

IRCA Winter Meeting 2020

Des Moines, Iowa – January 23-24, 2020

ASCE 7-16: Understanding new minimum design wind load requirements

presented by

Mark S. Graham

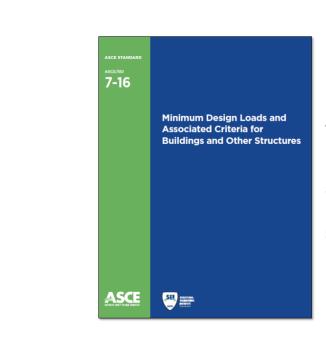
Vice President, Technical Services National Roofing Contractors Association



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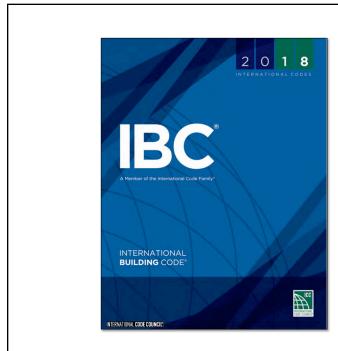
Topics

- ASCE 7-16
- Steel roof decks -- SDI bulletin
- Moisture in concrete roof decks
- Roof coatings
- Questions/other topics

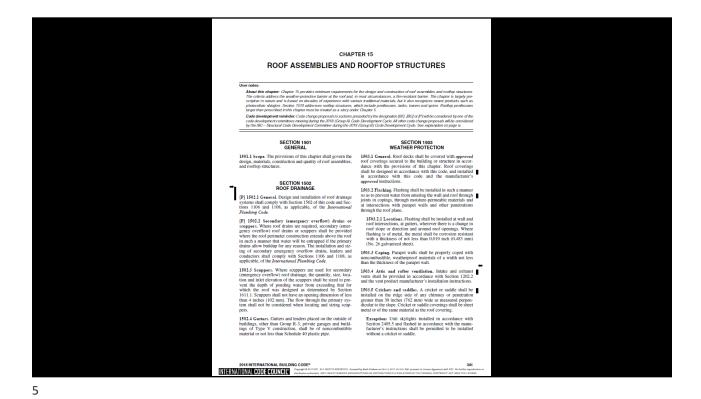


American Society of Civil Engineers Standard 7, "Minimum design loads and associated criteria for buildings and other structures" (ASCE 7-16)

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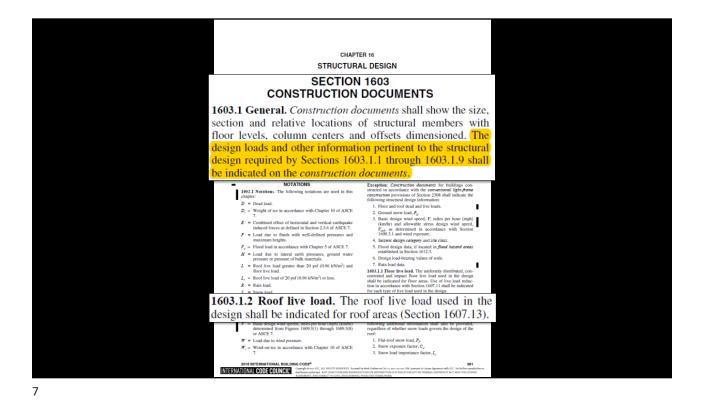


International Building Code, 2018 Edition

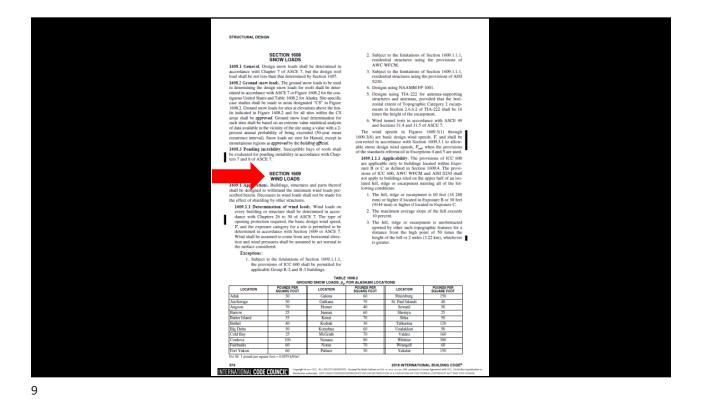


SECTION 1504 PERFORMANCE REQUIREMENTS **SECTION 1504** PERFORMANCE REQUIREMENTS 1504.1 Wind resistance of roofs. Roof decks and roof coverings shall be designed for wind loads in accordance with Chapter 16 and Sections 1504.2, 1504.3 and 1504.4. 1504.2 Wind resistance of clay and concrete tile. Wind loads on clay and concrete tile roof coverings shall be in accordance with Section 1609.5.

1504.2.1 Testing, Testing of concrete and clay roof tiles shall be in accordance with Sections 1504.2.1.1 and 1504.2.1.2. **ASCE 7-16** 1504.2.1.1 Overturning resistance. Concrete and clay roof tiles shall be tested to determine their resistance to overturning due to wind in accordance with Chapter 15 and either SBCCI SSTD 11 or ASTM C1568. 1504.3 Wind resistance of nonballasted roofs. Roof coverings insta 1507 that **ASCE 7-16's ASD method** are mecha k shall be designed or components and cladding in accordance with Section 1609.5.2. The wind load on the roof covering shall be permitted to be determined using allowable stress design. INTERNATIONAL CODE COUNCIL

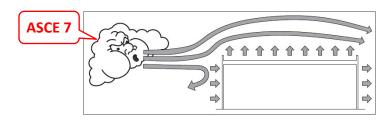


1603.1.4 Wind design data. The following information related to wind loads shall be shown, regardless of whether wind loads govern the design of the lateral force-resisting system of the structure: 1. Basic design wind speed, V, miles per hour and allowable stress design wind speed, V_{asd} , as determined in accordance with Section 1609.3.1. 2. Risk category. 3. Wind exposure. Applicable wind direction if more than one wind exposure is utilized. 4. Applicable internal pressure coefficient. 5. Design wind pressures to be used for exterior component and cladding materials not specifically designed by the registered design professional responsible for the design of the structure, psf (kN/ m^2). 1604.3.2 Reinforced concrete. The deflection of re forced concrete structural members shall not exceed the permitted by ACI 318. 2018 INTERNATIONAL BUILDING CODE INTERNATIONAL CODE COUNCIL® darkham



