 32.6, and

$(GC_{pi})$  = Net pressure coefficient from Section 29.4.3.

**32.16.3.5 Rooftop Solar Panels Parallel to the Roof Surface on Buildings of All Heights and Roof Slopes** Section 29.4.4 shall apply for determination of MWFRS loads on rooftop photovoltaic panels parallel to the roof surface on buildings of all heights and roof slopes as modified in this section. The design tornado pressure,  $p_r$ , for rooftop photovoltaic panels shall be

**32.17.1 Low-Rise Buildings** Section 30.3 shall apply for determination of component and cladding tornado loads on low-rise buildings, as modified in this section. The design tornado pressures,  $p_r$ , on C&C elements in low-rise buildings and buildings with  $h \leq 60$  ft ( $h \leq 18.3$  m) shall be determined in accordance with the following equation, which replaces Equation (30.3-1):

$$p_r = q_{rt} [K_{dt} K_{rt} (GC_p) - (GC_{piT})] \quad (\text{lb/ft}^2) \quad (32.17-1)$$

$$p_r = q_{rt} [K_{dt} K_{rt} (GC_p) - (GC_{piT})] \quad (\text{N/m}^2) \quad (32.17-1.S1)$$

where

$q_{rt}$  = Tornado velocity pressure from Section 32.10.2 evaluated at mean roof height  $h$ ,  $\text{lb/ft}^2$  ( $\text{N/m}^2$ );

$K_{dt}$  = Tornado directionality factor from Section 32.6;

$K_{rt}$  = Tornado pressure coefficient adjustment factor from Section 32.14;

$(GC_p)$  = External pressure coefficient from Section 30.3; and

$(GC_{piT})$  = Tornado internal pressure coefficient from Section 32.13.

**32.17.1.1 Bottom Horizontal Surfaces of Elevated Buildings** Section 30.3.2.1 shall apply for determination of C&C loads on bottom horizontal surfaces of elevated buildings, as modified in this section. The design tornado pressure,  $p_r$ , for the effects of tornado pressure on C&C shall be determined in accordance with Equation (32.17-1), where  $K_{rt} = 1.0$ .

**32.17.2 Buildings with  $h > 60$  ft ( $h > 18.3$  m)** Section 30.4 shall apply for the determination of component and cladding tornado loads on buildings with  $h > 60$  ft ( $h > 18.3$  m), as modified in this section. The design tornado pressures,  $p_r$ , on C&C elements for all buildings with  $h > 60$  ft ( $h > 18.3$  m) shall be determined in accordance with the following equation, which replaces Equation (30.4-1):

$$p_r = q K_{dt} K_{rt} (GC_p) - q_i (GC_{piT}) \quad (\text{lb/ft}^2) \quad (32.17-2)$$

$$p_r = q K_{dt} K_{rt} (GC_p) - q_i (GC_{piT}) \quad (\text{N/m}^2) \quad (32.17-2.S1)$$

where

$q = q_{zT}$  For external pressure on all walls evaluated at height  $z$  above the ground,  $\text{lb/ft}^2$  ( $\text{N/m}^2$ );

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***If the tornado loads are greater than the conventional wind loads, use the tornado loads as the basis for wind design***

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## A wind and tornado design example...

**Hypothetical situation:** A hospital (Risk Category IV) building with a 70 ft. mean roof height 343 square low-slope roof area is located in an urban (Exposure B) Tulsa, OK

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### **Solution:**

#### Wind design:

	Wind Speed	Z <sub>1</sub> (Field)	Z <sub>2</sub> (Perimeter)	Z <sub>3</sub> (Corner)
<b>Ult. method</b>	120 mph	53 psf	77 psf	101 psf
<b>ASD method</b>	93 mph	FM Class 75		

#### Tornado design:

A<sub>e</sub>=40,000 sq. ft.

	Wind Speed	Z <sub>1</sub> (Field)	Z <sub>2</sub> (Perimeter)	Z <sub>3</sub> (Corner)
<b>Ult. method</b>	107 mph	61 psf	81 psf	107 psf
<b>ASD method</b>	--	FM Class 75		

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### Impact of effective area ( $A_e$ )

$A_e=40,000$  sq. ft.

