


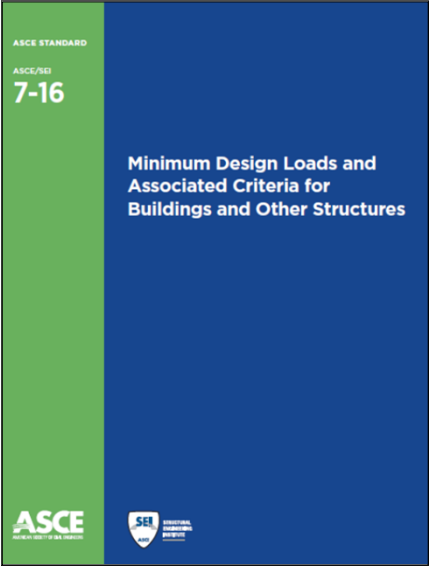
Roofing Week in Chicago
January 20-22, 2021

Roofing & New Wind Uplift Requirements
in 2018's Codes



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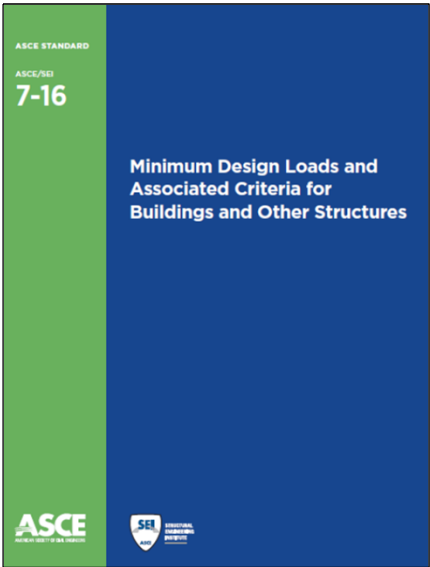
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- Provisions: 402 pages
- Commentary: 417 pages
- Soft cover
- Electronic file (PDF)

www.asce.org

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Wind loads:

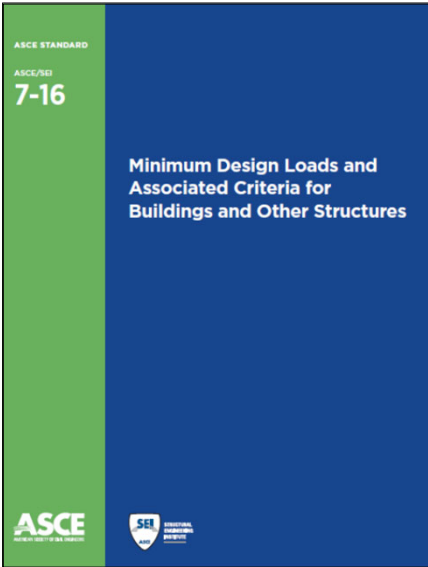
- Ch. 26—General requirements
- Ch. 27—Buildings-MWFRS (Directional procedure)
- Ch. 28—Buildings-MWFRS (Envelope procedure)
- Ch. 29—Appurtenances & other structures
- Ch. 30—Components and cladding
 - Part 1: Enclosed and partially-enclosed (low-rise)
 - Part 2: Simplified method (low-rise)
 - Part 3: Enclosed and partially-enclosed
 - Part 4: Simplified method (60 ft. < h ≤ 160 ft.)
 - Part 5: Open buildings
 - Part 6: Parapets & rooftop equipment
- Ch. 31—Wind tunnel procedure

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ASCE 7 is referenced in the International Building Code (IBC)



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Comparing IBC editions to ASCE 7 editions

