

Theory of SR Motor Operation

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About the instructor

- Companies worked for include:
 - Honeywell
 - Pacific Scientific
 - General Electric
 - AMC
- Currently
 - Dean Computer Science and Engineering at UVSC
 - consulting under Rocky Mountain Technologies Inc.

About the instructor

- has worked with SR motors since 1992
- has designed and built SR motors/generators and controllers
 - 0.5 kW to 80 kW
 - up to 120,000 RPM
 - 2, 3, 4 and 5 phase motors/controllers
 - military, industrial, consumer products
 - some designs are in the production cycle

Overview

- The history of the SR motor
- SR motor physics
- The design of SR motors
- Controller design for SR motors
- Sensorless control SR motors
- Application considerations

Overview

- The SR motor is an old technology
- The SR motor was invented by Davidson in Scotland in 1838
 - there were no suitable electronics to make the SR feasible at the time
- In 1920 Walker invented the variable reluctance (VR) stepper motor, which shares many features of the modern SR Motor

Overview

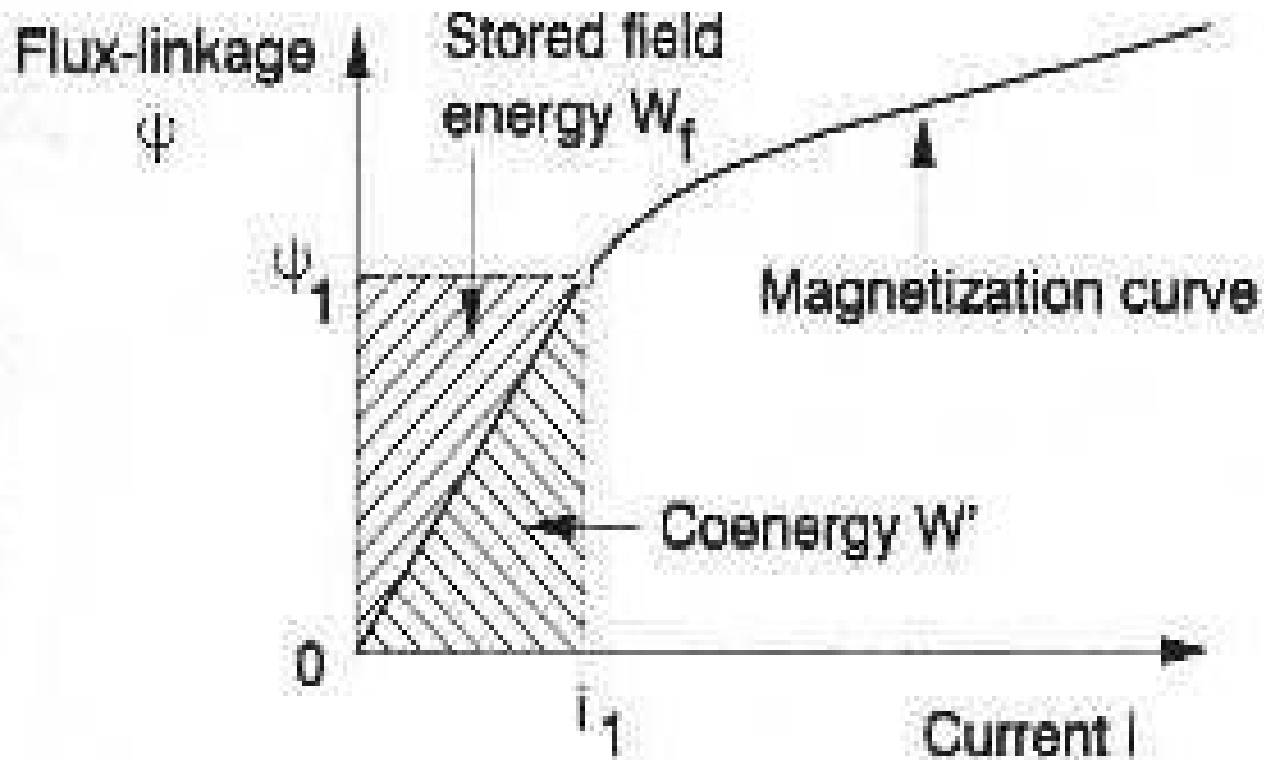
- In 1971 Bedford and Hoft filed US patents on the modern Switched Reluctance Motor
- Hewlett Packard used the first Switched Reluctance Motor in a volume application for the DraftMaster plotter
- Today several manufacturers have introduced successful SR products

SR motor physics

SR motor physics

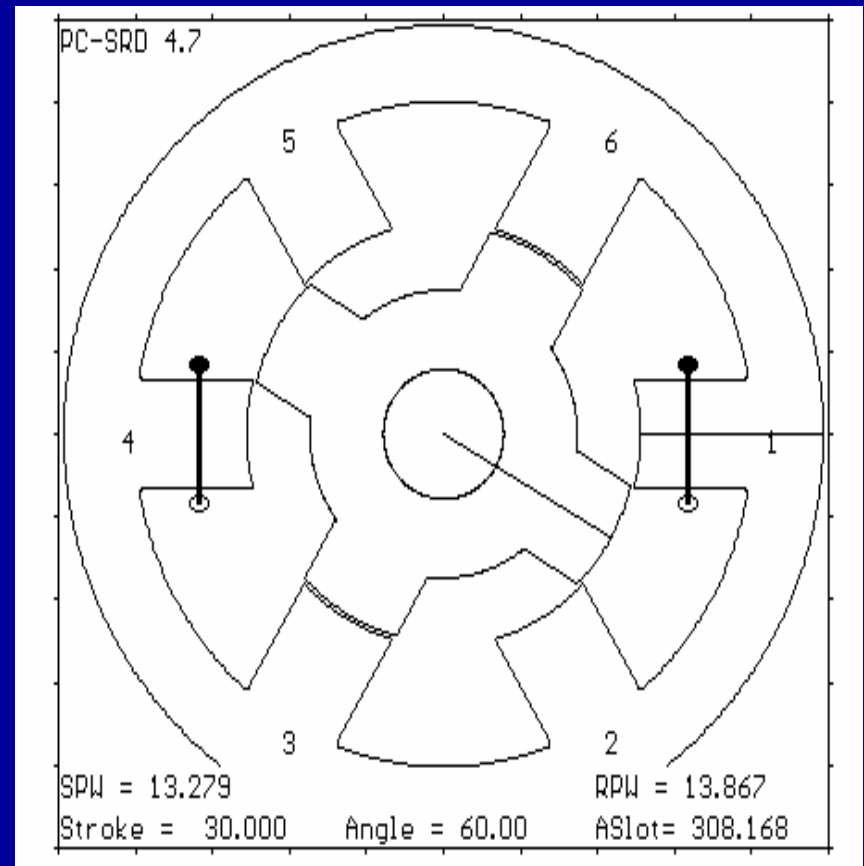
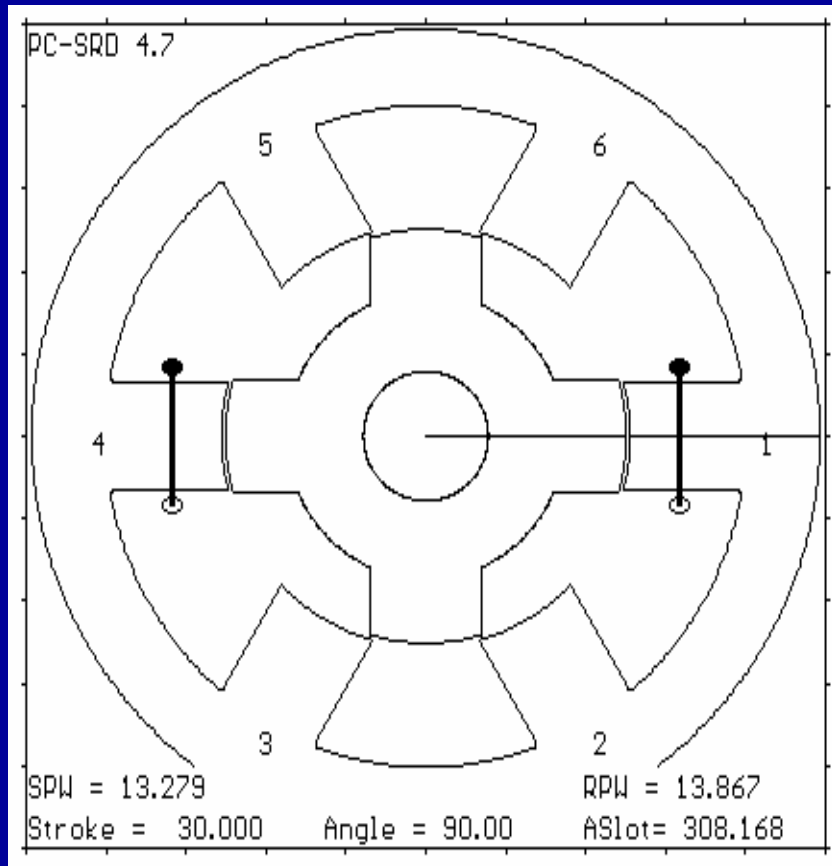
- The physical principle on which the VSR motor operates is that every magnetic circuit tries to maximize its stored energy

SR motor physics



Definition of coenergy W' and stored field energy W_f

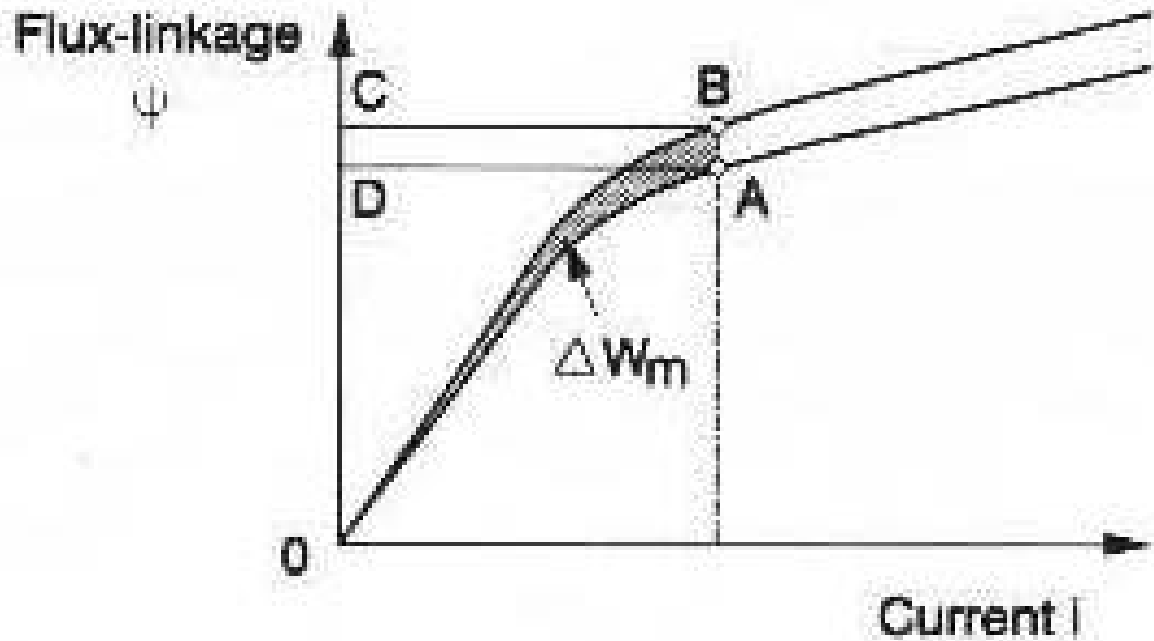
SR motor physics



SR motor physics

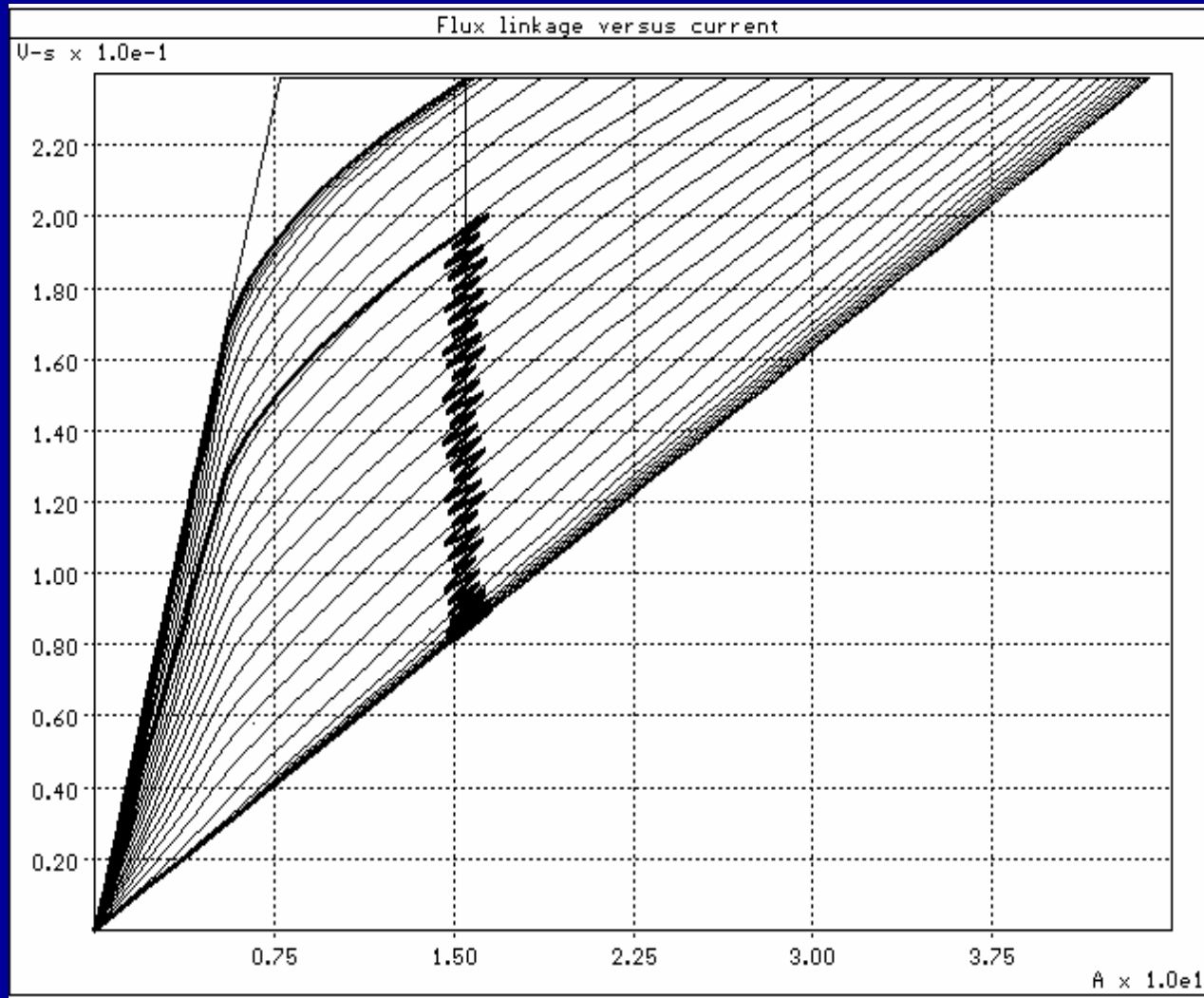
- Terminology
 - aligned position: rotor and stator tooth are aligned
 - un-aligned position: rotor and stator tooth are most unaligned between two neighboring phases
 - absolute torque zone: phase produces non-zero torque
 - effective torque zone: phase produces positive torque
 - regular SR motor: rotor and stator poles are equally spaced