1609.3.1 Wind speed conversion. Where required, the design wind speeds of Figures 1609.3(1) through **ASD** method permitted 1609.3(8) shall be converted to allowable stress design wind speeds, V_{asd} , using Table 1609.3.1 or Equation 16-33. (Sec. 1504.3) $V_{asd} = V\sqrt{0.6}$ (Equation 16-33) hall be determined in accordance with the following: Exposure B. For buildings with a mean roof height of less than or equal to 30 feet (9144 mm), Exposure B shall apply where the ground surface roughness, as defined by Surface Roughness B, prevails in the upwind direction for a distance of not less than 1,500 to 1,500 feet (1650 feet). The building means the leichter of the control of t $V_{asd} = V\sqrt{0.6}$ (Equation 16-33) 1609.5 Roof systems. Roof systems shall be designed and constructed in accordance with Sections 1609.5.1 through 1609.5.3, as applicable. 1609.5.1 Roof deck. The roof deck shall be designed to withstand the wind pressures determined in accordance with ASCE 7. 1609.5.2 Roof coverings. Roof coverings shall comply with Section 1609.5.1. getation as well as from controlled features and the MPO4. With differentian and effects, the cub elected wind effection and estimate, the explaint of the building or structure shall be determined for the two upwind sectors extending 45 degrees (O/P) and either shall of the selected wind direction. The exposures in these two sectors shall be determined in accordance with Sections 1009.42 and 1009.43 and the exposure resulting in the highest wind loads shall be used to opperate the solid from their direction. Exception: Rigid tile roof coverings that are air permeable and installed over a roof deck complying with Section 1609.5.1 are permitted to be designed in accordance with Section 1609.5.3. Asphalt shingles installed over a roof deck complying with Section 1609.5.1 shall comply with the wind-resistance requirements of Section 1504.1.1. TABLE 1609.3.1 WIND SPEED CONVERSIONS^{a, b, c}
130 140 150 16 160 78 85 93 101 124 132 155 108 116 139 147 For SI: 1 mile per hour = 0.44 m/s.
a. Linear interpolation is permitted.
b. V_{max} = allowable stress design wind speed applicable to methods specified in Exceptions 1 through 5 of Section 1609.1.1.
c. V = basic design wind speeds determined from Figures 1609.3(1) through 1609.3(8). INTERNATIONAL CODE COUNCIL® distribution and

The fundamental concept



Wind creates pressures/forces on building elements

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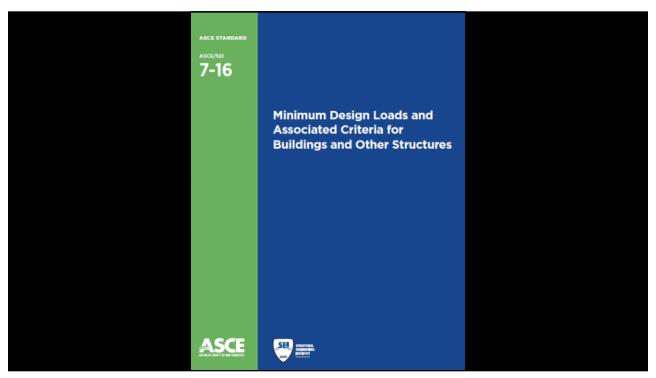
Fundamental concept -- continued

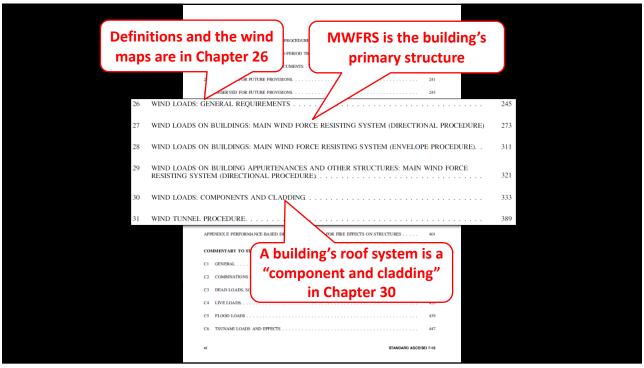
Adhesion or attachment ≥ Uplift pressure FM rating