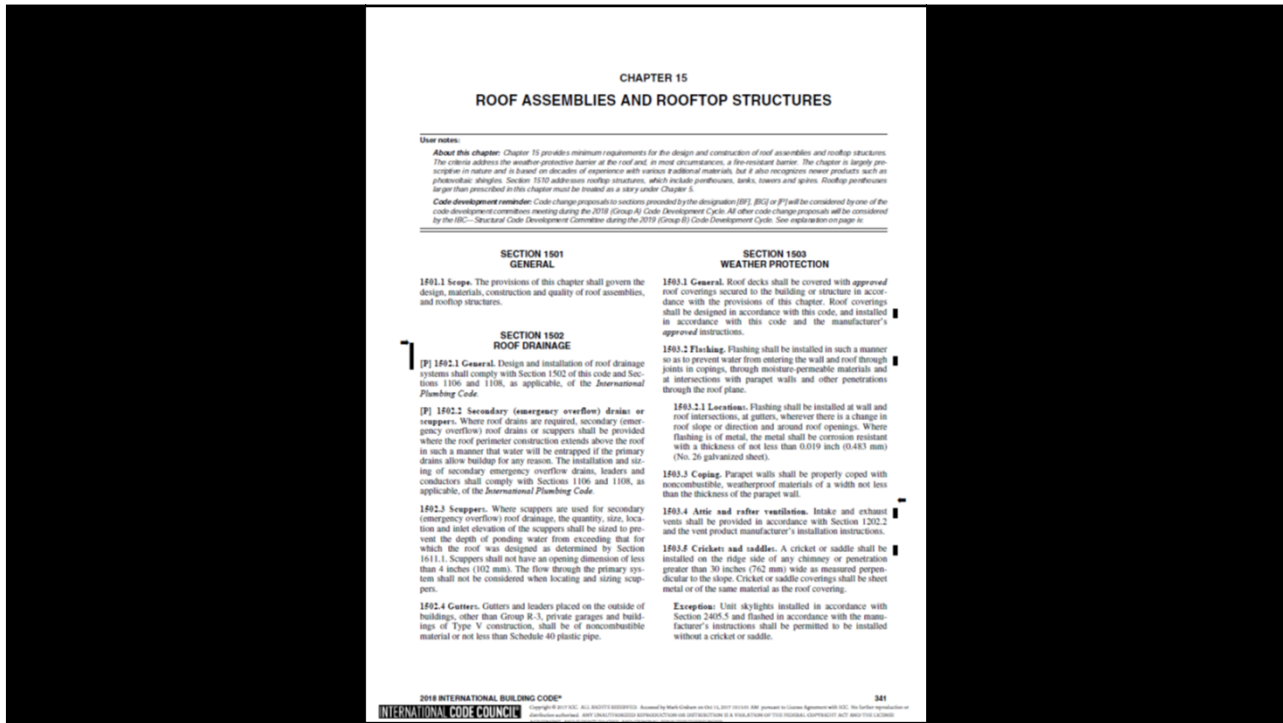
IBC	ASCE 7
IBC 2006	ASCE 7-05
IBC 2009	ASCE 7-05
IBC 2012	ASCE 7-10
IBC 2015	ASCE 7-10
IBC 2018	ASCE 7-16
IBC 2021	ASCE 7-16

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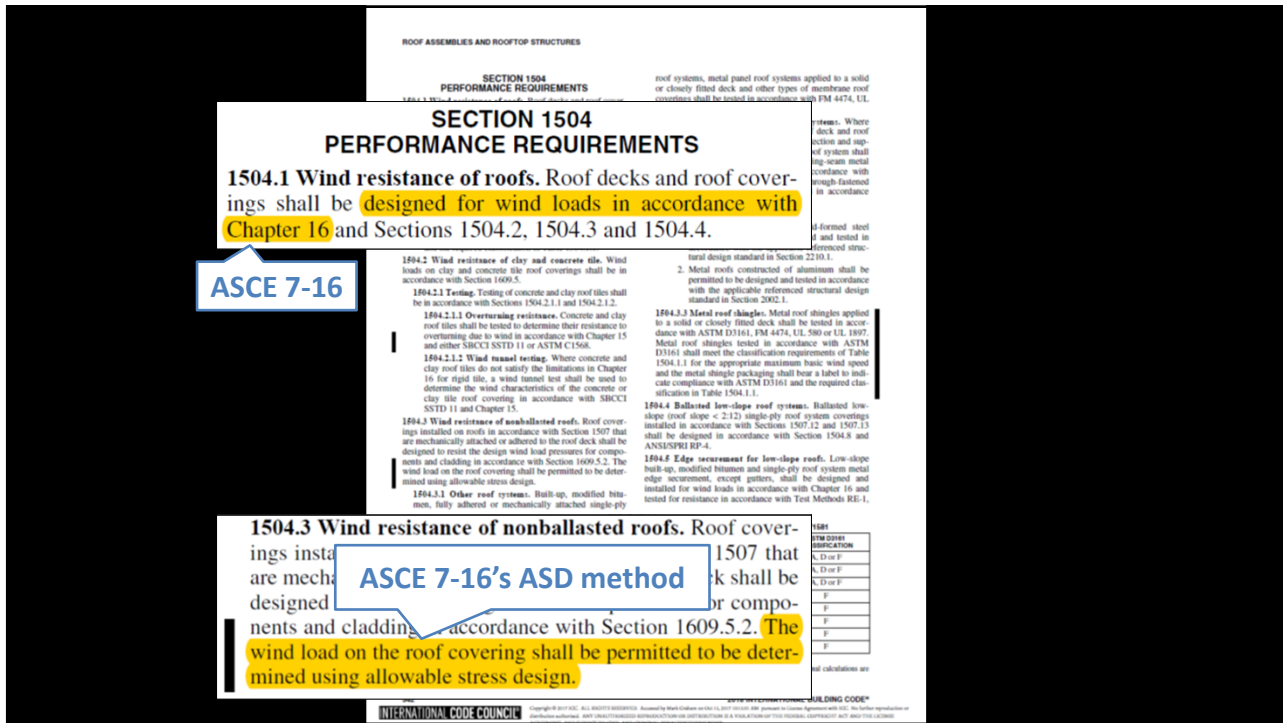