SR motor physics



Calculation of instantaneous torque from the rate of change of coenergy at constant current

SR motor physics



SR motor physics

- The SRM generates torque in all regions where

$$\frac{dL(i, \Theta)}{d\Theta} \neq 0$$

- The inductance L is a function of the current i (saturation) and the angle of rotation Θ :

$$L = L(i, \Theta)$$

SR motor physics

- It is possible to build an SR motor without saturation in the motor's steel
 - the power density will be low

$$T = \frac{1}{2} \cdot i^2 \frac{dL}{d\Theta}$$

SR motor physics

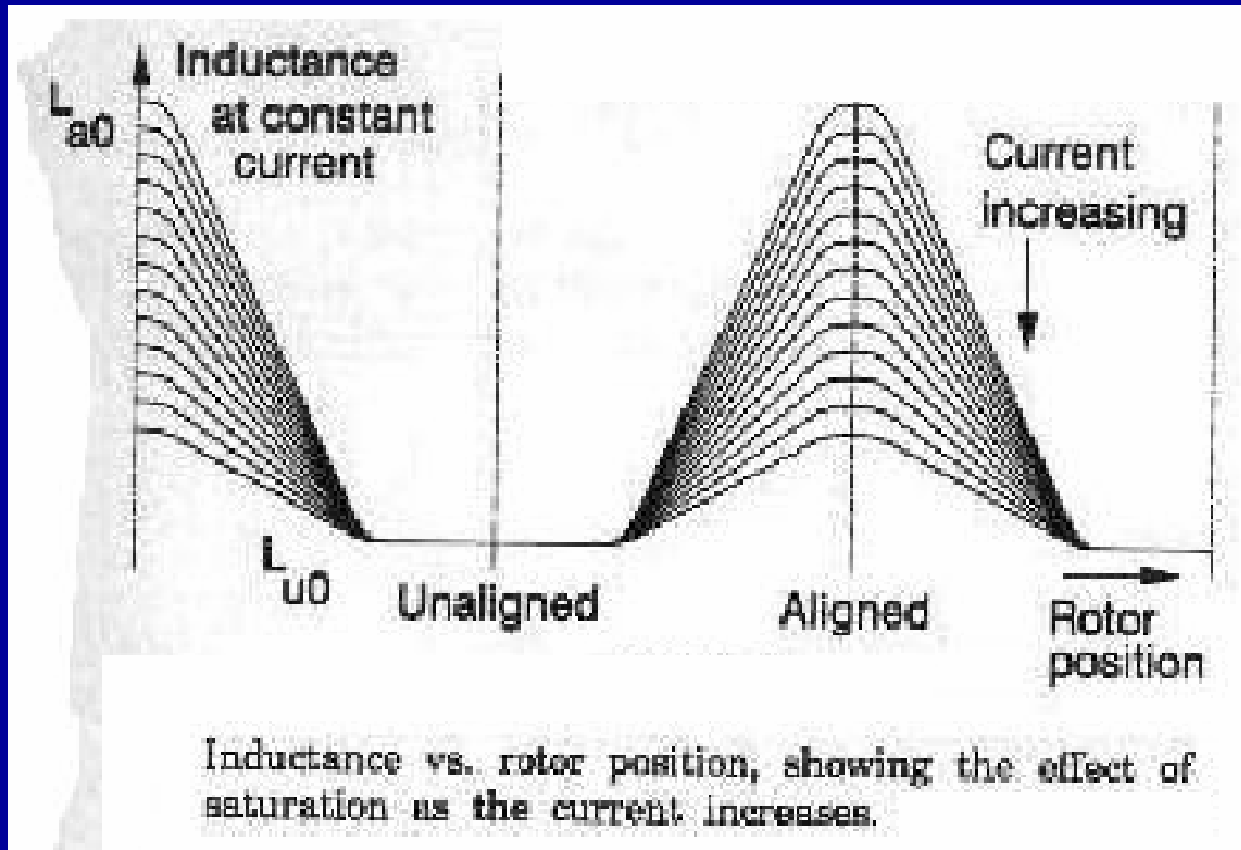
- Typically a SR motor will operate with heavily saturated steel
 - efficient SR motors require high saturation in the motor's steel
 - high quality steels must be used to limit the magnetization and eddy current losses in the steel
 - the ratio of the inductance in the aligned vs. the unaligned position yields information about the performance of the SR motor

SR motor physics

- The torque generated by the SR motor is a function of its rotor angle and the current

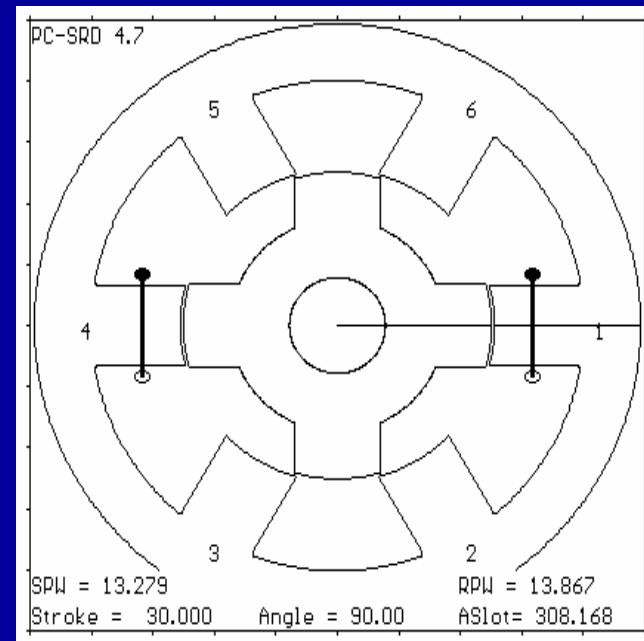
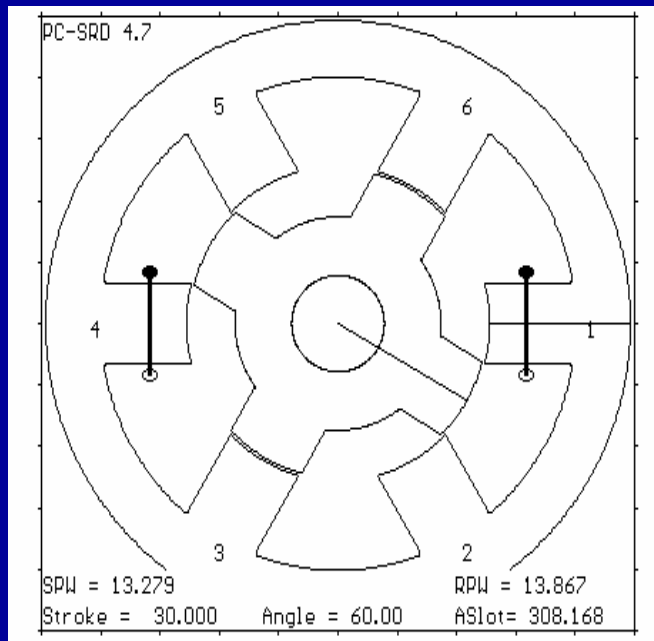
$$T = f(i, \Theta) = \frac{\partial W}{\partial \Theta}$$