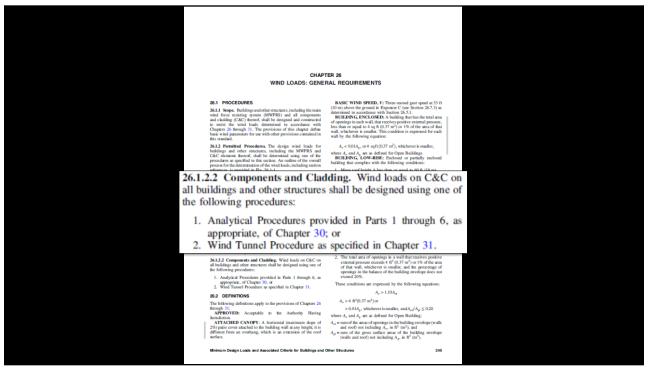
UL classification ≥ ASCE 7

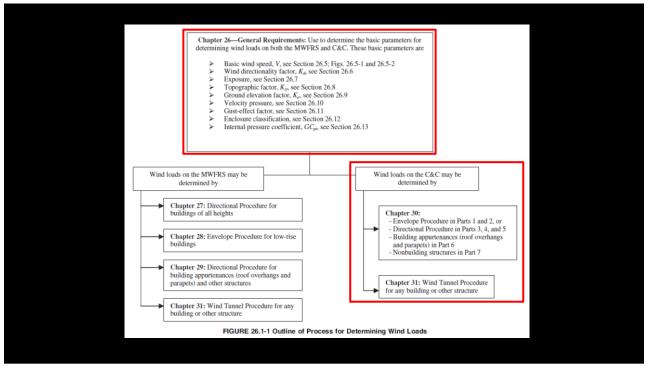
Engineering

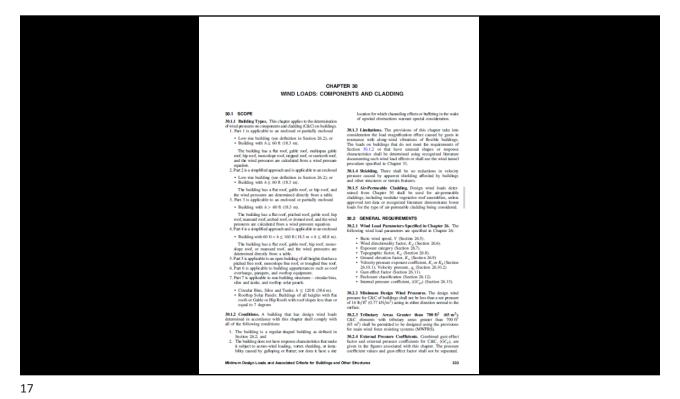


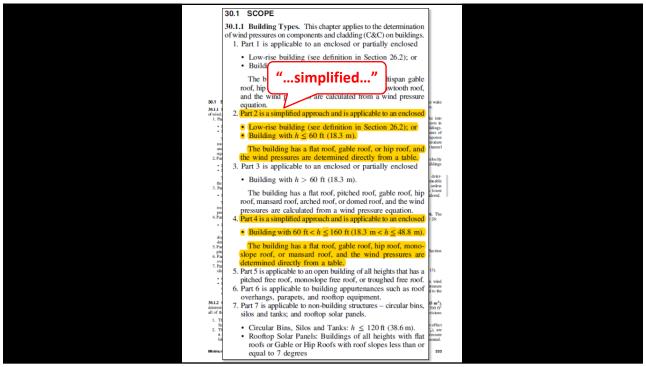


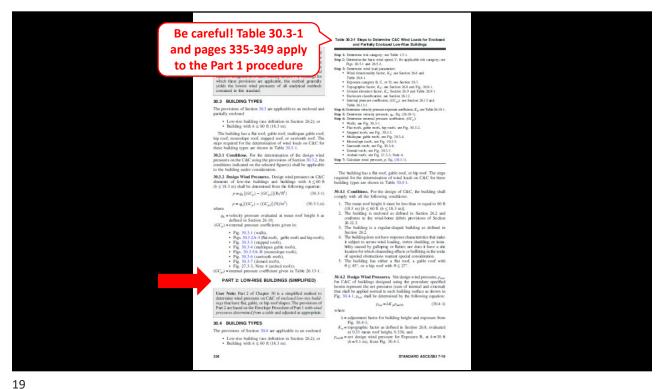


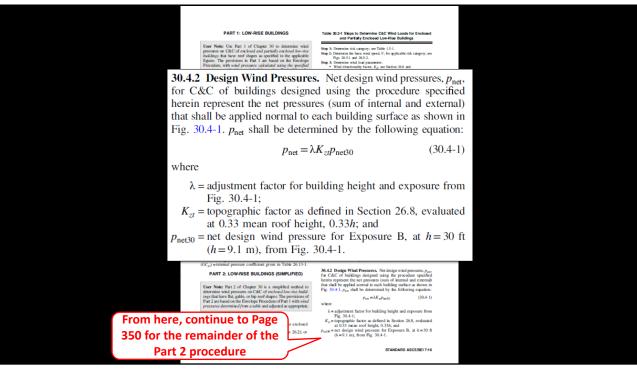


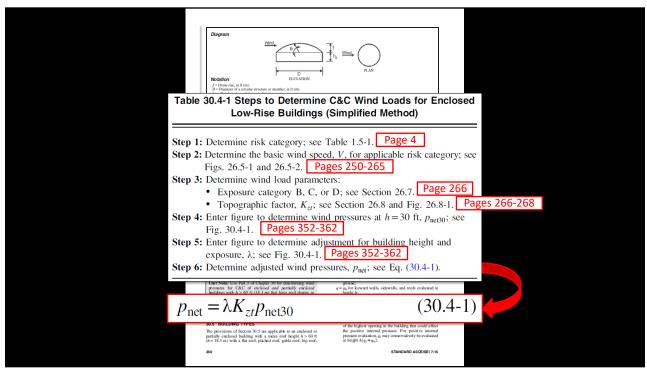


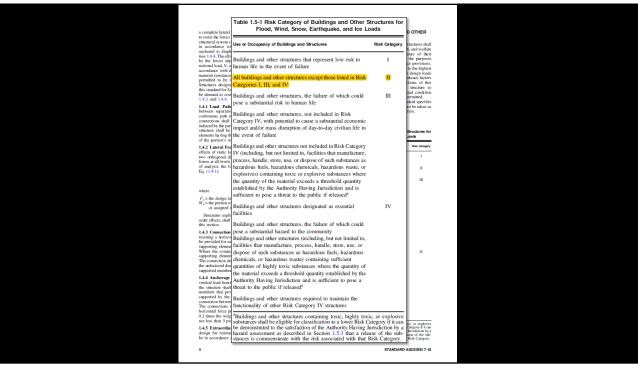


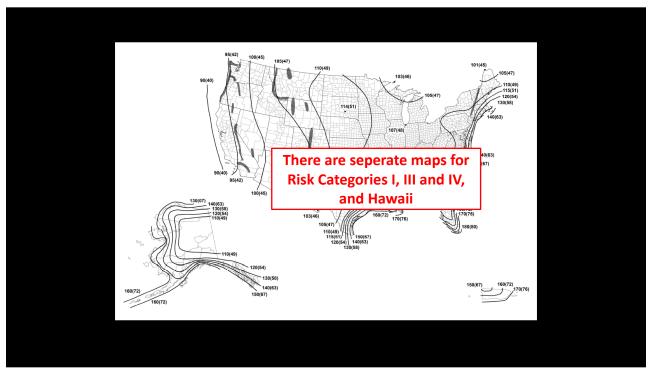


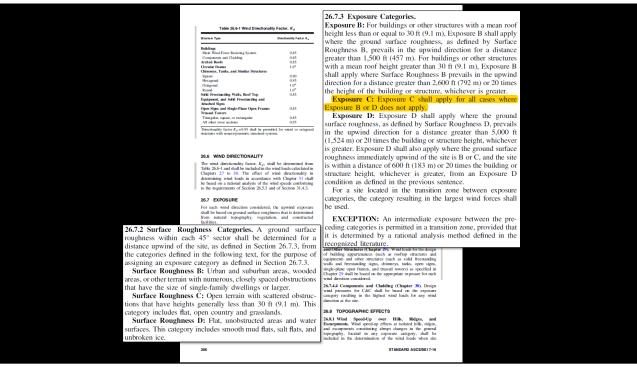


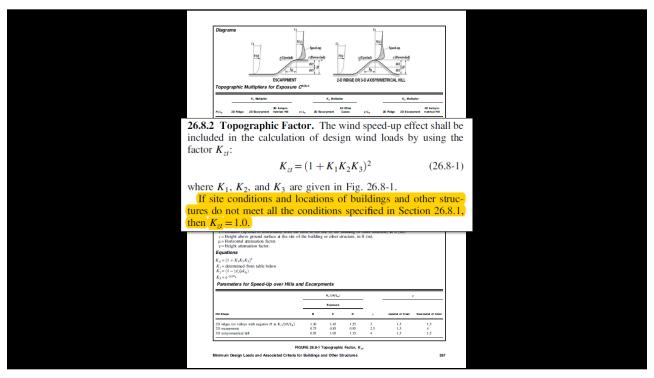


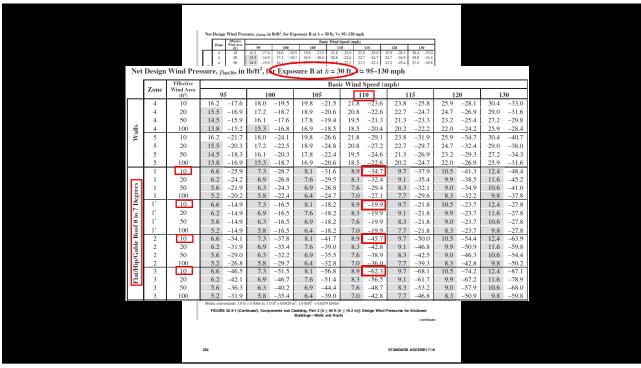


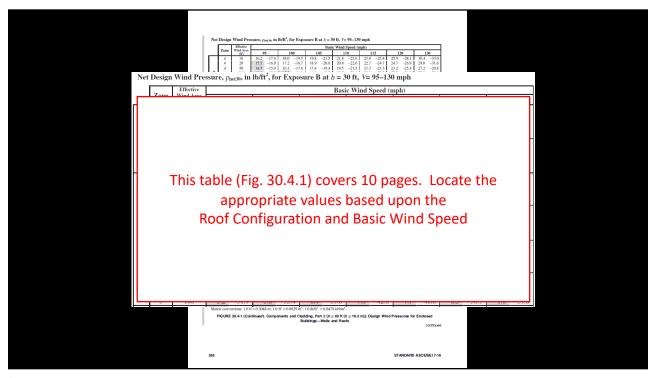












,	Net Design Wind Pressure for Roof Overhang, ρ_{meso} , in lb/ft ² , for Exposure B at $h=30$ ft, $V=95-200$ mph							
	Effective Wind Speed (mph) Zane							
	1 10 1 20 1 50	-31.6 -35.1 -38 -29.1 -32.2 -35 -25.7 -28.5 -31	5 -39.0 -42.6	-50.5 -59.3 -68.7 -78.9 -89.8 -101.3 -113.6 -12 -46.4 -54.5 -63.2 -72.5 -82.5 -93.2 -104.5 -11 -41.1 -48.2 -55.9 -64.1 -73.0 -82.4 -92.4 -10	26.6 -140.3 16.4 -129.0			
	1 100 2e 10	23.2 25.7 28	3 -31.1 -34.0		92.7 -102.8			
	2e 20 2e 50	-31.6 -35.0 -38 -22.9 -25.4 -28	.6 -42.3 -46.3 .0 -30.7 -33.6	-50.4 -59.1 -68.6 -78.7 -89.6 -101.1 -113.4 -12 -36.6 -42.9 -49.8 -57.1 -65.0 -73.4 -82.3 -9	26.3 -140.0 91.7 -101.6			
	2r 10	-22.0 -24.4 -26 -46.1 -51.1 -56	.9 -29.5 -32.3 .3 -61.8 -67.5	-35.1 -41.2 -47.8 -54.9 -62.4 -70.5 -79.0 -8 -73.5 -86.3 -100.1 -114.9 -130.7 -147.6 -165.5 -18 -63.3 -74.3 -86.2 -98.9 -112.5 -127.0 -142.4 -15	88.1 -97.6 84.4 -204.3			
Adjustme	1 Factor			_63.3	58.7 -175.8			
rajastire	it i detoi	ioi buii	g	girt and Exposure, x				
Mean		Exposure	2				ı	
Roof				1				
Height (ft)	В	С	D	-				
15	0.82	1.21	1.47					