	Wind Speed	$Z_1$ (Field)	$Z_2$ (Perimeter)	$Z_3$ (Corner)
<b>Ult. method</b>	103 mph	61 psf	81 psf	107 psf
<b>ASD method</b>	--	<b>FM Class 75</b>		

$A_e=100,000$  sq. ft.

	Wind Speed	$Z_1$ (Field)	$Z_2$ (Perimeter)	$Z_3$ (Corner)
<b>Ult. method</b>	107 mph	65 psf	87 psf	115 psf
<b>ASD method</b>	--	<b>FM Class 90</b>		

$A_e=250,000$  sq. ft.

	Wind Speed	$Z_1$ (Field)	$Z_2$ (Perimeter)	$Z_3$ (Corner)
<b>Ult. method</b>	113 mph	73 psf	97 psf	128 psf
<b>ASD method</b>	--	<b>FM Class 90</b>		

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### Impact of effective area ( $A_e$ ) - continued

$A_e=1,000,000$  sq. ft.

	Wind Speed	$Z_1$ (Field)	$Z_2$ (Perimeter)	$Z_3$ (Corner)
<b>Ult. method</b>	125 mph	89 psf	119 psf	156 psf
<b>ASD method</b>	--	<b>FM Class 120</b>		

$A_e=4,000,000$  sq. ft.

	Wind Speed	$Z_1$ (Field)	$Z_2$ (Perimeter)	$Z_3$ (Corner)
<b>Ult. method</b>	138 mph	109 psf	145 psf	191 psf
<b>ASD method</b>	--	<b>FM Class 135</b>		

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*While ASCE 7-22's wind load provisions are relatively manageable, the tornado provisions, where applicable, can get rather complex.*

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## Roof Wind Designer

www.roofwinddesigner.com



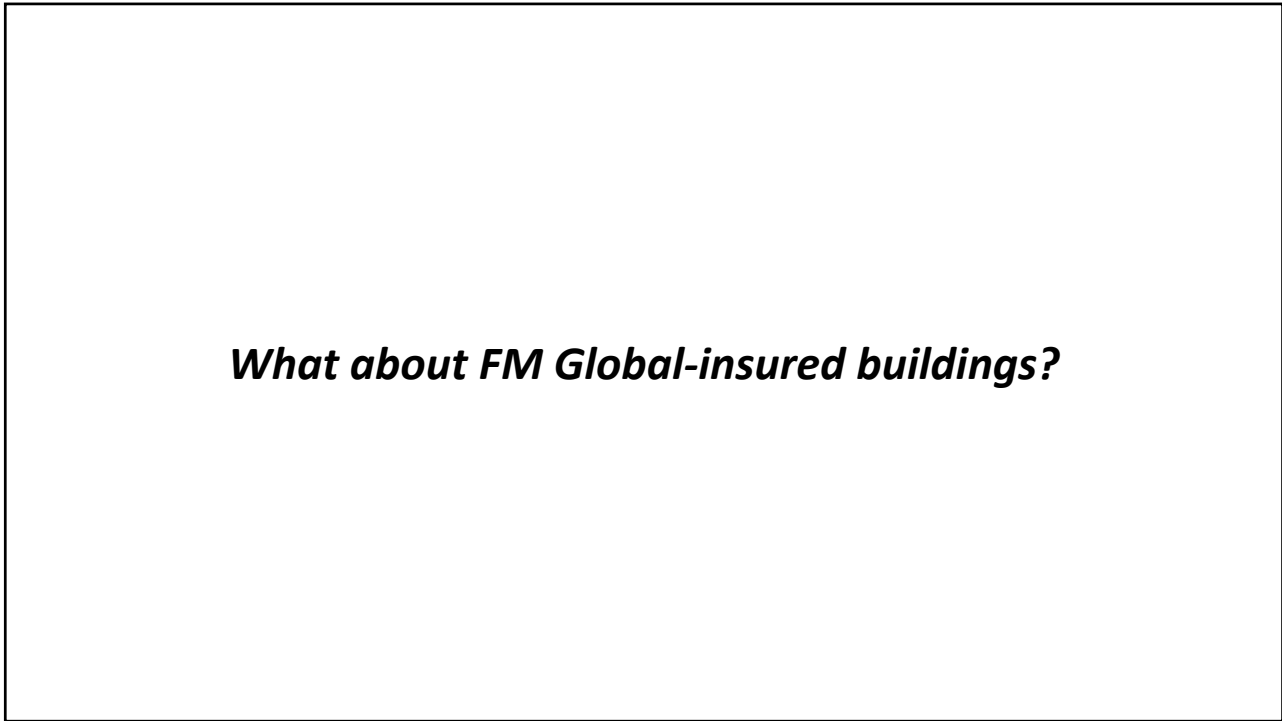
**Tornado design has been added to Roof Wind Designer**