SR motor physics

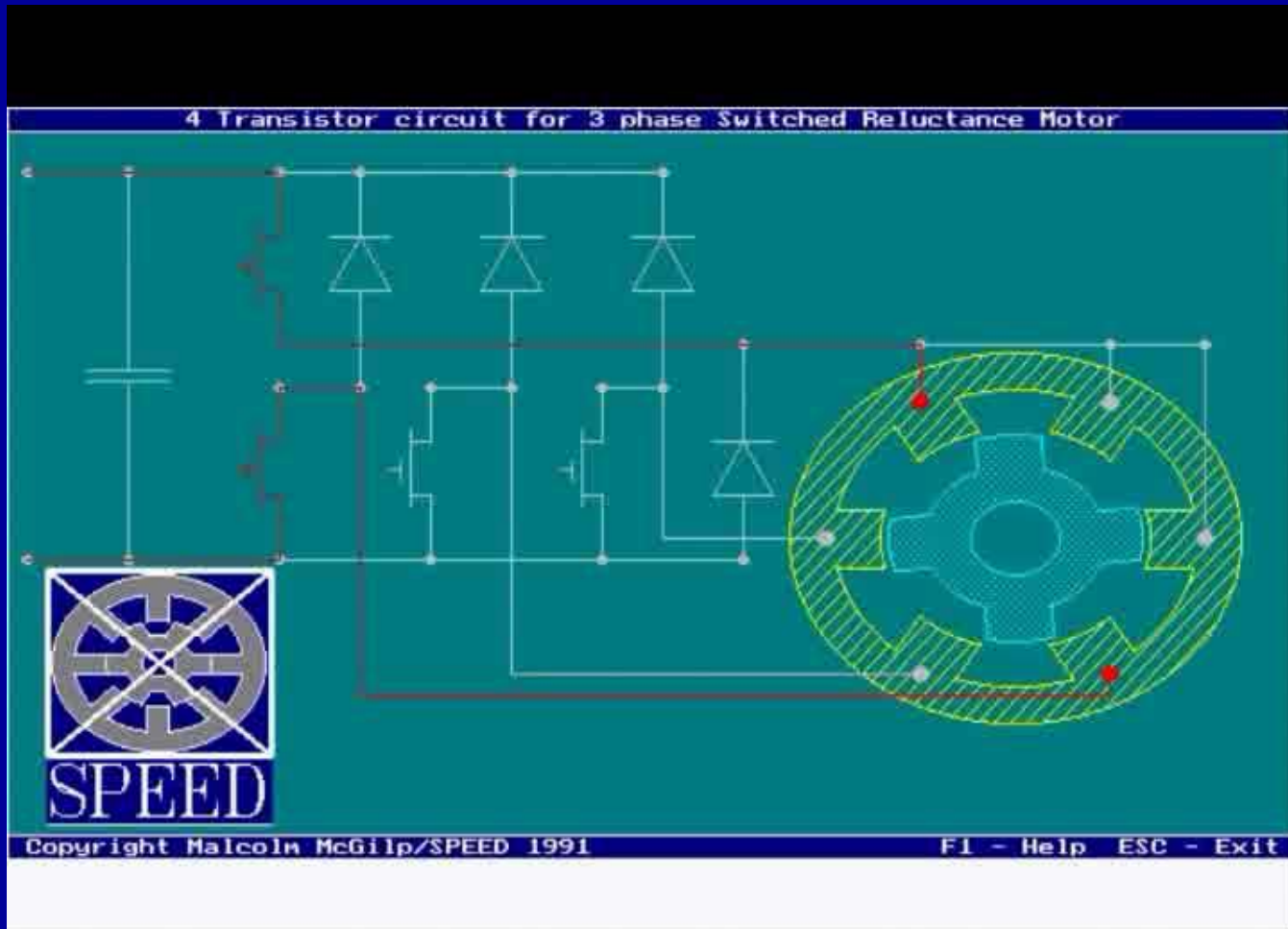


SR motor physics

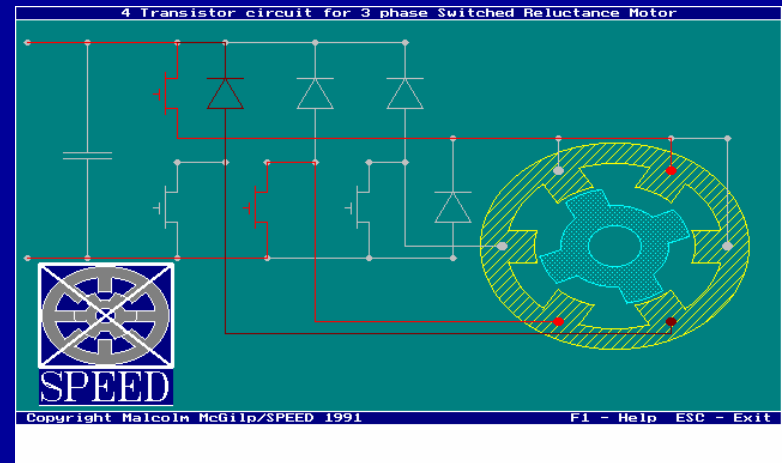
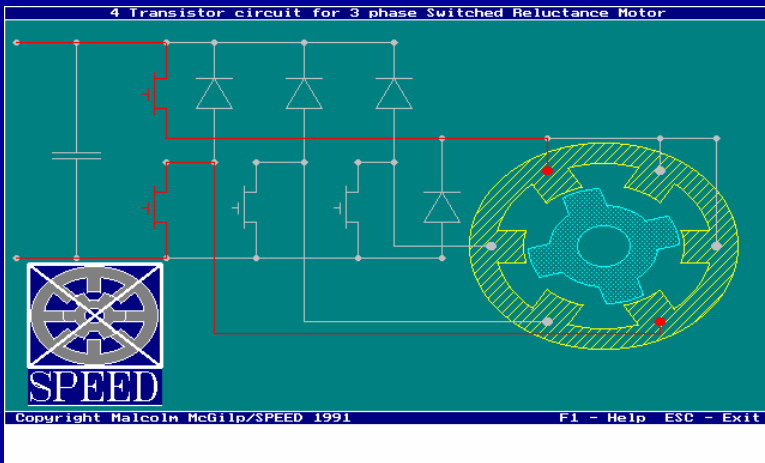
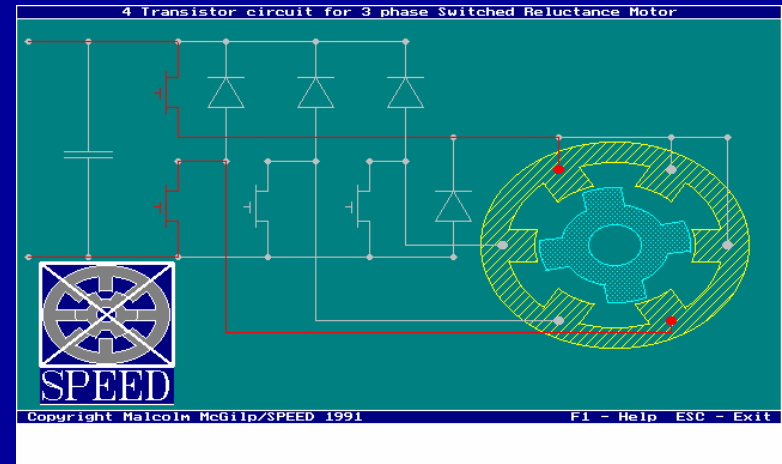
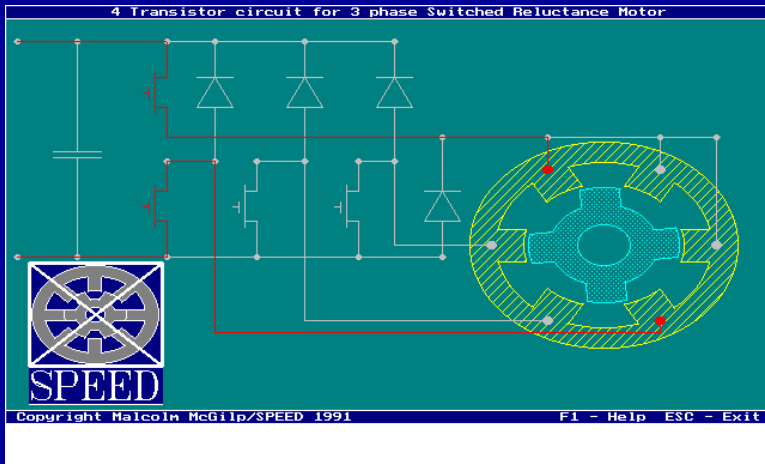
- The rotation of the SR motor is achieved by sequentially energizing and de-energizing the phases of the motor



SR motor physics



SR motor physics



SR motor physics

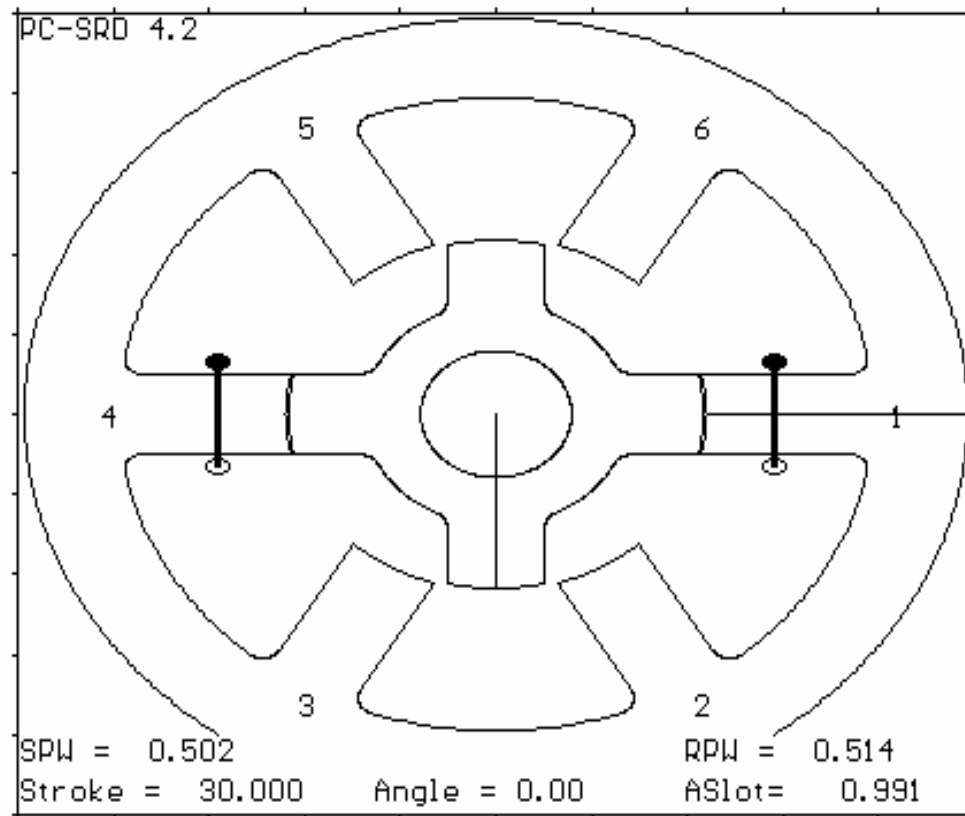
- A clockwise sequential excitation of the phases results in a counter clockwise rotation of the SR motor

SR motor physics

- Example of a typical 3 phase SR motor

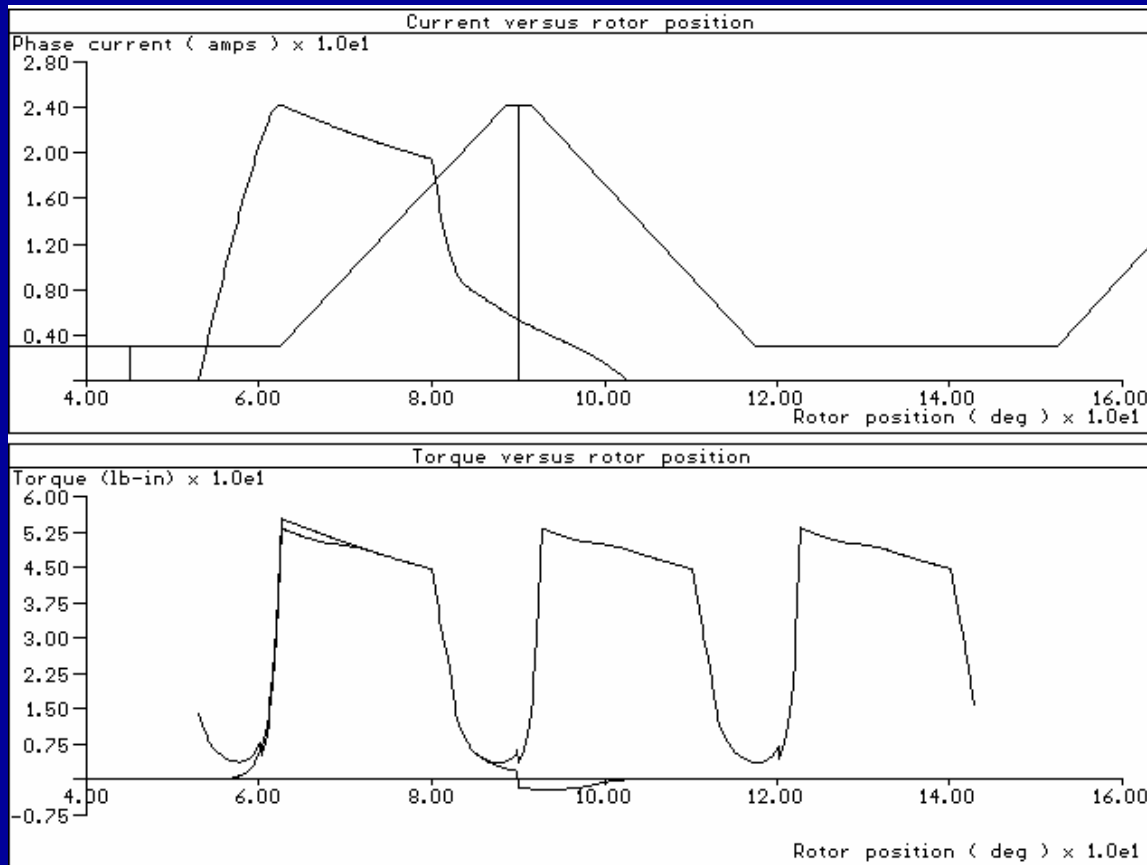
```
in. & mech°  
Rsh.. > 0.4000  
R0... 0.7000  
R1... 1.1000  
Gap.. 0.0150  
R2... 2.0000  
R3... 2.5000  
Ns... 6.0000  
Nr... 4.0000  
BetaS 26.0000  
BetaR 27.0000  
tpr_S 0.0000  
tpr_R 0.0000  
fil_S 0.1000  
fil_R 0.1000  
D1s.. 0.0000  
D2s.. 0.0000  
Ntp.. 1.0000  
LStk. 3.0000  
Angle 0.0000
```

```
Draw      Save  
Quit      Help
```



SR motor physics

- The torque profile



SR motor physics

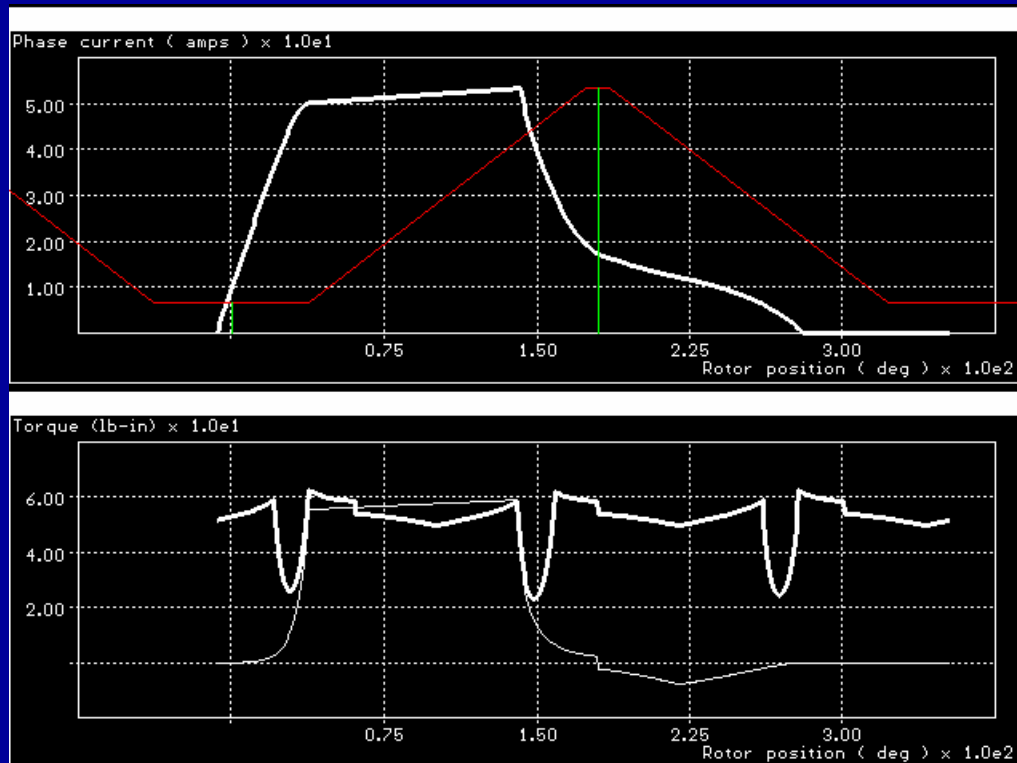
- All of this sounds just like a VR stepper, what is so special about the SR motor ???
 - answer: the SR motor is a self commutated motor
 - in the SR motor the field follows the rotor. T
 - the rotor position determines which phase will be energized.
 - this is called: closed loop commutation
 - in contrast operation of the stepper motor assumes that
 - in the stepper motor the rotor follows the field
 - stability problems result
 - the rotor may lose steps and/or stall

SR motor physics

- closed loop commutation requires that:
 - rotor position feedback must be provided
 - rotor position feedback must be used for commutation
 - commutation angles may not be fixed and constant
 - technology is available to determine the rotor position of the SR motor without adding physical position sensors:
sensorless control