20	0.89	1.29	1.55]				
30	1.00	1.40	1.66]				
35	1.05	1.45	1.70]				
40	1.09	1.49	1.74]				
45	1.12	1.53	1.78]				
50	1.16	1.56	1.81					
55	1.19	1.59	1.84					
60	1.22	1.62	1.87					
			= 0.3048 r	m; $1.0 \text{ ft}^2 = 0.0929 \text{ m}^2$; 1.0 lb/ft	$ft^2 = 0.0479$	kN/m ² .		
	Now 3: Demander what had prantners: • Wind districtionally place, K _g are Section 26.6 and Yahle 26.61.							
	 Exposume categops B, C, or D; see Section ΔC, 7. *Topographic loss κ, ξ_i: see Section ΔC, 10.5 and Fig. 26.8-1. 							
	 Ground elevation fastir, £, ; see Section 269 and Table 26,94 Enclosus e Leistration; see Section 5.61.2. 							
Step 4:	 Internal pressume coefficient, (Gr_a): we Section 26.13 and Table 26.13-1. Sign 4: Determine websign pressume exposure coefficient, K_i or K_i are architect, K_i or K_i are architect. 							
Step 6:	Step 5: Determine velocity pressure, q_i , Eq. (26.10-4). Step 6: Determine termal pressure coefficient; $G(\omega_i)$:							
	 Walls and fits roofs (0 × 107), see Fig. 30.5-1 Gable and bip roots, or Fig. 30.2-2 per fits of 60 Fig. 30.5-1 							
	Arnhad roofs, one Fig. 27.3-3, Note 4 Downal roofs, one Fig. 30.3-7							
Step 7;	alculate wind pressure	p, Eq. (30.5-1).						
362				STANDARD	D ASCE/SEI 7-16			

30.4.2 Design Wind Pressures. Net design wind pressures, p_{net} , for C&C of buildings designed using the procedure specified herein represent the net pressures (sum of internal and external) that shall be applied normal to each building surface as shown in Fig. 30.4-1. p_{net} shall be determined by the following equation:

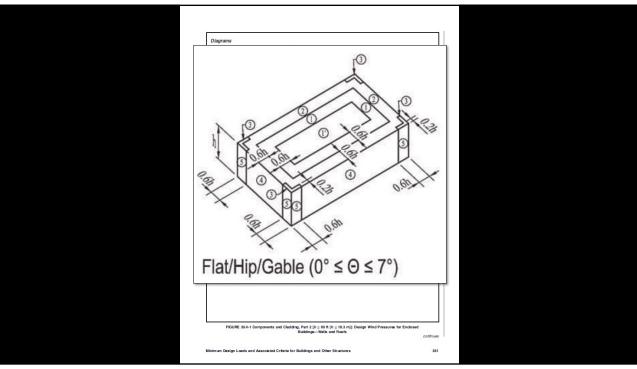
$$p_{\text{net}} = \lambda K_{zt} p_{\text{net30}} \tag{30.4-1}$$