Roof Wind Designer is intended to provide users with an easy-to-use means for determining roof systems' design wind loads for many commonly encountered building types that are subject to building code compliance.

Design-wind loads are derived using the American Society of Civil Engineers (ASCE) Standard ASCE 7, "Minimum Design Loads for Buildings and Other Structures." This standard is a widely recognized consensus standard and is referenced in and serves as the technical basis for wind load determination in the International Building Code and NFPA 5000: Building Construction and Safety Code. Roof Wind Designer allows users to choose between ASCE 7's 2005, 2010, 2016, and 2022 editions. Roof Wind Designer uses ASCE 7-05's Method 1—Simplified Method, ASCE 7-10's Envelope Procedure, Part 2: Low-rise Buildings (Simplified) of Chapter 30, ASCE 7-16's Envelope Procedure, Part 2: Low-rise Buildings (Simplified) of Chapter 30, and Part 4: Buildings with 60ft < h ≤ 160ft (Simplified), and ASCE 7-22's Part 1: Low-rise Buildings, Part 2: Buildings with h > 60 ft [(h > 18.3 m)], and Part 4: Building appurtenances, rooftop structures and equipment. [A more detailed explanation of ASCE 7's four editions.](#)

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**What about FM Global-insured buildings?**

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### FM 1-28, “Wind design”

- Intended to apply to FM Global-insured buildings
- ASD basic wind speed maps and design method
- Some ultimate design concepts (e.g., zones)
- Importance Factor = 1.15
- Tornado provisions added

[Link](#)

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**WIND DESIGN**

**INSUREDS OF FM GLOBAL SHOULD CONTACT THEIR LOCAL FM GLOBAL OFFICE BEFORE BEGINNING ANY ROOFING WORK.**

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**1.1 Changes**

**January 2024. Interim revision. The following changes were made:**

A. The tornado guidance formerly in Appendix D has been transferred to new Sections 2.11 and 3.12, and to existing Section 4.2. All tables, figures and equations have been re-numbered to the new sections. Appendix D has been deleted in its entirety.

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**Legend**

- Area with wind speed  $\geq 140$  mph where tornado design is recommended.
- Area with wind speed  $< 140$  mph where tornado design may be defensible.

Map details: Shows the contiguous United States with state boundaries. Major cities like Chicago, St. Louis, Kansas City, Dallas, Houston, and New York are marked. Wind speed contours are shown as red lines with numerical values. A large orange-shaded area in the central US indicates wind speeds  $\geq 140$  mph. A scale bar at the bottom right shows 0, 250, and 500 miles. A north arrow is also present.

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## Tornado design recommendations

FM 1-28, Sec. 2.11-Tornados

- Assume “partially enclosed” and Exposure C
- Avoid the use of windows
  - When windows are provided, use FM 4350 Level D or E impact-resistant glazing
- Limit other exterior wall openings (e.g., doors)
  - Doors should open outward and have positive latching
- Do not use aggregate on roofs
- Consider full-time QAO during exterior wall and roof application

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### 3.12.4.5 Design Wind Speeds and Wind Pressures

The guidance in this document is primarily for locations on the map in Figure 2.11.1 with wind speeds of 140 mph (62 m/s) and greater. If desired by the client or account team, design guidance can be given for locations on the map with wind speeds less than 140 mph (62 m/s).