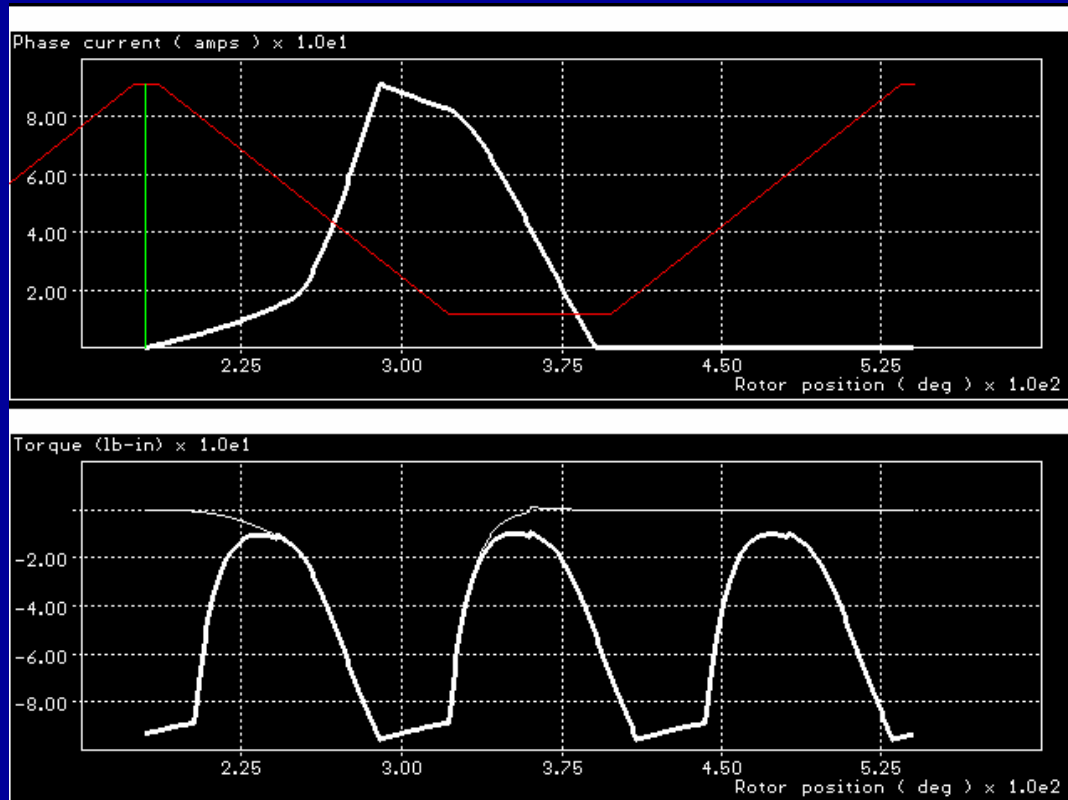
SR motor physics

- The SR motor can operate both as a motor



SR motor physics

- and a generator



SR motor physics

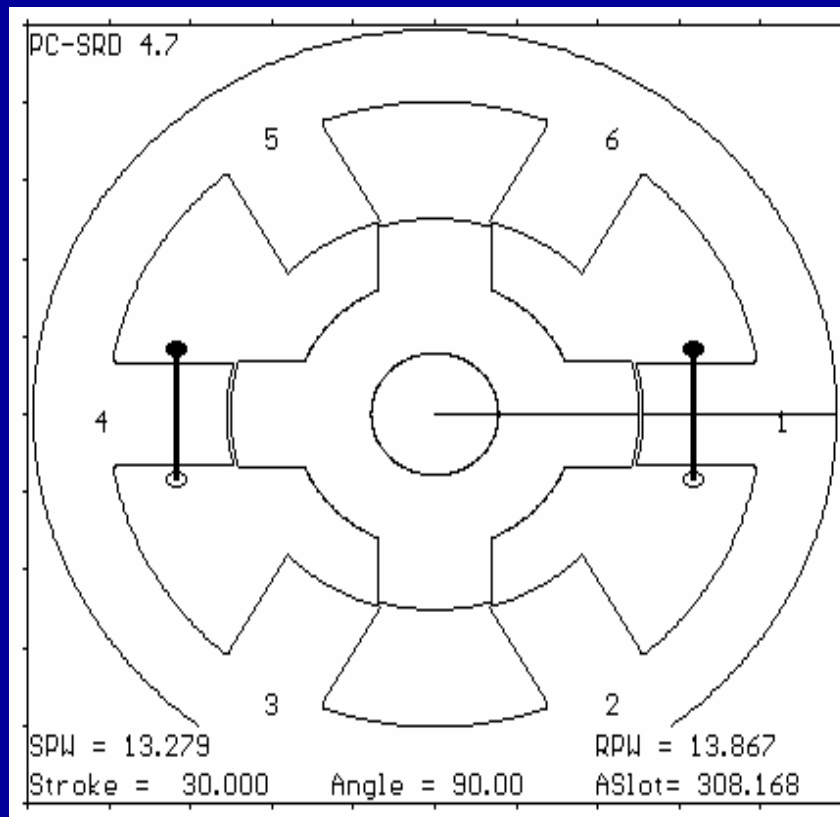
- the SR Generator is a current source
 - generation process needs energy to be excited
 - once the phase is exited it is difficult to control the generation process
 - unlike other technologies a well designed SR motor is not necessarily a good generator

SR motor physics

- the phase/pole combinations in the SR motor
 - a typical SR motor is referenced as an x/y n-phase
 - x = number of rotor poles
 - y = number of stator poles
 - n = number of phases
 - the number of rotor and stator poles must be different to allow a motor to generate torque at stall
 - x = y is possible for a generator or a specialized application
 - typically $y = x - 2$ but other combinations are possible
 - the number of stator poles is an integral multiple of the number of phases
 - $x = n * m$; $m = 2, 4, 6 \dots$

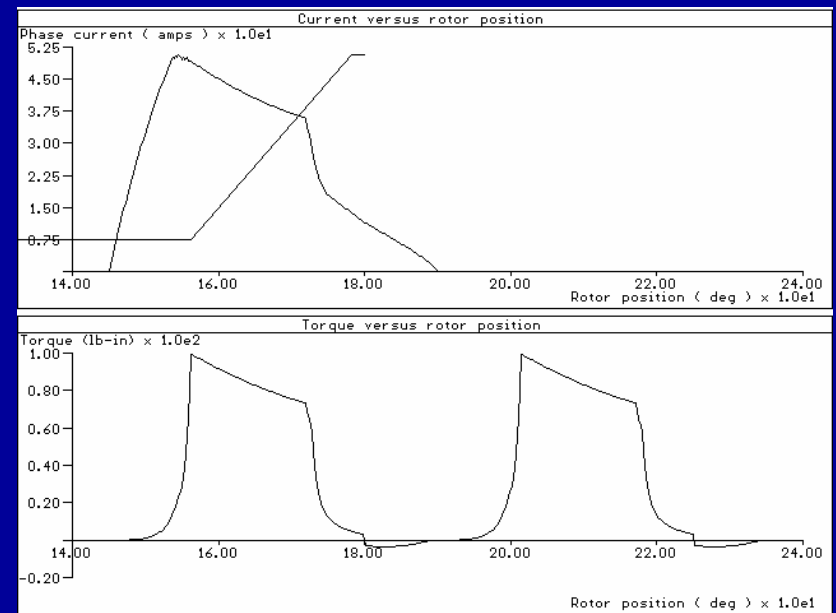
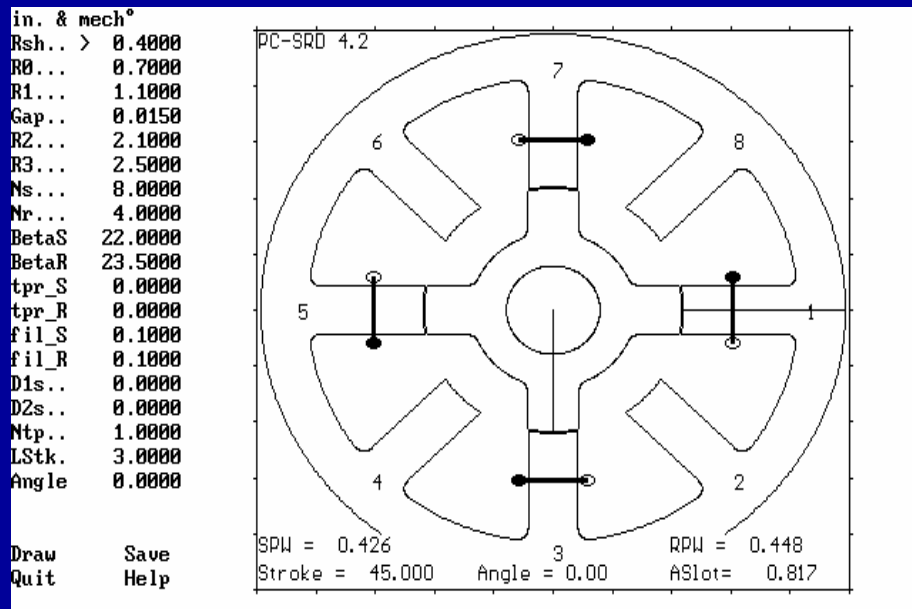
SR motor physics

- example of a 6/4 3 phase motor



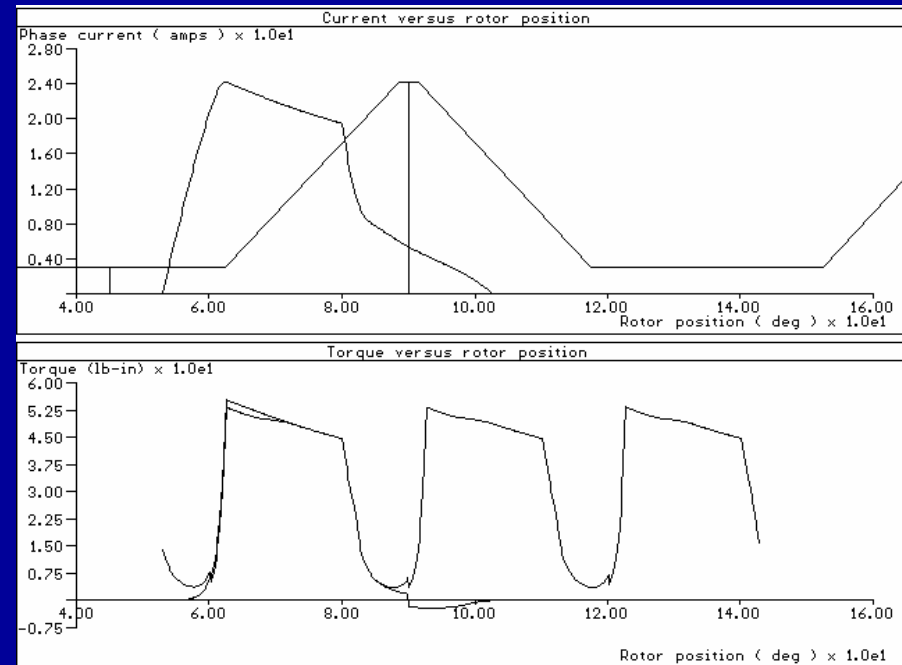
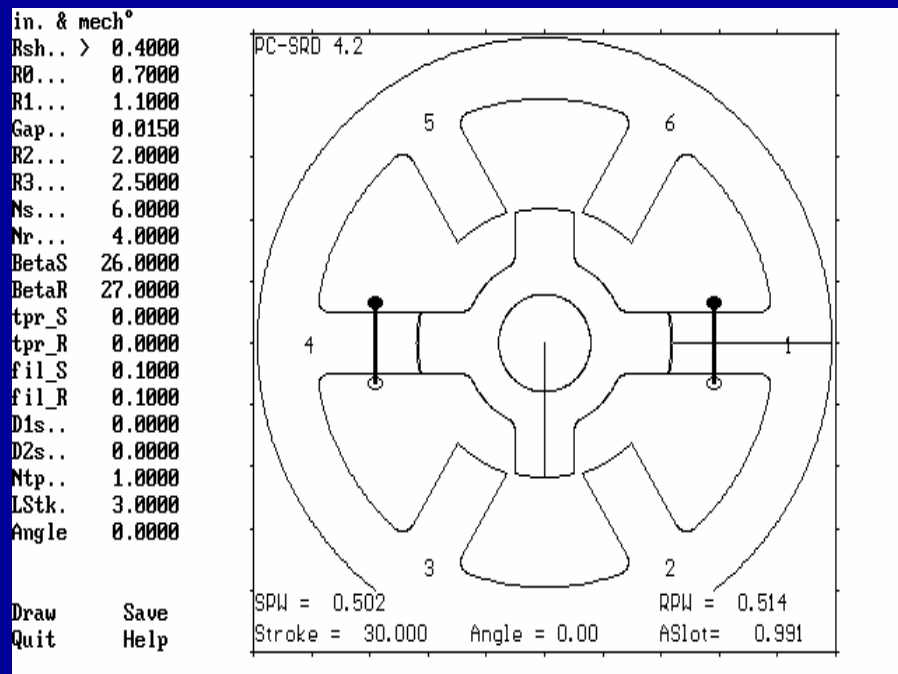
SR motor physics

- the 8/6 2 phase motor



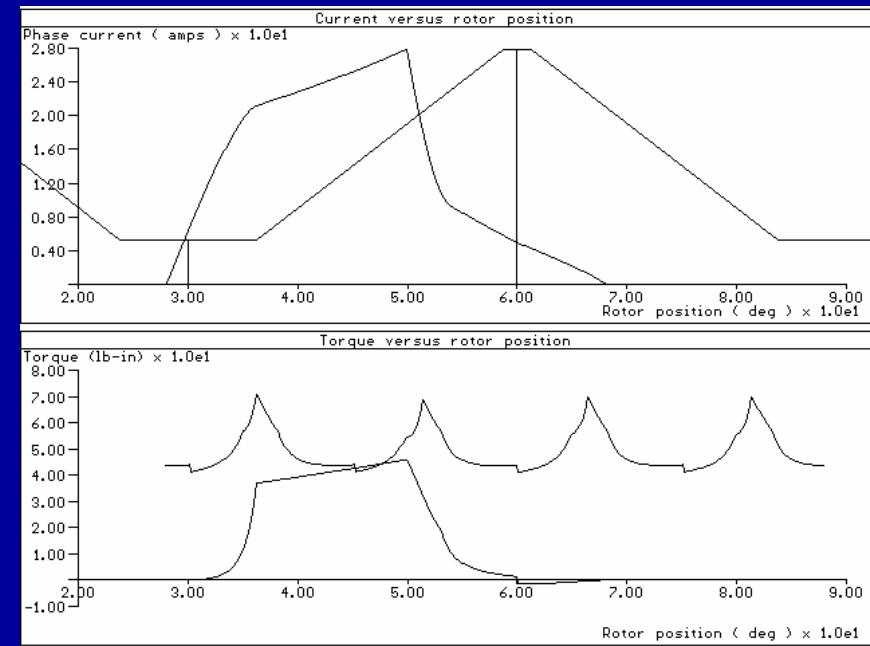
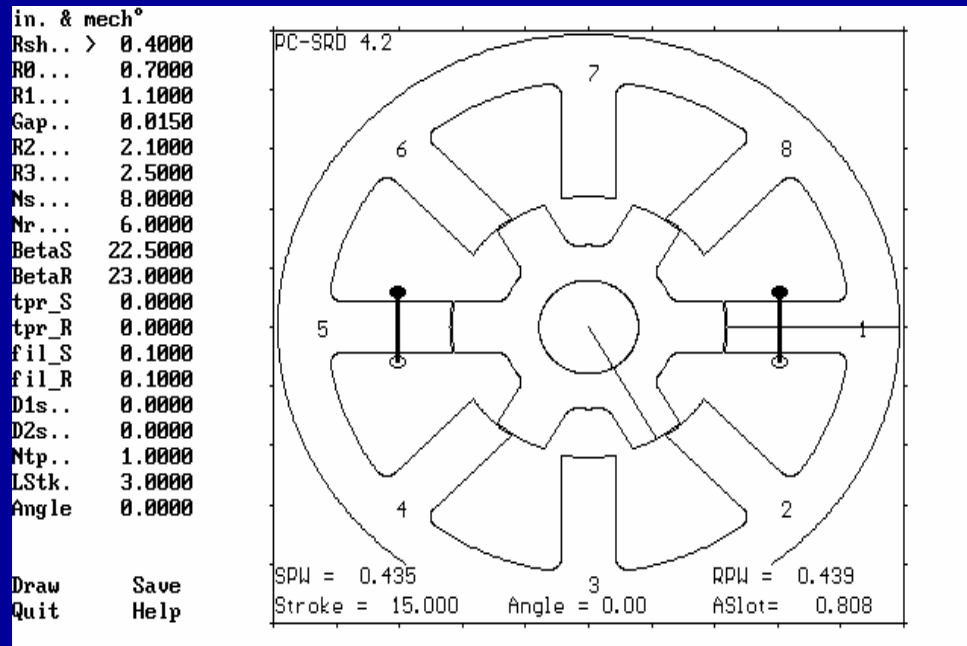
SR motor physics