International Building Code, 2018 Edition

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Allowable stress design vs. Ultimate strength design

- ASD has been a traditional design method
- Ultimate strength design is not new
 - First implemented into ASCE 7 with the 2010 Edition
- What's the difference (as it applies to wind design)?
 - Different wind maps
 - V_{ULT} has higher basic wind speeds than V_{ASD}
 - Factors:
 - Ultimate strength design uses a “strength design pressure” (1.0W)
 - Allowable stress design uses a “allowable stress design load factor” of 0.6W

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STRUCTURAL DESIGN

**SECTION 1608
SNOW LOADS**

1608.1 General. Design snow loads shall be determined in accordance with Chapter 7 of ASCE 7, but the design roof load shall be not less than that determined by Section 1607.

1608.2 Ground snow load. The ground snow load to be used in determining the design snow loads for roofs shall be determined in accordance with ASCE 7 or Figure 1608.2 for the contiguous United States and Table 1608.2 for Alaska. Site-specific case studies shall be made in areas designated “CS” in Figure 1608.2. Ground snow loads for sites at elevations above the limits indicated in Figure 1608.2 and for all sites within the CS areas shall be approved. Ground snow load determination for such sites shall be based on an extreme value statistical analysis of data available in the vicinity of the site using a value with a 2-percent annual probability of being exceeded (50-year mean recurrence interval). Snow loads are zero for Hawaii, except in mountainous regions as approved by the building official.

1608.3 Ponding instability. Susceptible bays of roofs shall be evaluated for ponding instability in accordance with Chapters 7 and 8 of ASCE 7.

**SECTION 1609
WIND LOADS**

1609.1 Application. Buildings, structures and parts thereof shall be designed to withstand the minimum wind loads prescribed herein. Decreases in wind loads shall not be made for the effect of shielding by other structures.

1609.1.1 Determination of wind loads. Wind loads on every building or structure shall be determined in accordance with Chapters 26 to 30 of ASCE 7. The type of opening protection required, the basic design wind speed, F , and the exposure category for a site is permitted to be determined in accordance with Section 1609 or ASCE 7. Wind shall be assumed to come from any horizontal direction and wind pressures shall be assumed to act normal to the surface considered.

Exception:

- Subject to the limitations of Section 1609.1.1.1, the provisions of ICC 600 shall be permitted for applicable Group R-2 and R-3 buildings.

2. Subject to the limitations of Section 1609.1.1.1, residential structures using the provisions of AWC WFCM.

3. Subject to the limitations of Section 1609.1.1.1, residential structures using the provisions of ANSI S230.

4. Design using NAAMM FP 1001.

5. Design using TIA-222 for antenna-supporting structures and antennas, provided that the horizontal extent of Topographic Category 2 encampments in Section 2.6.6.2 of TIA-222 shall be 16 times the height of the encampment.

6. Wind tunnel tests in accordance with ASCE 49 and Section 31.4 and 31.5 of ASCE 7.

The wind speeds in Figures 1609.3(1) through 1609.3(8) are basic design wind speeds, F , and shall be converted in accordance with Section 1609.1.1 to allowable stress design wind speeds, F_w , when the provisions of the standards referenced in Exceptions 4 and 5 are used.

1609.1.1.1 Applicability. The provisions of ICC 600 are applicable only to buildings located within Exposure B or C as defined in Section 1609.4. The provisions of ICC 600, AWC WFCM and ANSI S230 shall not apply to buildings sited on the upper half of an isolated hill, ridge or escarpment meeting all of the following conditions:

- The hill, ridge or escarpment is 60 feet (18 288 mm) or higher if located in Exposure B or 30 feet (9144 mm) or higher if located in Exposure C.
- The maximum average slope of the hill exceeds 10 percent.
- The hill, ridge or escarpment is unobstructed upwind by other such topographic features for a distance from the high point of 50 times the height of the hill or 2 miles (3.22 km), whichever is greater.