**Note:** The cost increase to change from a 90 mph (40 m/s) design wind speed (as is the case with the majority of the central United States) to a higher tornado wind design will vary, depending on geography, the specific design criteria, percentage of windows, etc. Increased construction costs for components and cladding are expected in areas not normally designed for increased wind speeds. This cost increase could be as high as 50%.

Similar to what occurs with hurricanes, most tornado damage is much greater to the building envelope than to the building frame. Using an importance factor of 1.15 (based on ASCE 7-05), some larger structures designed for more typical code-required wind speeds ( $\geq 90$  mph [40 m/s]), have experienced considerable damage to the building envelope, yet limited damage to the structural frame. One cost-effective approach would be to provide a limited increase in design strength for the building frame, but a considerable increase in resistance for the building envelope.

$C_{pe}$  = External pressure coefficient (see Section 3.2.2, Table 3.2.4.1-2 and reference tables and figures)  
 $C_{pi}$  = Tornado Internal pressure coefficient (use +/- 0.55 for partially enclosed)  
 Since the value of  $p_s$  is based off of an ultimate 10,000-year MRI wind speed, convert to an allowable/design pressure by multiplying by 0.6. For plain review/new construction, a safety factor of 2.0 should be applied.

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***FM Global's tornado design provisions are more stringent than IBC 2024's and ASCE 7-22's***

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**Some useful references**  
Tornado design

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FEMA/NIST Design Guide

## Design Guide for New Tornado Load Requirements in ASCE 7-22

This instructional guidance is for design professionals and building officials to help them determine when a building or other structure is required to be designed to minimum tornado loads and how to calculate design tornado forces. This guide is in accordance with the updated requirements of the American Society of Civil Engineers (ASCE) / Structural Engineering Institute (SEI) standard ASCE 7-22, *Minimum Design Loads and Associated Criteria for Buildings and Other Structures*.<sup>1</sup>


This Design Guide is intended for users with a basic understanding of ASCE 7 and who know how to determine wind loads using ASCE 7 methodology, as presented in Chapters 26 through 31.

### Introduction and Background

Tornadoes have historically killed more people in the United States than hurricanes and earthquakes combined (NWS, 2020; USGS, 2015). According to the Insurance Information Institute, Inc. (2020), the average annual insured catastrophe losses for events involving tornadoes exceeded those for both hurricanes and tropical storms combined, for the period of 1997-2016. The 2011 Joplin tornado disaster was the deadliest and costliest tornado in the U.S. since 1950 and was one of the primary drivers for the addition of tornado load provisions in ASCE 7 (NIST, 2022). With the publication of ASCE 7-22 (ASCE, 2021), tornado load requirements are now considered as a minimum design load in conventional building design when buildings are located in tornado-prone areas. The new ASCE 7 tornado load provisions do not apply to storm shelters or safe rooms. The ASCE 7 tornado load requirements will be included in the 2024 International Building Code (IBC), the 2024 National Fire Protection Association (NFPA) 5000 Building Construction and Safety Code, and the 2023 Florida Building Code. The adoption of the ASCE 7 tornado load provisions by the State of Florida is an example of local Authorities Having Jurisdiction incorporating the most current design guidance prior to their inclusion in the model building codes.

Storm shelters and safe rooms are specifically designed for life safety protection during the most extreme wind events and require more extreme design hazard intensities than conventional buildings. Buildings and other structures designed per Chapter 32 of ASCE 7 do not meet the requirements for storm shelters or safe rooms.

<sup>1</sup> The references to ASCE 7 within the design guide represent references to ASCE 7-22.