- the 6/4 3 phase motor



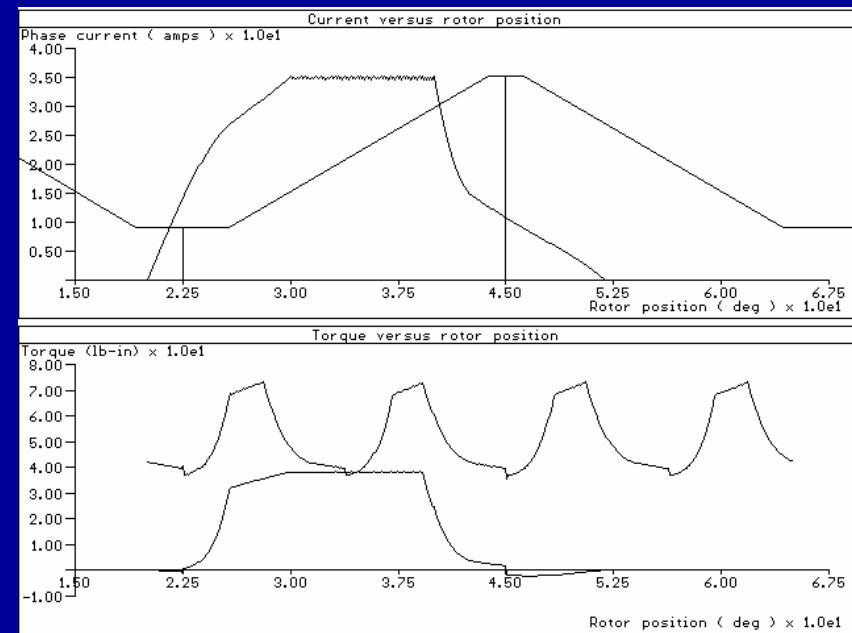
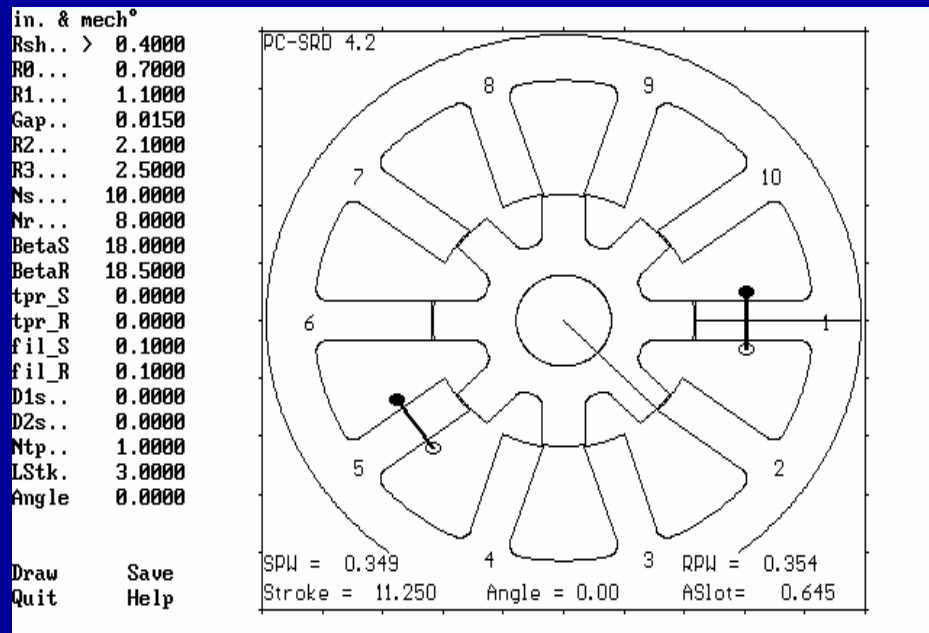
SR motor physics

- the 8/6 4 phase motor



SR motor physics

- the 10/8 5 phase motor



SR motor physics

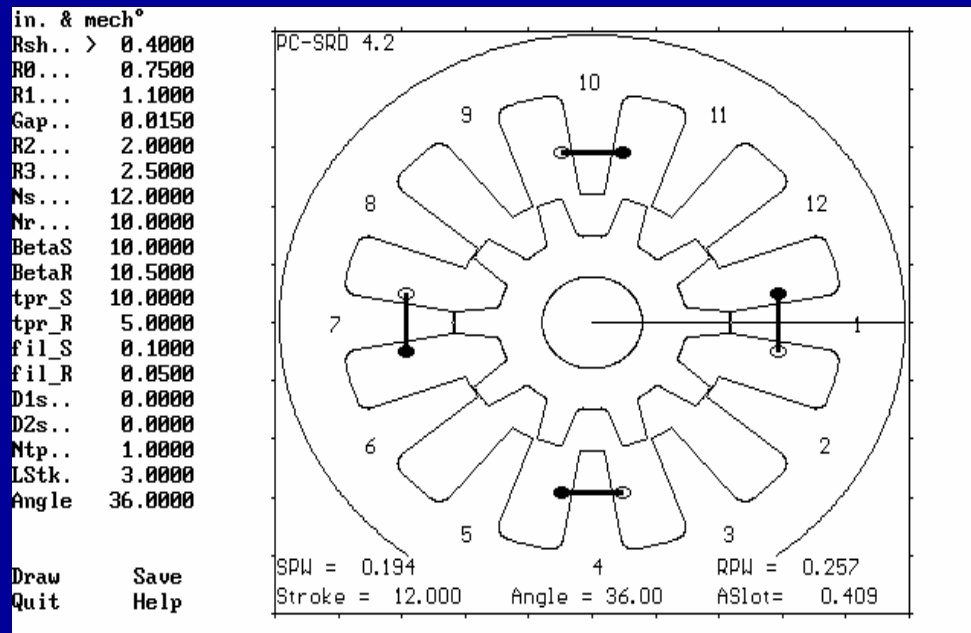
- acoustic noise in SR motors
 - the magnetic forces are strong enough to force the teeth to elongate and to distort the stator yoke
 - the radial forces are significantly higher than the tangential forces (torque) by a factor of 10:1 or more
 - a small airgap can aggregate the problem due to mechanic tolerances

SR motor physics

- acoustic noise in SR motors
 - the rate of change in the magnetic field has an impact on the acoustic noise
 - geometry, mechanical construction and electronic control schemes can be used to reduce acoustic noise

SR motor physics

- acoustic noise in SR motors
 - the 12/10 3 phase SR motor
 - short flux path
 - good force distribution
 - patented design



SR motor physics

- acoustic noise in SR motors
 - tooth design can help to reduce the acoustic noise
 - strong backiron in the stator can help to reduce the acoustic noise
 - a large airgap can help to reduce the acoustic noise

SR motor physics

- acoustic noise in SR motors
 - commutation is critical: turn on early, turn off late when the inductance is highest (if possible)
 - tradeoff: efficiency vs. quiet operation
 - Polluck has described and patented a scheme to turn the phase off in 2 steps
 - must be tuned to the motor's natural frequency
 - mixed results have been reported

SR motor physics

- acoustic noise in SR motors
 - measurements in actual systems show that BLDC and SR are similar in audible noise (within 3 dB)
 - the emitted audible spectra are different between a BLDC and an SR motor
 - SR has a more defined spectrum
 - can be used as an advantage
 - can be mechanically suppressed

SR motor physics

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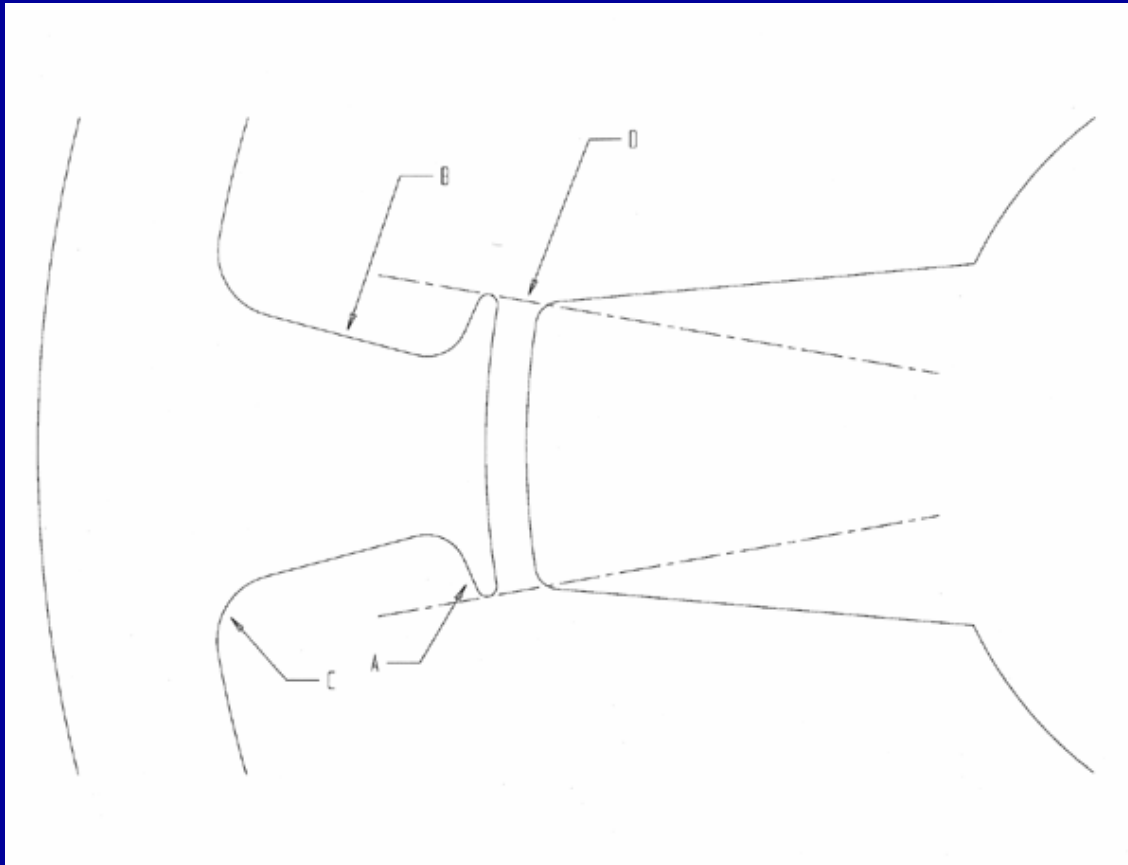
The design of SR motors

The design of SR motors

- the mechanical and magnetic design of the SR motor is of extreme importance

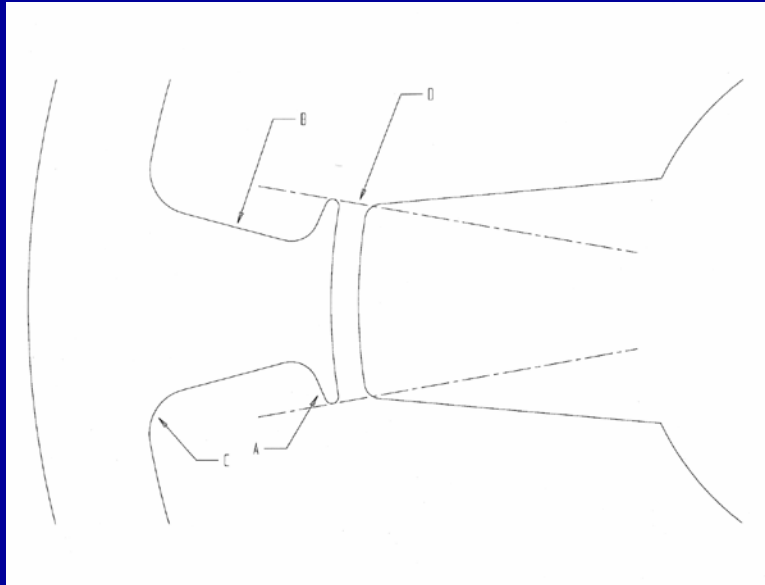
The design of SR motors

- geometric considerations



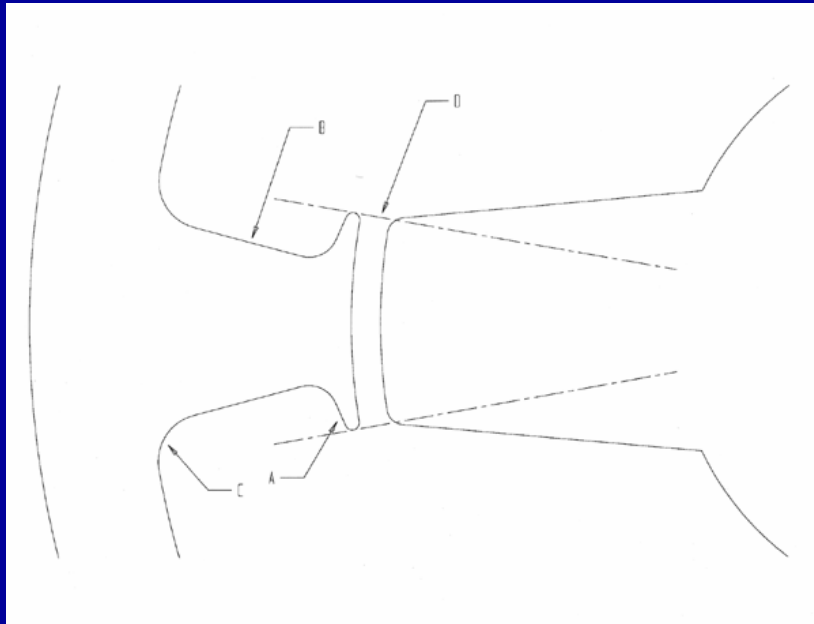
The design of SR motors

- geometric considerations
 - wide rotor tooth tip
 - improved saturation pattern
 - more winding space