**TABLE 1608.2
GROUND SNOW LOADS, p_g , FOR ALASKAN LOCATIONS**

LOCATION	POUNDS PER SQUARE FOOT	LOCATION	POUNDS PER SQUARE FOOT	LOCATION	POUNDS PER SQUARE FOOT
Adak	40	Galena	40	Peavine	150
Anchorage	30	Galena	70	St. Paul Islands	40
Aspen	30	Homer	40	Seward	30
Barrow	25	Juneau	40	Sitka	25
Barrow Island	35	Ketchikan	70	Sitka	50
Bethel	40	Kodiak	30	Talkeetna	120
Big Lake	30	Kotzebue	40	Ukiahville	50
Chadley	25	McGrath	70	Valdez	160
Cordova	100	Nemana	80	Whitmer	300
Edwards	40	Nome	70	Wrangell	80
Fort Yukon	60	Palmer	50	Yakutat	150

For 30:1 ponded per square foot = 0.6479 kN/m²

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STRUCTURAL DESIGN

ASD method permitted (Sec. 1504.3)

1609.3.1 Wind speed conversion. Where required, the basic design wind speeds of Figures 1609.3(1) through 1609.3(8) shall be converted to allowable stress design wind speeds, V_{asd} , using Table 1609.3.1 or Equation 16-33.

$$V_{asd} = V_s / 0.6 \quad \text{(Equation 16-33)}$$

1609.3.2 Wind speed conversion. Where required, the basic design wind speeds of Figures 1609.3(1) through 1609.3(8) shall be converted to allowable stress design wind speeds, V_{asd} , using Table 1609.3.1 or Equation 16-33.

$$V_{asd} = V_s / 0.6 \quad \text{(Equation 16-33)}$$

where:

- V_{asd} = Allowable stress design wind speed applicable to methods specified in Exceptions 4 and 5 of Section 1609.1.1.
- V_s = Basic design wind speeds determined from Figures 1609.3(1) through 1609.3(8).

1609.3 Exposure category. For each wind direction considered, an exposure category that adequately reflects the characteristics of ground surface irregularities shall be determined for the site at which the building or structure is to be constructed. Account shall be taken of variations in ground surface roughness that arise from natural topography and vegetation as well as from constructed features.

1609.4.1 Wind directions and sectors. For each selected wind direction at which the wind loads are to be evaluated, the exposure of the building or structure shall be determined for the two upwind sectors extending 45 degrees (0.79 rad) either side of the selected wind direction. The exposures in these two sectors shall be determined in accordance with Sections 1609.4.2 and 1609.4.3 and the exposure resulting in the highest wind loads shall be used to represent winds from that direction.

1609.4.2 Surface roughness categories. A ground surface roughness within each 45-degree (0.79 rad) sector shall be determined for a distance upwind of the site as defined in Section 1609.4.3 from the following categories, for the purpose of assigning an exposure category as defined in Section 1609.4.4.

1609.4.3 Roof deck. The roof deck shall be designed to withstand the wind pressures determined in accordance with ASCE 7.

1609.4.4 Roof coverings. Roof coverings shall comply with Section 1609.5.1.

Exception: Rigid tile roof coverings that are air permeable and installed over a roof deck complying with Section 1609.5.1 are permitted to be designed in accordance with ASCE 7.

1609.5 Roof system. Roof systems shall be designed and constructed in accordance with Sections 1609.5.1 through 1609.5.3, as applicable.

1609.5.1 Roof deck. The roof deck shall be designed to withstand the wind pressures determined in accordance with ASCE 7.

1609.5.2 Roof coverings. Roof coverings shall comply with Section 1609.5.1.

Exception: Rigid tile roof coverings that are air permeable and installed over a roof deck complying with Section 1609.5.1 are permitted to be designed in accordance with ASCE 7.

V_s	100	110	120	130	140	150	160	170	180	190	200
V_{asd}	78	85	93	101	108	116	124	132	139	147	155

For SI: 1 mile per hour = 0.44 m/s.
 a. Linear interpolation is permitted.
 b. V_{asd} = allowable stress design wind speed applicable to methods specified in Exceptions 1 through 5 of Section 1609.1.1.
 c. V_s = basic design wind speeds determined from Figures 1609.3(1) through 1609.3(8).

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With ASCE 7-10 and ASCE 7-16, there are four different Basic Wind Speed maps, based on Risk Category

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Basic wind speeds

Chicago:

ASCE 7-05:

- $V_{ASD} = 90$ mph (50-year return period)