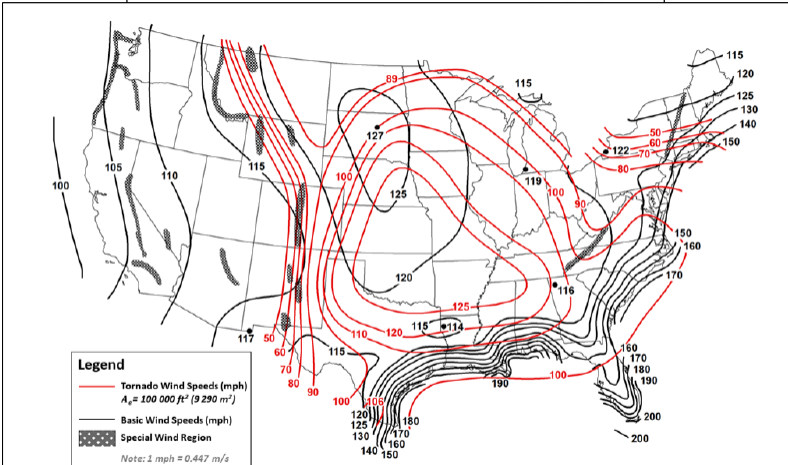


January 2023 - 1 [Link](#)

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### NIST Technical Note 2214

## Economic Analysis of ASCE 7-22 Tornado Load Requirements



Basic wind speeds shown are based on Risk Category IV

[Link](#)

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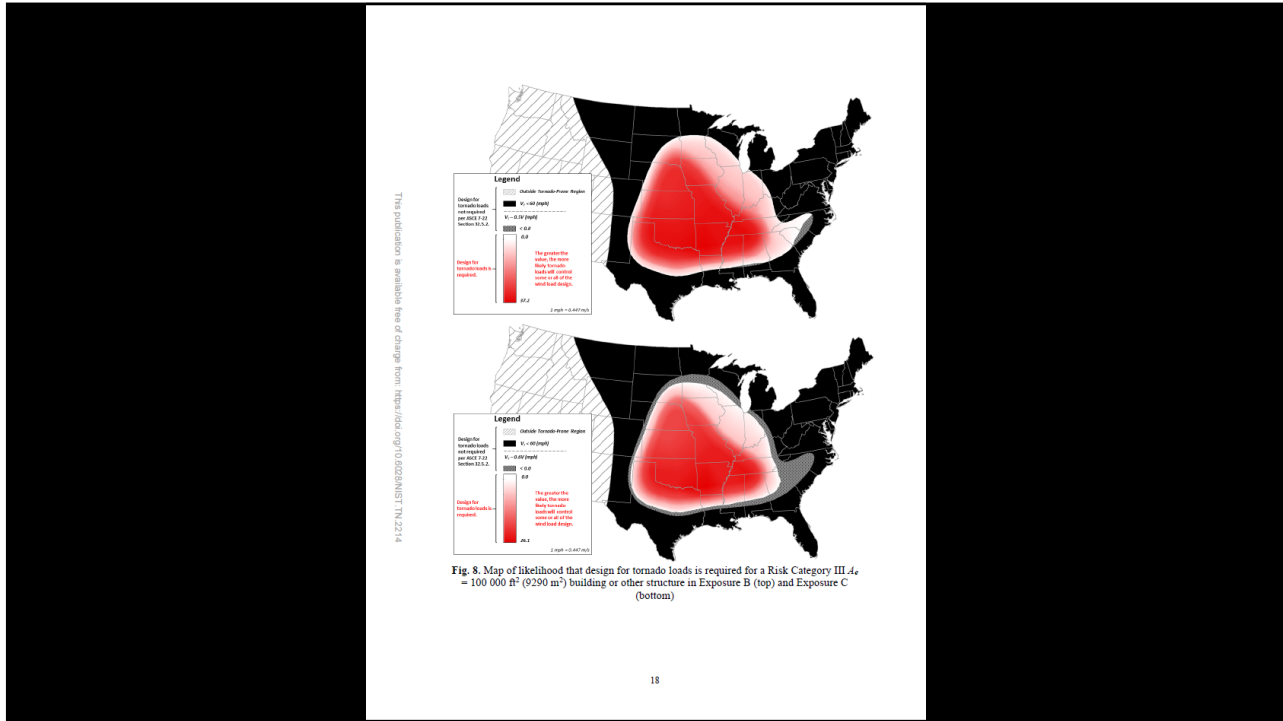


Fig. 8. Map of likelihood that design for tornado loads is required for a Risk Category III A, = 100 000 ft<sup>2</sup> (9290 m<sup>2</sup>) building or other structure in Exposure B (top) and Exposure C (bottom)

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