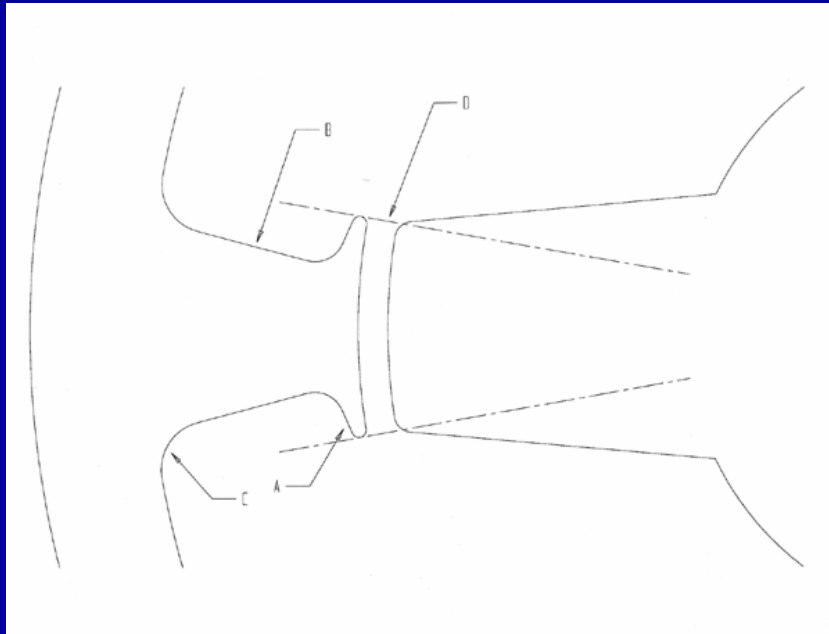
The design of SR motors

- geometric considerations
 - angled stator tooth
 - improved magnetics
 - Improved mechanic integrity
 - improved acoustic noise



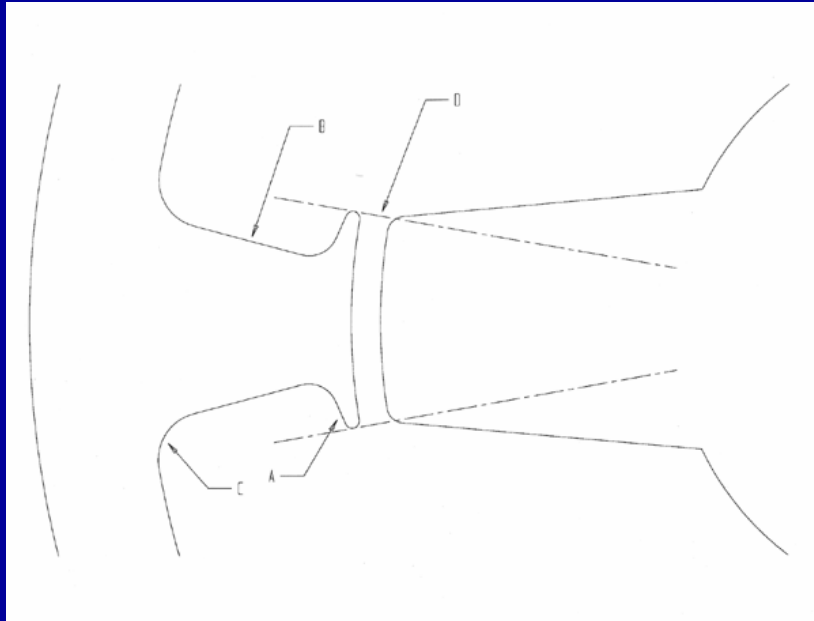
The design of SR motors

- geometric considerations
 - chamfered transitions
 - reduced mechanical stress



The design of SR motors

- geometric considerations
 - angled rotor tooth
 - reduced inertia
 - improved magnetics
 - Improved mechanical integrity



The design of SR motors

- the airgap
 - an airgap of 0.01” is typical for most SR motors
 - many designers believe that an SR motor can not be designed with a large airgap
 - SR motors with 0.025” – 0.04” have been successfully build and demonstrated
 - loss in efficiency is as low as 0.5% increasing the airgap from 0.01” to 0.03”

The design of SR motors

- the airgap
 - SR motors with large airgaps reduce some manufacturing problems
 - mechanical tolerances
 - contamination
 - shaft vibration
 - SR motors with large airgaps are more cost effective
 - cost of bearings
 - tolerances

The design of SR motors

- no good mathematical models exist to design or describe the SR motor
- the use of simulation tools and magnetic design software are required for the design of SR motors and systems
- PC-SRD is commonly used for SR motor design
 - developed by the SPEED Consortium
 - software is distributed by Motorsoft in the US

The design of SR motors

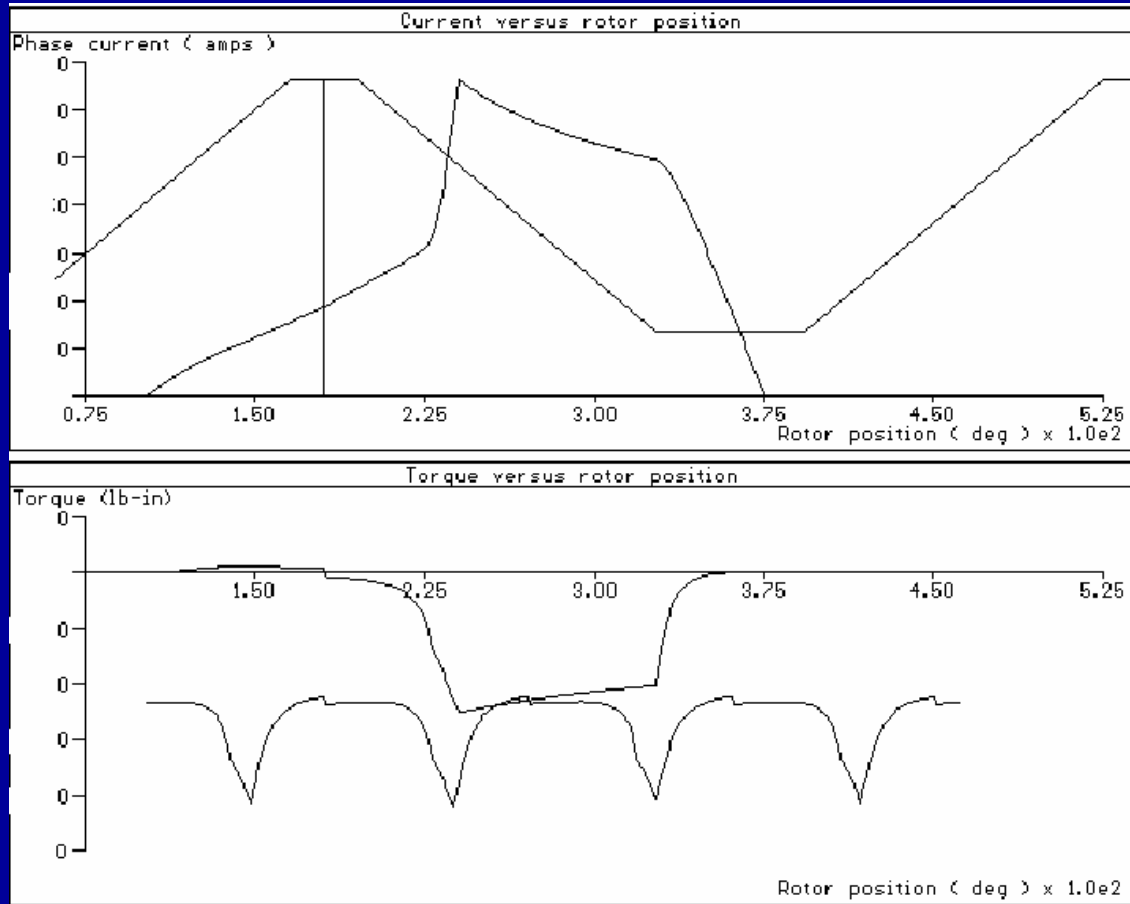
- finite element magnetic (FEM) software can also be used to design and analyze SR motors
 - PC-SRD is a better tool for the initial sizing
 - FEM yields more valid results

The design of SR motors

- both tools were used simultaneously in one instance to design an 80kW generator
 - initial sizing was done using PC-SRD
 - due to the cost of the prototypes (~ \$100k) additional performance assurance was desired
 - MAGSOFT FEM software was used to validate the result
 - the FEM confirmed the general performance but indicated some minor, favorable differences in the torque distribution
 - measurements performed on the actual generator confirmed both the overall performance as well as the torque distribution closer to the one predicted by FEM

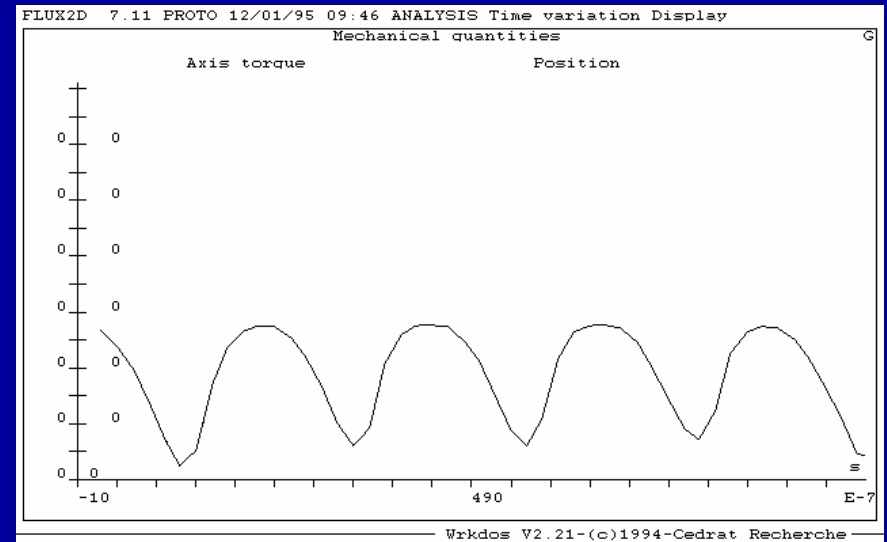
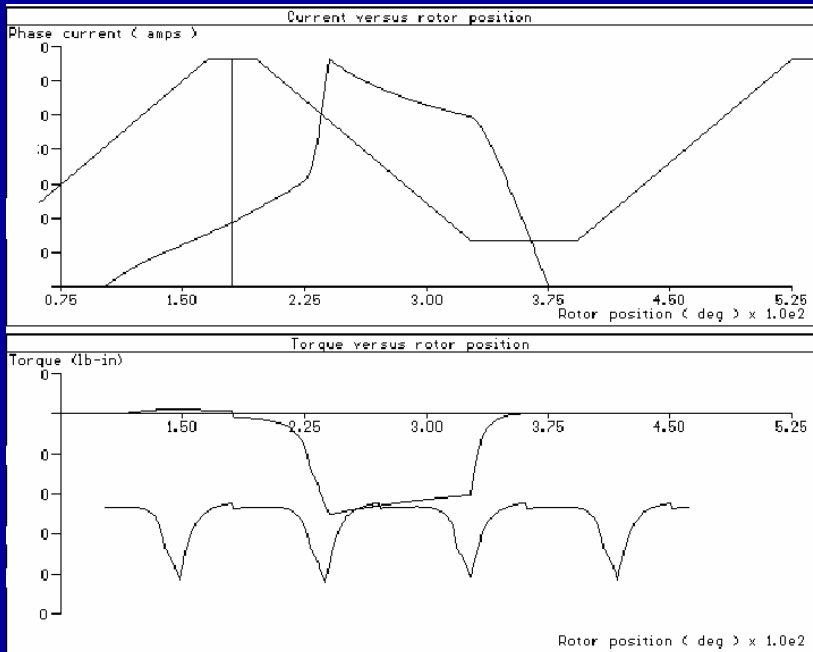
The design of SR motors