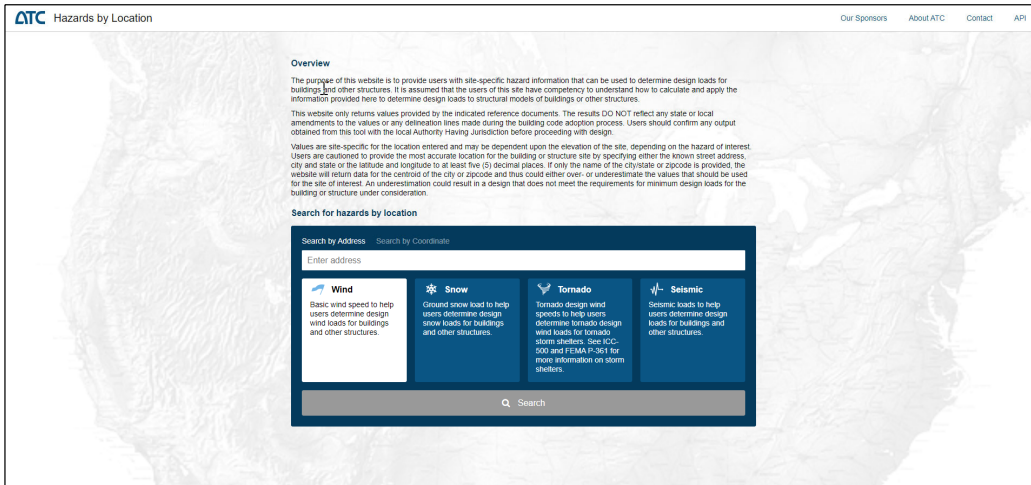
ASCE 7-16:

- Risk Category I (MRI = 300 years): $V_{ULT} = 100$ mph
- Risk Category II (MRI = 700 years): $V_{ULT} = 107$ mph
- Risk Category III (MRI = 1,700 years): $V_{ULT} = 114$ mph
- Risk Category IV (MRI = 3,000 years): $V_{ULT} = 119$ mph

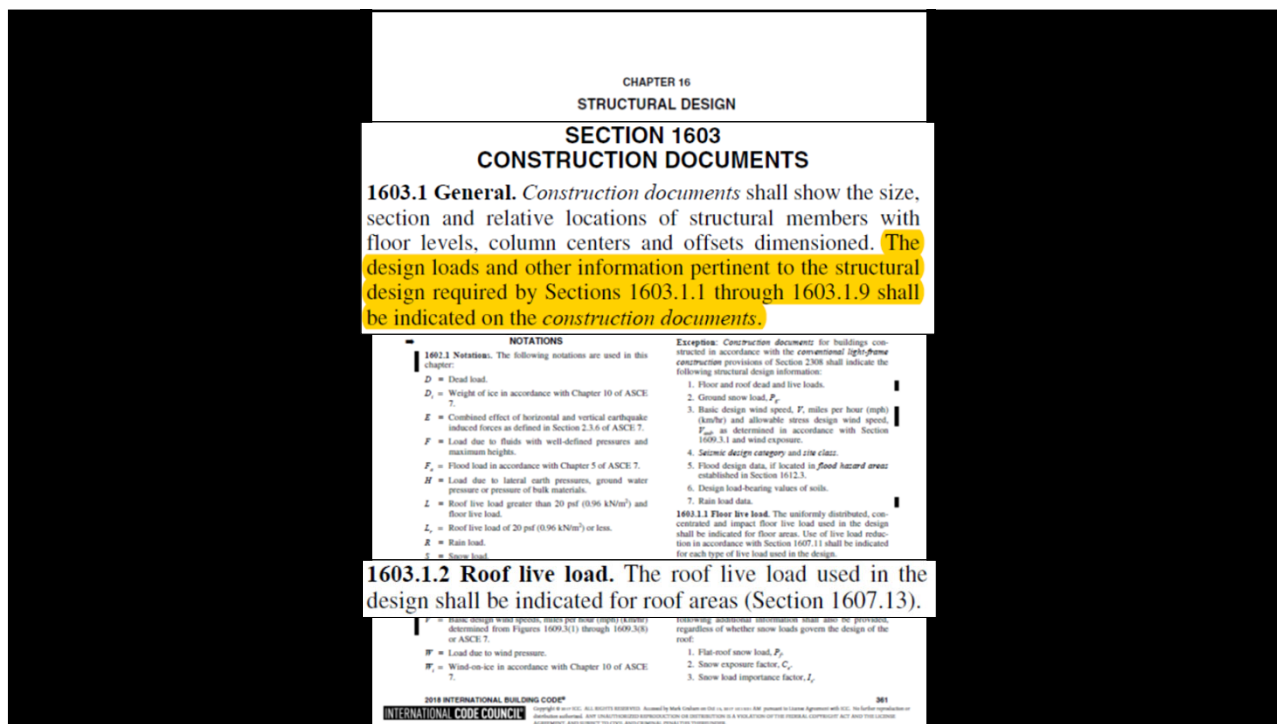
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Applied Technology Council (ATC) hazards by location