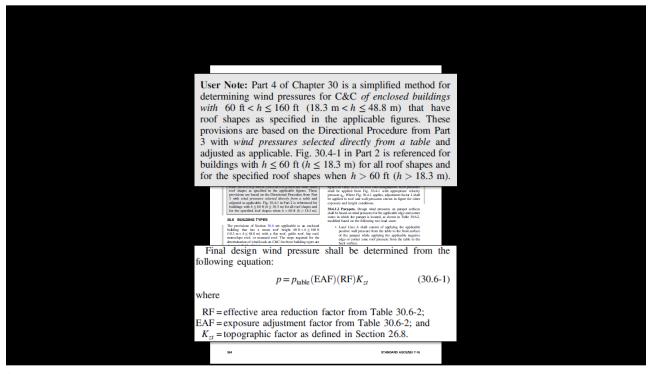
So for our hypothetical example, where:

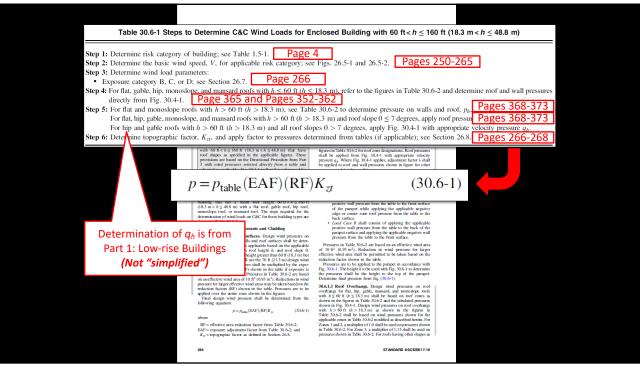
- Enclosed structure
- Risk Category II
- v = 110 mph
- Exposure C
- $K_{ZT} = 1.0$
- Mean roof height = 60 ft

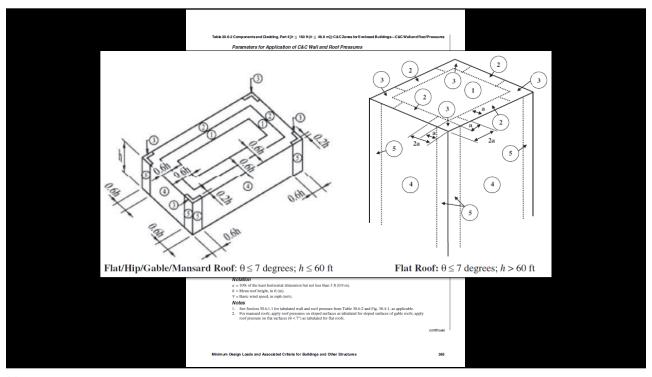
Zone 1': $p_{net} = 1.62 \times 1.0 \times (-19.9) = -32.2 \text{ psf}$ Zone 1: $p_{net} = 1.62 \times 1.0 \times (-34.7) = -56.2 \text{ psf}$ Zone 2: $p_{net} = 1.62 \times 1.0 \times (-45.7) = -74.0 \text{ psf}$ Zone 3: $p_{net} = 1.62 \times 1.0 \times (-62.3) = -100.1 \text{ psf}$

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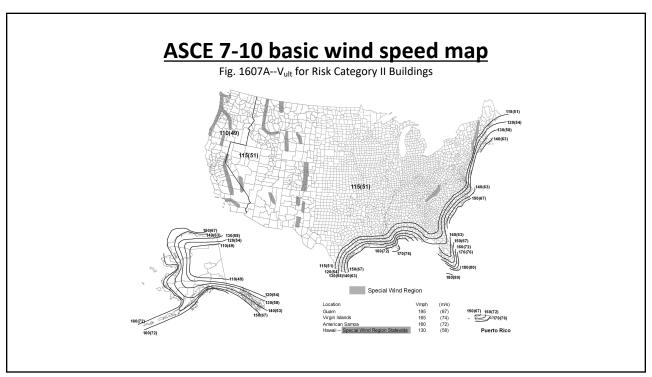


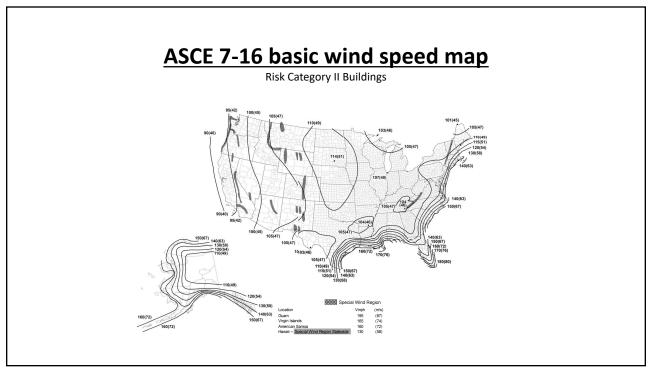
...so, it really is "simplified".

Noteworthy changes in ASCE 7-16

Compared to ASCE 7-10

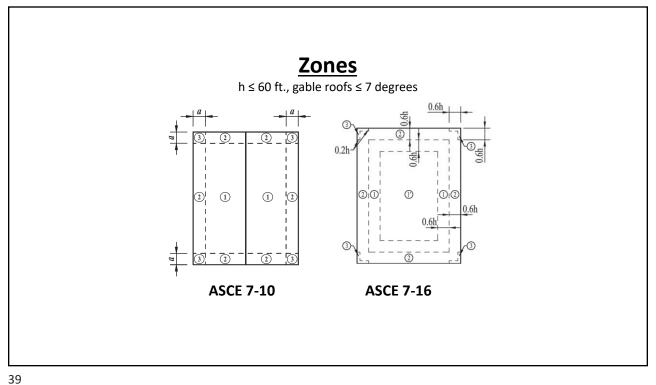
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$\underline{ \begin{tabular}{ll} \textbf{Comparing GC}_{\underline{p}} \begin{tabular}{ll} \textbf{pressure coefficients} \\ \textbf{h} \le 60 \mbox{ ft., gable roofs} \le 7 \mbox{ degrees} \\ \end{tabular} }$

Zone	ASCE 7-10	ASCE 7-16	Change
1'	n/a	0.9	-10%
1 (field)	-1.0	-1.7	+70%
2 (perimeter)	-1.8	-2.3	+28%
3 (corners)	-2.8	-3.2	+14%