- the design as predicted by PC-SRD



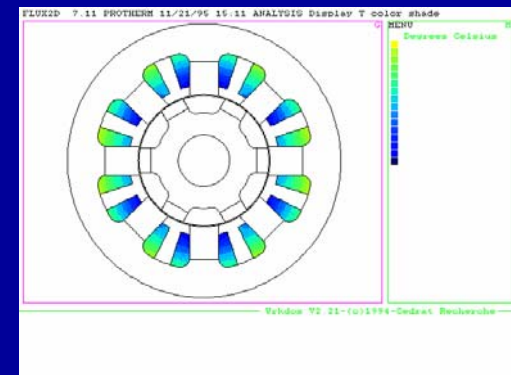
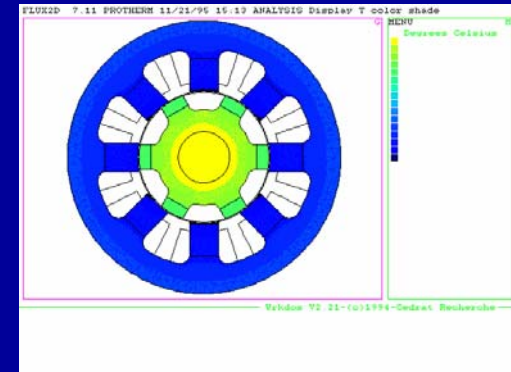
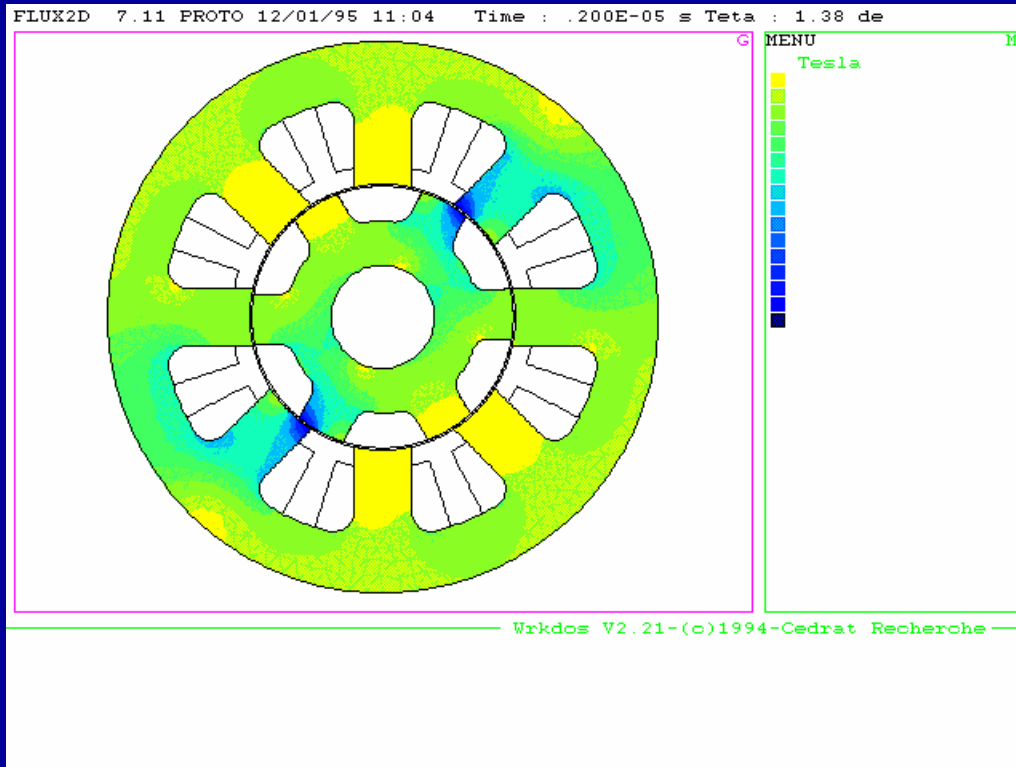
The design of SR motors

- comparison of the results



The design of SR motors

- magnetic saturation and operating temperature as predicted by FLUX2D



The design of SR motors

- SR motors require high quality steel
- Asian manufacturers often have problems providing quality steel with consistency
- M-17 and M-19 are typically used, M-15 is a good steel for high speed motors
- very high performance motors use Hyperco and Vanadium Permendur steels

The design of SR motors

AISI Designation	Allegheny Ludlum Designation	General Use
M-6	Silectron 66	Lowest core loss at high induction for use in power & distribution transformers and large turbogenerators.
M-14	Transformer AA	Low core loss transformer steel for high efficiency rotating machines and transformers
M-15	Transformer A	Higher core loss than M-14 Used for distribution transformers & rotary machines
M-17	Transformer B	Used occasionally for power transformers
M-19	Transformer C	Most suitable for high performance servo motors
M-22	Dynamo Special	Most suitable for high performance induction motors
M-27	Dynamo	Popular grade for servo motors
M-36	Electrical	Used especially for rotary machines. Popular grade for permanent magnet motors.
M-43	Armature	Used for fractional horsepower motors and relays
M-50	Field	Used for pole pieces and intermittent electric devices

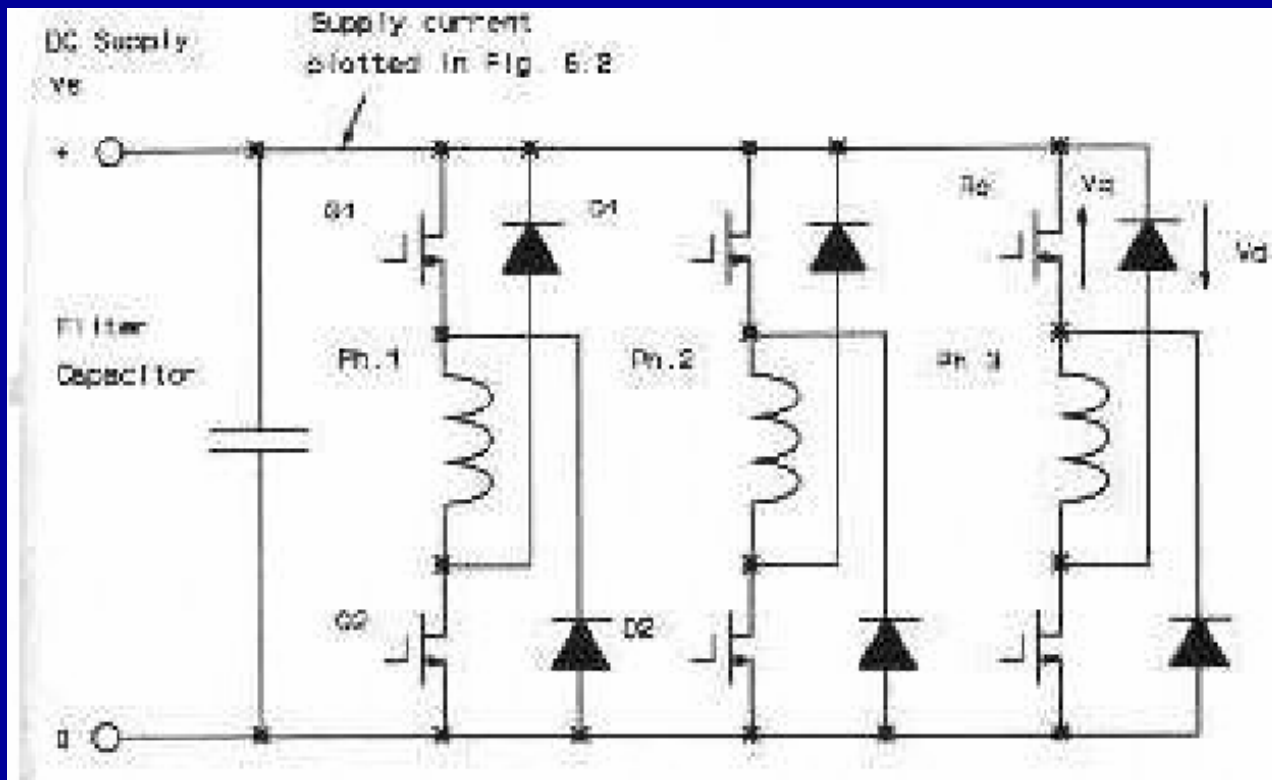
The design of SR motors

- “inside out” and linear SR motor designs are possible although more difficult than in PMBL motors
- pancake motors are typically inefficient
- best results are obtained when the stacklength equals the diameter although motors from $\frac{1}{2}$ to 2 times this “ideal” stacklength perform well

Controller design for SR motors

Controller design for SR motors

- the typical power stage configuration for a 3 phase SR motor controller is shown here

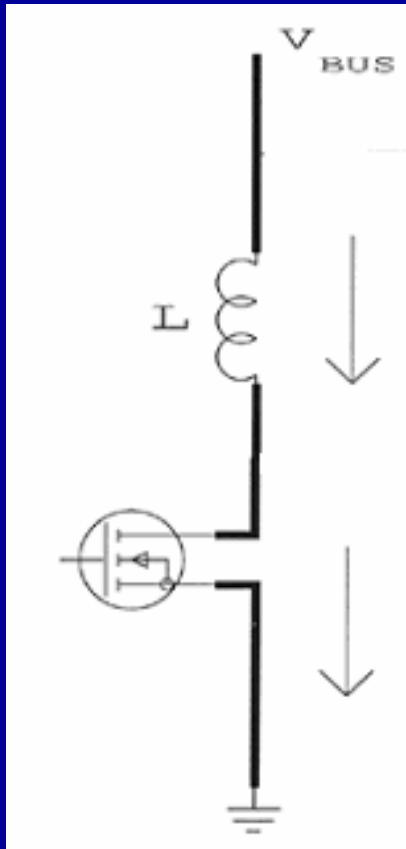


Controller design for SR motors

- the phases in the SR motor are typically independently controlled
 - methods have been introduced that allow to use a “standard” 3 phase inverter to control an SR motor
 - a controller (inverter) designed to drive an SR motor can be used to drive BLDC motors

Controller design for SR motors

- why not use a single switch ???



Controller design for SR motors

- a mathematical analysis will quickly show the reason

$$V_{bus} = L \cdot \frac{di}{dt} + i \cdot \frac{dL}{d\vartheta} + R \cdot i$$

V_{bus} : supply voltage

L : armature (phase) inductance

R : armature (phase) resistance

ϑ : the angular position of the rotor

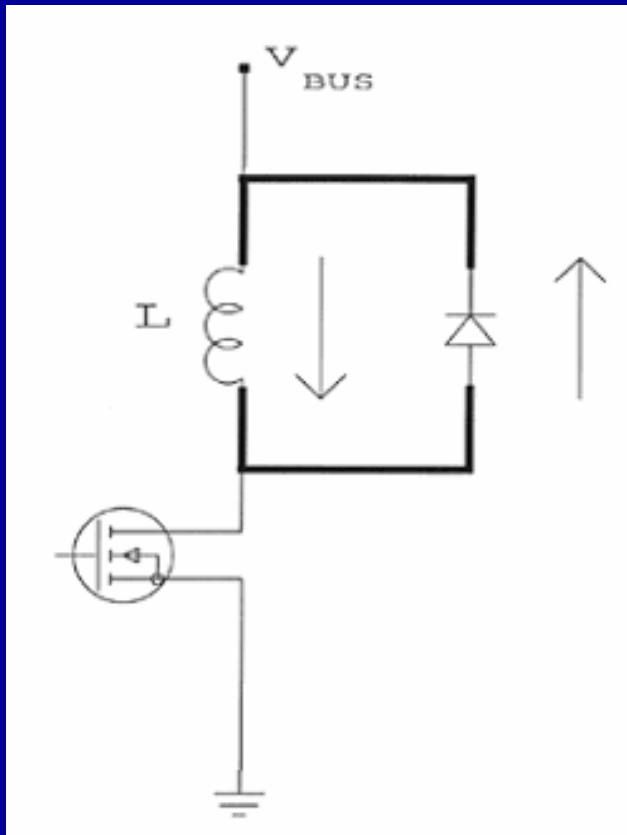
Controller design for SR motors

- solving this when the phase is turned on yields:

$$i(t) = \frac{V_{bus}}{R} \cdot \left(1 - e^{-\frac{t}{L/R}} \right) + i(t=0) \cdot e^{-\frac{t}{L/R}}$$

Controller design for SR motors

- what happens when the phase current turns off ???



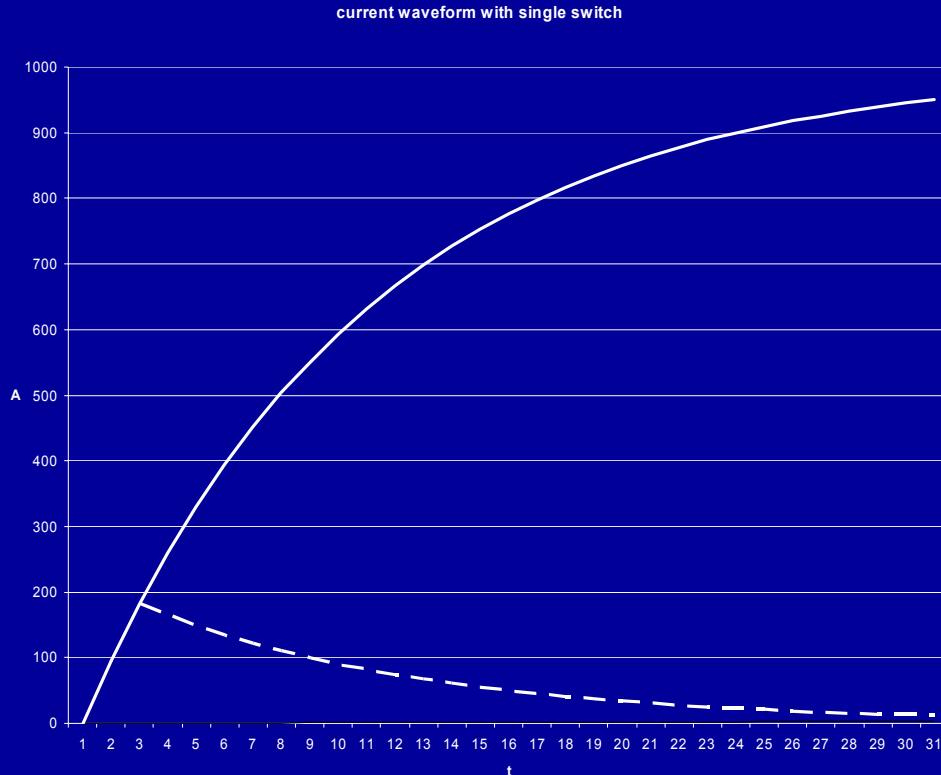
Controller design for SR motors

- solving the equations yields yields:

$$i(t) = -\frac{V_{diode}}{R} \cdot \left(1 - e^{-\frac{t}{L/R}} \right) + i(t=0) \cdot e^{-\frac{t}{L/R}}$$