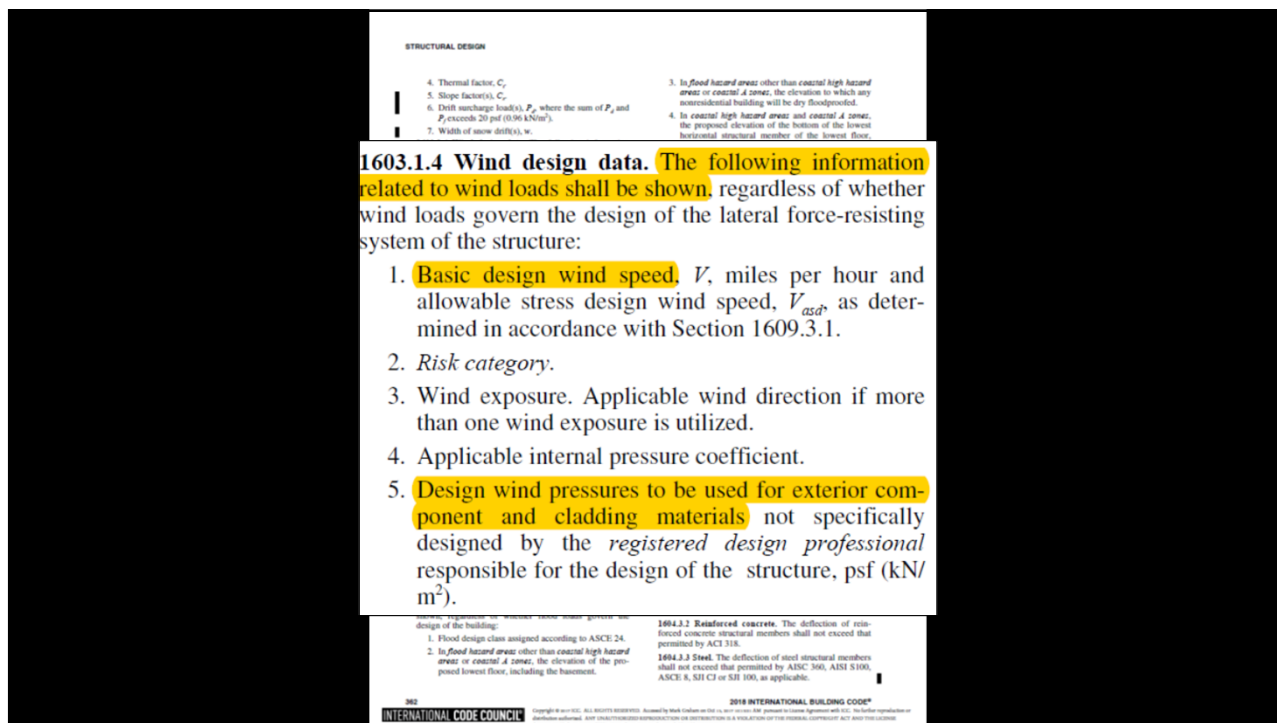
www.hazards.atcouncil.org



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Noteworthy changes in ASCE 7-16

Compared to ASCE 7-10

- Revised basic wind speed maps
- Changes (and new) pressure coefficients
- Revised perimeter and corner zones

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Comparing GC_p pressure coefficients

h ≤ 60 ft., gable roofs ≤ 7 degrees

Zone	ASCE 7-10	ASCE 7-16	Change
1'	n/a	0.9	-10%
1 (field)	-1.0	-1.7	+70%
2 (perimeter)	-1.8	-2.3	+28%
3 (corners)	-2.8	-3.2	+14%

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ASCE 7-10's roof zones

$h \leq 60 \text{ ft.}, \text{ gable roofs } \leq 7 \text{ degrees}$

$a = 10\%$ of the least horizontal dimension, or $0.4h$,
whichever is smaller but not less than either 4%
of the least horizontal dimension or $3 \text{ ft } (0.9 \text{ m})$.

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Table 30.6-2 Components and Cladding, Part 4 ($h \leq 180 \text{ ft}$ ($\leq 48.8 \text{ m}$)) CAC Zones for Enclosed Buildings—CAC Wall and Roof Pressures
Parameters for Application of CAC Wall and Roof Pressures

Flat/Hip/Gable/Mansard Roof: $\theta \leq 7 \text{ degrees}; h \leq 60 \text{ ft}$

Flat Roof: $\theta \leq 7 \text{ degrees}; h > 60 \text{ ft}$

NOTATION
 a = 10% of the least horizontal dimension but not less than 3 ft (0.9 m).
 h = Mean roof height, in ft (m).
 V = Basic wind speed, in mph (m/s).

Notes
 1. See Section 30.6.1.1 for tabulated wall and roof pressure from Table 30.6-2 and Fig. 30.4-1, as applicable.
 2. For mansard roofs, apply roof pressures on sloped surfaces as tabulated for sloped surfaces of gable roofs; apply roof pressure on flat surfaces ($\theta < 7^\circ$) as tabulated for flat roofs.

continue

Minimum Design Loads and Associated Criteria for Buildings and Other Structures 365

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Comparing ASCE 7-05, ASCE 7-10 and ASCE 7-16

Example: A low-rise office building (Risk Category II) in Chicago, IL. The building is an enclosed structure with a mean roof height of 60 ft. The building is in an open terrain area that can be categorized as Exposure Category C.