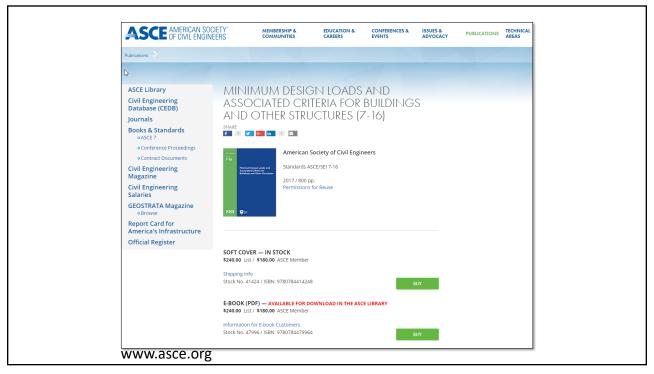
,,

Noteworthy changes in ASCE 7-16

compared to ASCE 7-10

- Revised basic wind speed map
- Changes (and new) pressure coefficients
- Revised perimeter and corner zones

While center field pressures may be slightly lower, field, perimeter and corner uplift pressures will generally be greater





How the roofing industry will adapt to ASCE 7-16 remains to be seen....

FM Global has indicated they will update their FM 1-28 to be based on ASCE 7-16 (with modifications) by the end of the 2018.

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This comparison illustrates why it is important for Designers to include wind design loads in their Construction Documents (per IBC Sec. 1603.1)...

...It also illustrate why specifying a wind warrantee can create an uneven playing field. Unless the Designer indicates the wind design loads, which design method will the manufacturer use (e.g., in a competitive environment)?

Steel roof decks/seam-fastened systems

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SDI bulletin

2009



The SDGERS research is looking at noding systems that irrusposite wide membranes oberts attached to be set dead following law patterns agreed at eye in \$12.0 Each will be the membrane looked to take the law to be set of the set of the law to be set of the law due to the value of the law due to the law to law

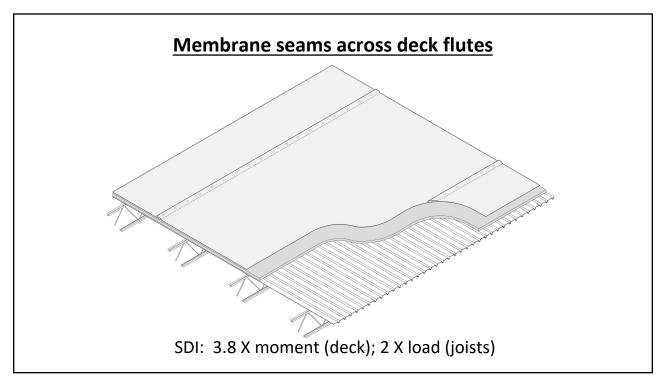
The strength of crowed convication between the membrane and the steel data, as well as the strength of crowed, balled, or which defend with the strength of crowed, balled, or which defend with the strength of crowed, balled, or which defend with the strength of the stre

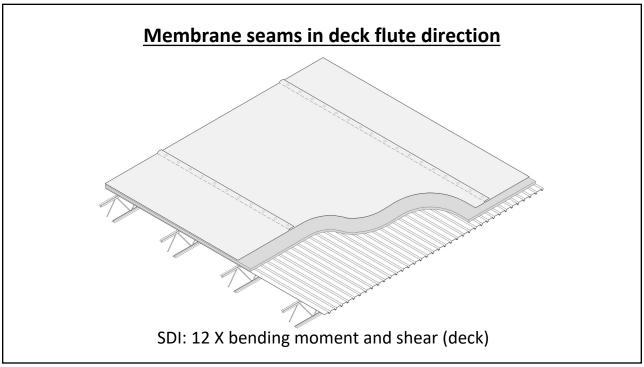
The zeror listening of wide conling membranes (up to 12th) and the corresponding spacing of the line of serows holding the membrane on the deck, will have a very different effect on the deck and transport stars as membrane that is adhered over its entire surface. The screws will produce a line load along the deck instead of a wideline had of the entire deck surface. The loads can be perpendicular or parallel to the deck flutte depending on the orientation of the membrane each condition can have different indications of the bodient had its anotified in the view membrane each condition can have

If the roofing membrane seam is perpendicular to the flutes of the deck, as illustrated in Figure 1, the are two special conditions that need to be considered.

if the membrane seam occurs at the mid-span of the steel deck an
 if the membrane seam occurs at the structural purpost ficialty.

- Decks designed for joist spacing between
 5' and 6' 8" o.c.
- Deck designed for uniform loading
- Seam-fastened singleply membranes are a concern





SDI bulletin – Conclusion

2009 hulletin

"...SDI does not recommend the use of roofing membranes attached to the steel deck using line patterns with large spacing unless a structural engineer has reviewed the adequacy of the steel deck and the structural supports to resist to wind uplift loads transmitted along the lines of attachment. Those lines of attachment shall only be perpendicular to the flutes of the deck."

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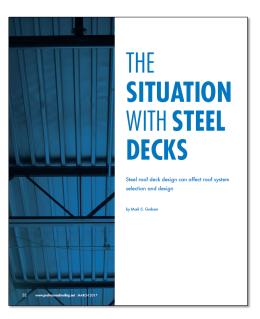
FM Global's Loss Prevention Data Sheet 1-29

April 2016



Revised/new criteria:

- Steel roof decks:
 - Uniformly-distributed loading
 - Concentrated loading
- Lightweight structural concrete



Professional Roofing

March 2017 www.professionalroofing.net

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Fastener pull-out tests...

There is little correlation between fastener pull-out resistance and a steel roof deck's yield strength and uplift (bending) strength



SDI Technical Note-No. 7 (Nov. 2019)

Mechanical attachment of single-ply roofing membranes to steel roof deck: Implications for steel deck design

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Analysis of Steel Deck and Supports for Mechanically Attached Membrane Roofs

For both new construction, and recovering or reroofing, the following guidelines reflect generally accepted industry practice:

- 1. Analyze the deck as a continuous 3-span beam, unless shorter spans are used.
- 2. Utilize all load combinations required by the applicable building code.
- 3. For the design spacing of fastener lines, place the first uplift line load at the midspan of the first deck span, then continue to add line loads as applicable. Repeat as necessary to determine the maximum positive and negative bending moments.
- 4. To determine maximum uplift on deck securement fasteners and support framing, place a line load atop a support.