Document	Basic wind speed (mph)	Design wind pressure (psf)			
		Zone 1' (Center)	Zone 1 (Field)	Zone 2 (Perimeter)	Zone 3 (Corners)
ASCE 7-05	$V_{ASD} = 90$	--	24	40	58
ASCE 7-10 Ult.	$V_{ULT} = 115$	--	39	65	97
ASCE 7-10 ASD	$V_{ASD} = 90$	--	23	39	58
ASCE 7-16 Ult.	$V_{ULT} = 105$	30	51	67	92
ASCE 7-16 ASD	$V_{ASD} = 90$	18	31	30% increase	

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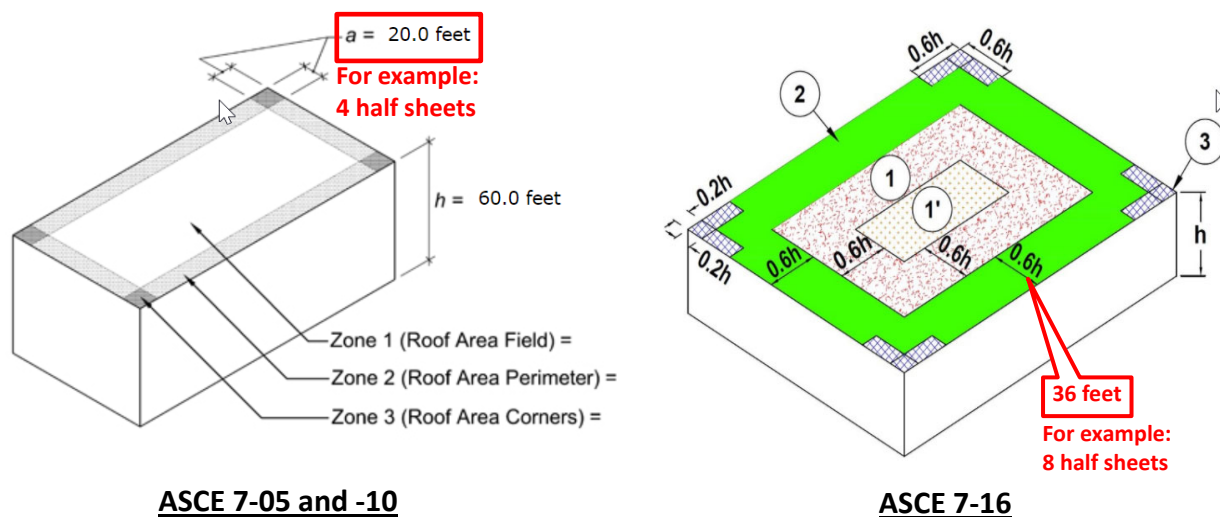
Comparing ASCE 7-05, ASCE 7-10 and ASCE 7-16

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Document	Basic wind speed (mph)	Design wind pressure (psf)			
		Zone 1' (Center)	Zone 1 (Field)	Zone 2 (Perimeter)	Zone 3 (Corners)
ASCE 7-05	$V_{ASD} = 90$	--	24	FM 1-60	58
ASCE 7-10 Ult.	$V_{ULT} = 115$	--	39		97
ASCE 7-10 ASD	$V_{ASD} = 90$	--	23	FM 1-60	58
ASCE 7-16 Ult.	$V_{ULT} = 105$	30	51		92
ASCE 7-16 ASD	$V_{ASD} = 90$	18	31	FM 1-75 or FM 1-90	

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ASCE 7-16's impact on perimeter and corner zones



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A few words on “safety factors” ...

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Safety factor

A factor of safety is intended to address possible variances in load determination; normally anticipated variances in materials, including material aging and deterioration; and in application.

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A safety factor in wind design

- Use of a safety factor is not required by the Code
- FM Global assigns a SF = 2.0 in their ASD-based classifications
 - A FM I-90 classification has a maximum 45 psf uplift in Zone 2 (field)
- ASTM D6630 (a guide) suggest a SF = 2.0 based on ASD
- CSA A123.21 uses a SF = 1.5
- SPRI WD-1 suggests a SF = 2.0 for ASD and uses a SF = 1.0 in their Ultimate Design examples

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So, what is an appropriate/a reasonable safety factor for Ultimate Strength Design?

Since Ultimate Strength Design's loads are inherently higher than ASD's loads, in a sense, there is somewhat of an additional "factor addressing an additional level of safety" already built into wind design using Ultimate Strength Design

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Comparing ASCE 7-05, ASCE 7-10 and ASCE 7-16

Example: A low-rise office building (Risk Category II) in Chicago, IL. The building is an enclosed structure with a mean roof height of 60 ft. The building is in an open terrain area that can be categorized as Exposure Category C.

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ASCE 7-16 Ult.	$V_{ULT} = 105$	30	51	65 % increase	
ASCE 7-16 ASD	$V_{ASD} = 90$	18	31	41	55

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If a SF = 2.0 is applied to Ultimate Strength Design...

Comparing ASCE 7-05, ASCE 7-10 and ASCE 7-16

Example: A low-rise office building (Risk Category II) in Chicago, IL. The building is an enclosed structure with a mean roof height of 60 ft. The building is in an open terrain area that can be categorized as Exposure Category C.

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ASCE 7-05	$V_{ASD} = 90$	--	24	40	58
ASCE 7-10 Ult.	$V_{ULT} = 115$	--	39	65	97
ASCE 7-10 ASD	$V_{ASD} = 90$	--	23	39	58
ASCE 7-16 Ult.	$V_{ULT} = 105$	30	51	FM 1-105 or FM 1-120	
ASCE 7-16 ASD	$V_{ASD} = 90$	18	31	FM 1-75 or FM 1-90	

A SF = 2.0 seems excessive for Ultimate Strength Design

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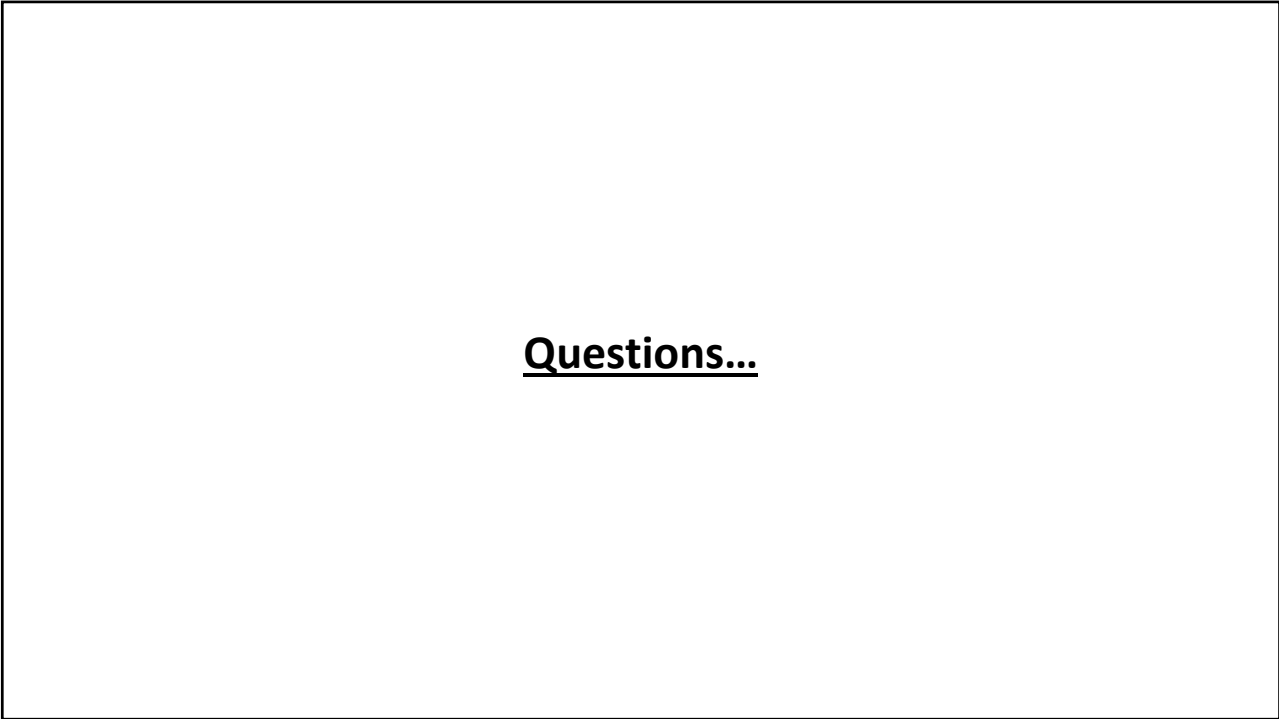
A safety factor of about 1.5 appears to be reasonable when using the Ultimate Strength Design method for wind uplift design

Mark S. Graham
CRCA/IIBEC-Chicago "Roofing Week in Chicago"
January 22, 2021

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The Designer has the authority/responsibility to determine an appropriate safety factor (if any)... and it should be clearly indicated

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