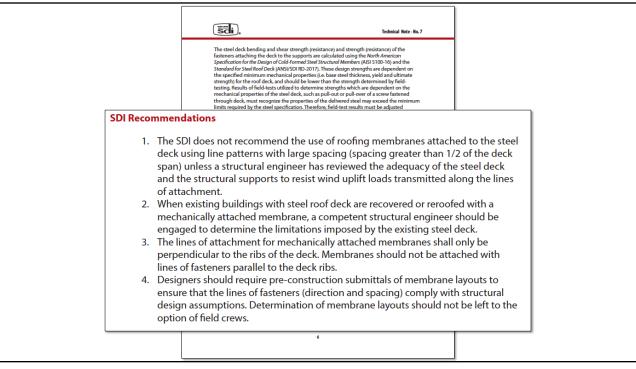
- tecommendations

 1. The SDI does not recommend the use of roofing membranes attached to the steel deck using line patterns with large spacing (spacing greater than 1/2 of the deck span) unless a structural engineer has reviewed the adequacy of the steel deck and the structural supports to resist wind upfill foods transmitted along the lines of attachment.

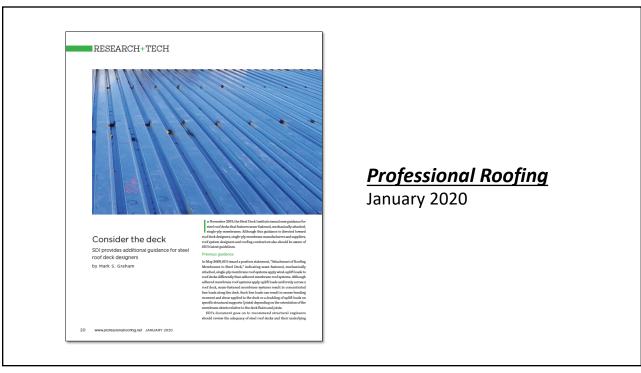
 2. When existing buildings with steel roof deck are recovered or reroofed with a mechanically attached membrane, a competent structural engineer should be engaged to determine the limitations imposed by the existing steel deck.

 3. The lines of attachment for mechanically attached membranes shall only be perpendicular to the ribs of the deck, Membranes should not be attached with lines of fasteners parallel to the deck ribs.

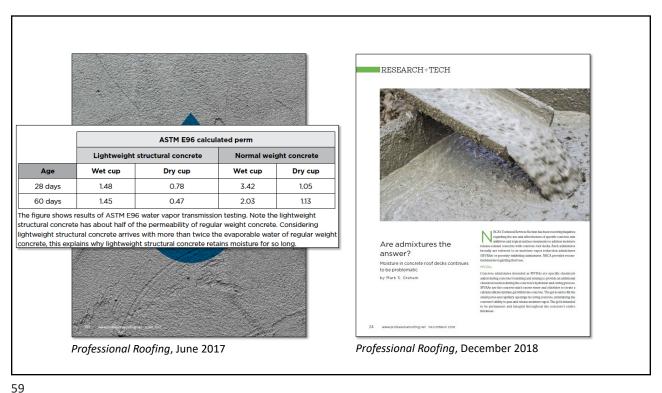
 A Designers should require pre-construction submittals of membrane layouts to ensure that the lines of fasteners (direction and spacing) comply with structural design assumptions. Determination of membrane layouts should not be left to the option of field crews.

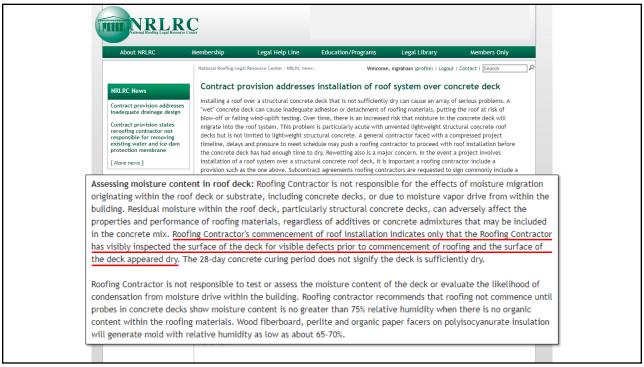


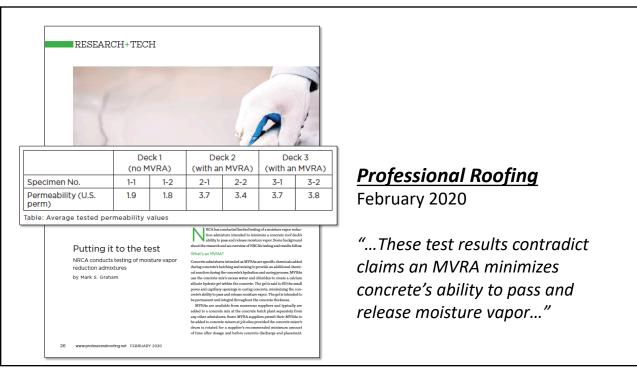
Expect additional scrutiny of seam-fastened, mechanically-attached, single-ply membrane roof systems



Moisture in concrete roof decks





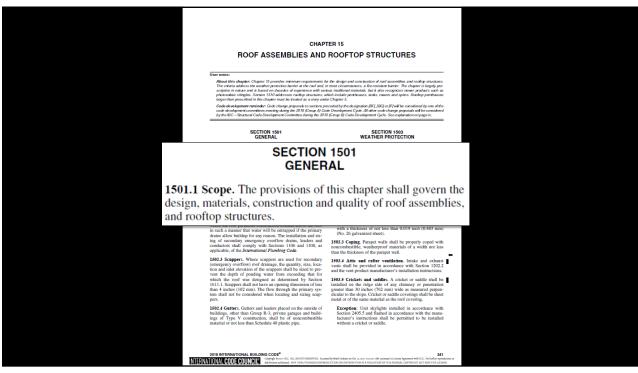


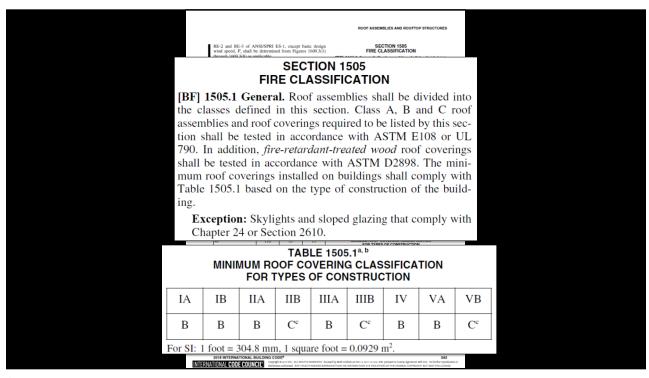
Roof coatings

International Building Code, 2018 Edition (IBC 2018)



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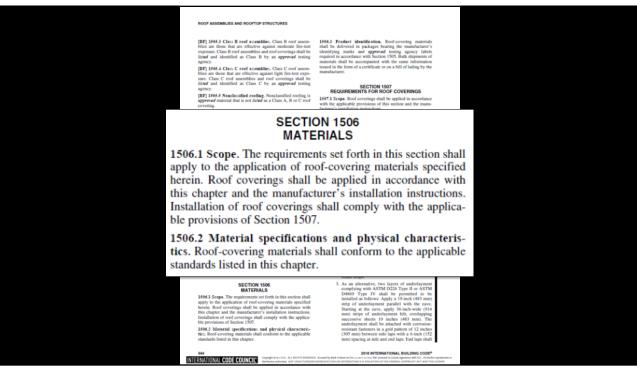


TABLE 1507.10.2 BUILT-UP ROOFING MATERIAL STANDARDS				
MATERIAL STANDARD	STANDARD			
Acrylic coatings used in roofing	ASTM D6083			
Aggregate surfacing	ASTM D1863			
Asphalt adhesive used in roofing	ASTM D3747			
Asphalt cements used in roofing	ASTM D2822; D3019; D4586			
Asphalt-coated glass fiber base sheet	ASTM D4601			
Asphalt coatings used in roofing	ASTM D1227; D2823; D2824; D4479			
Asphalt glass felt	ASTM D2178			
Asphalt primer used in roofing	ASTM D41			
Asphalt-saturated and asphalt-coated organic felt base sheet	ASTM D2626			
Asphalt-saturated organic felt (perforated)	ASTM D226			
Asphalt used in roofing	ASTM D312			
Coal-tar cements used in roofing	ASTM D4022; D5643			
Coal-tar saturated organic felt	ASTM D227			
Coal-tar pitch used in roofing	ASTM D450; Type I or II			
Coal-tar primer used in roofing, dampproofing and waterproofing	ASTM D43			
Glass mat, coal tar	ASTM D4990			
Glass mat, venting type	ASTM D4897			
Mineral-surfaced inorganic cap sheet	ASTM D3909			
Thermoplastic fabrics used in roofing	ASTM D5665, D5726			

1507.14 Sprayed polyurethane foam roofing. The installation of sprayed polyurethane foam roofing shall comply with the provisions of this section.

1507.14.1 Slope. Sprayed polyurethane foam roofs shall have a design slope of not less than one-fourth unit vertical in 12 units horizontal (2-percent slope) for drainage.

1507.14.2 Material standards. Spray-applied polyure-thane foam insulation shall comply with ASTM C1029 Type III or IV or ASTM D7425.

1507.14.3 Application. Foamed-in-place roof insulation shall be installed in accordance with the manufacturer's instructions. A liquid-applied protective coating that complies with Table 1507.14.3 shall be applied not less than 2 hours nor more than 72 hours following the application of the foam.

TABLE 1507.14.3 PROTECTIVE COATING MATERIAL STANDARDS

FILOTECTIVE CONTINUE MATERIAL STANDARDS				
MATERIAL	STANDARD			
Acrylic coating	ASTM D6083			
Silicone coating	ASTM D6694			
Moisture-cured polyurethane coating	ASTM D6947			

1507.14.4 Foam plastics. Foam plastic materials and installation shall comply with Chapter 26.

$\frac{\textbf{ASTM product standards}}{\text{Roof coatings}}$

ASTM D6083: acrylic

• ASTM D1227: emulsified asphalt

• ASTM D2823: asphalt

• ASTM D2824: aluminum

• ASTM D4479: asphalt

• ASTM D6694: silicone

• ASTM D6947: polyurethane

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Roof coatings Liquid-applied membranes

The differences

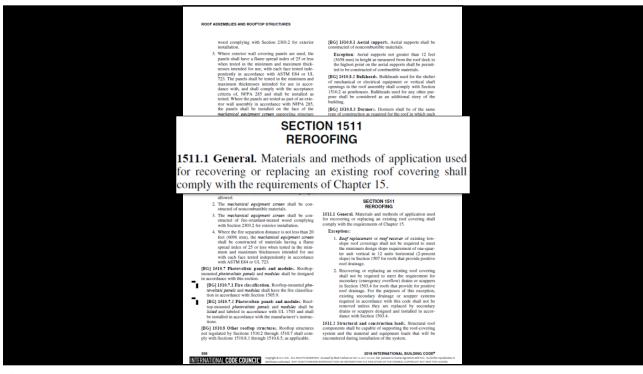
- Roof coatings are classified as surfacing products
- Liquid-applied membranes are classified as roof membranes

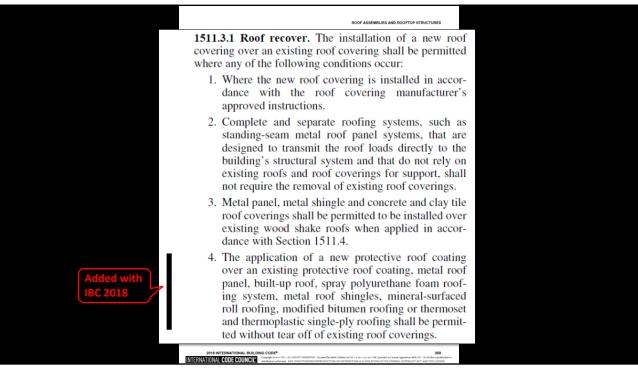
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1507.15 Liquid-applied roofing. The installation of liquid-applied roofing shall comply with the provisions of this section.

1507.15.1 Slope. Liquid-applied roofing shall have a design slope of not less than one-fourth unit vertical in 12 units horizontal (2-percent slope).

1507.15.2 Material standards. Liquid-applied roofing shall comply with ASTM C836, ASTM C957, ASTM D1227 or ASTM D3468, ASTM D6083, ASTM D6694 or ASTM D6947.





Roof coatings -- summary

- Fire classification (Class A, B or C) tested as an assembly
- Installed per the coating manufacturer's instructions
- ASTM product standards
- Reroofing? (Clarified in IBC 2018)

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Questions... and other topics

Mark S. Graham



Vice President, Technical Services National Roofing Contractors Association 10255 West Higgins Road, 600 Rosemont, Illinois 60018-5607

(847) 299-9070 mgraham@nrca.net www.nrca.net

Twitter: @MarkGrahamNRCA

Personal website: www.MarkGrahamNRCA.com