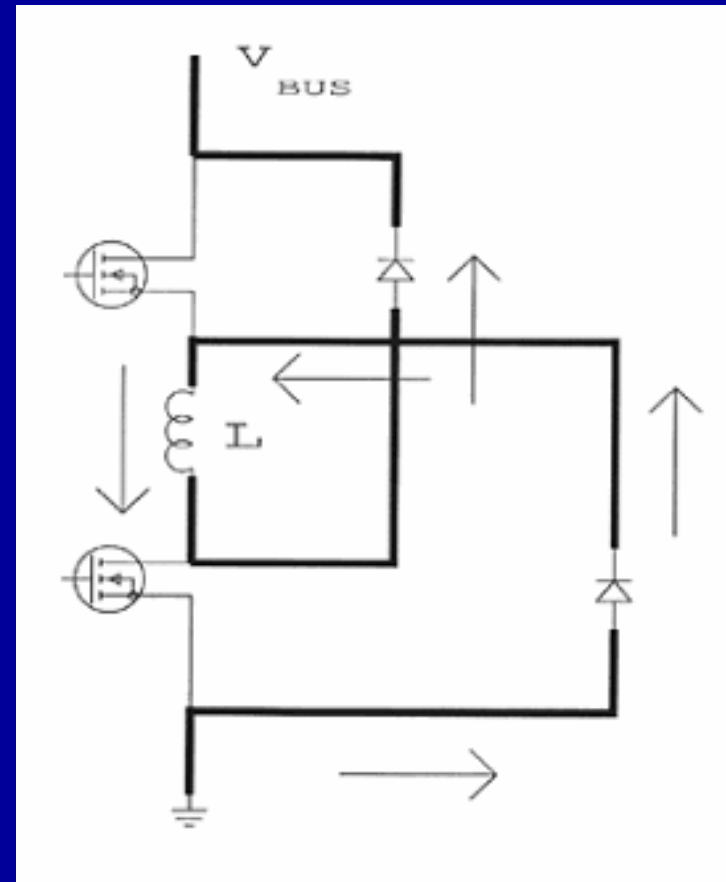
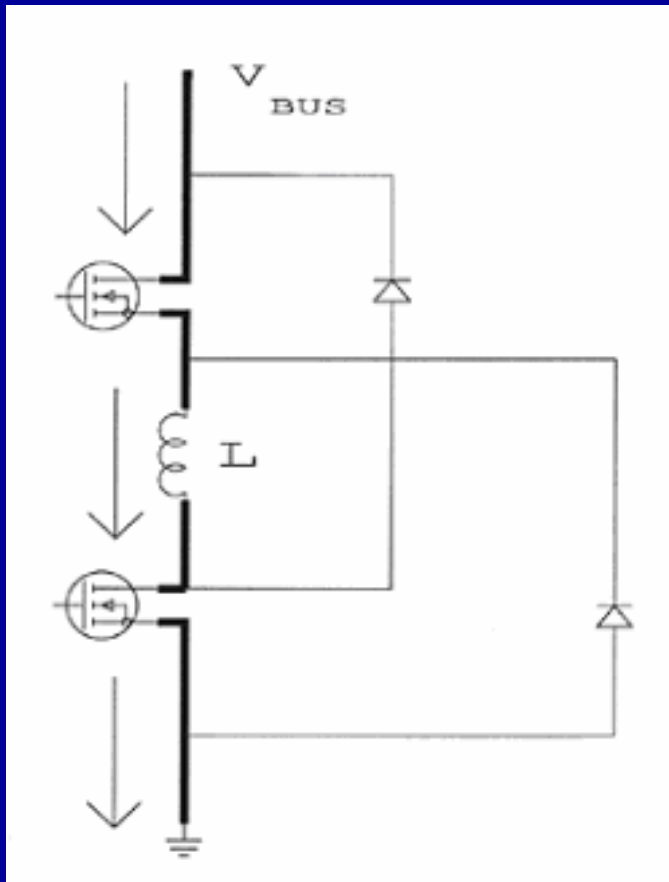
Controller design for SR motors

- solving the equations yields yields:



Controller design for SR motors

- what happens with 2 switches ???



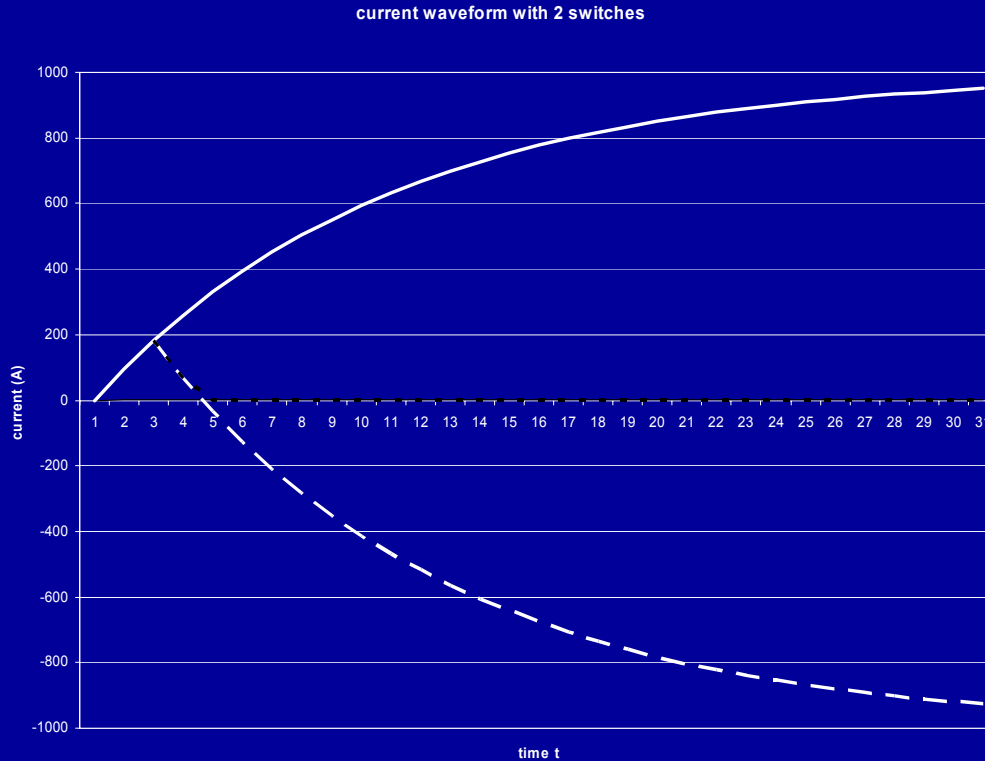
Controller design for SR motors

- the turn on does not change significantly
- solving the turn off yields:

$$\left\{ \begin{array}{ll} i(t) = -\frac{V_{bus}}{R} \cdot \left(1 - e^{-\frac{t}{L/R}} \right) + i(t=0) \cdot e^{-\frac{t}{L/R}} & i > 0 \\ 0 & else \end{array} \right.$$

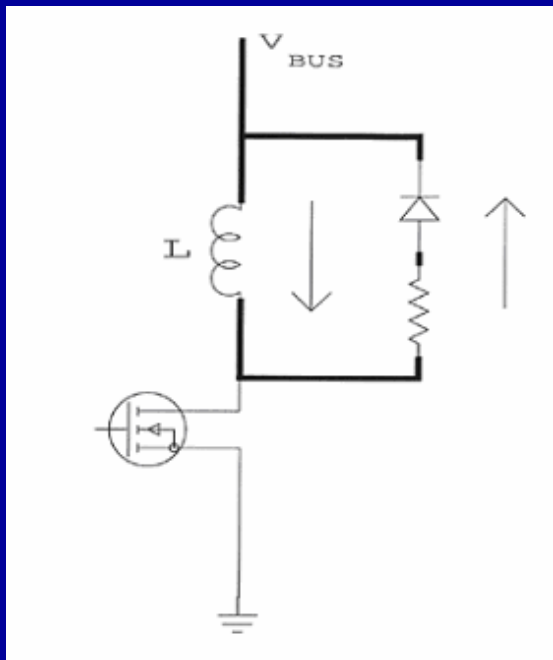
Controller design for SR motors

- solving the equations yields yields:



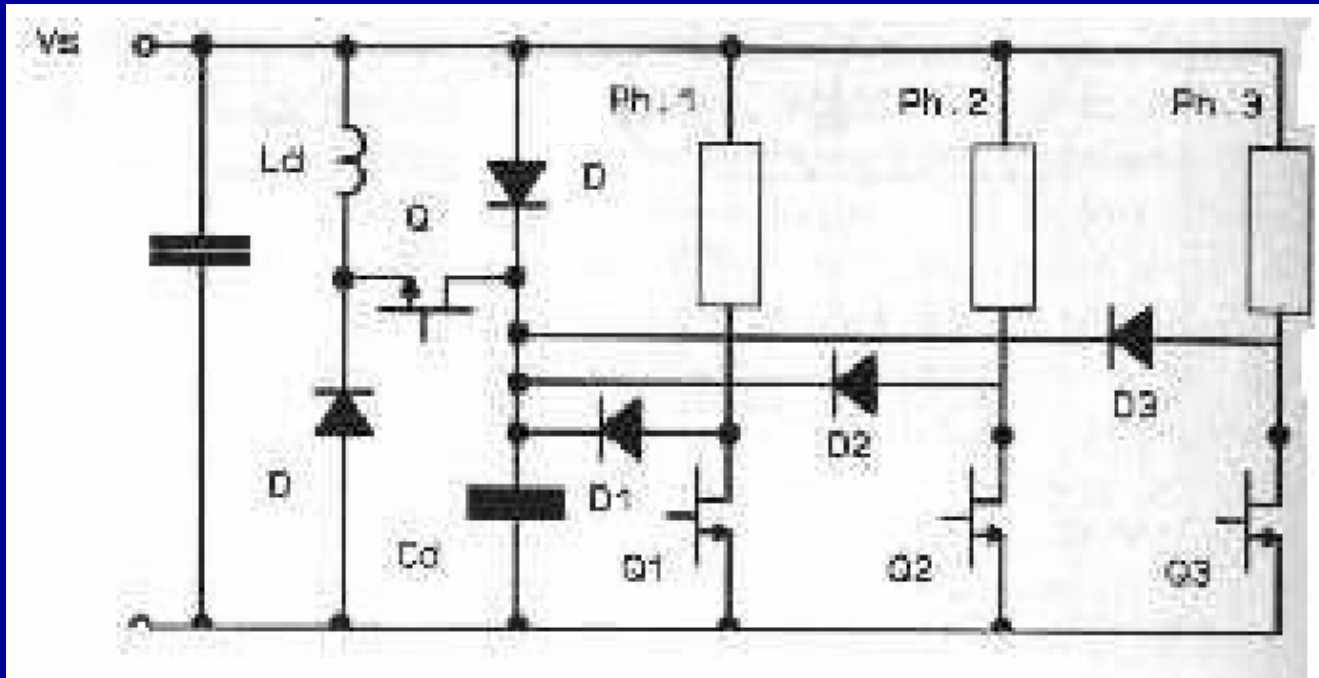
Controller design for SR motors

- what else can be done ???
 - add a series resistor



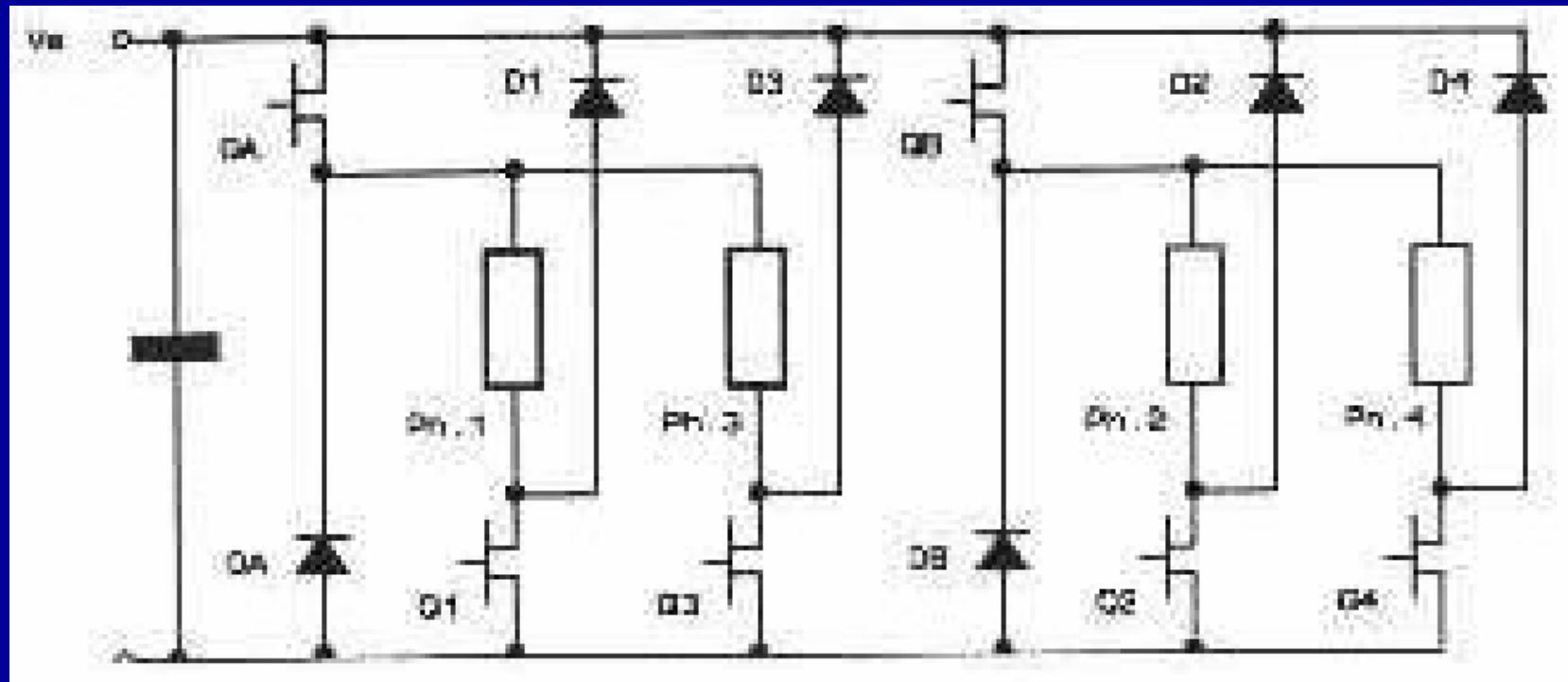
Controller design for SR motors

- what else can be done ???
 - use a C-dump circuit



Controller design for SR motors

- controller for a 4 phase SR motor

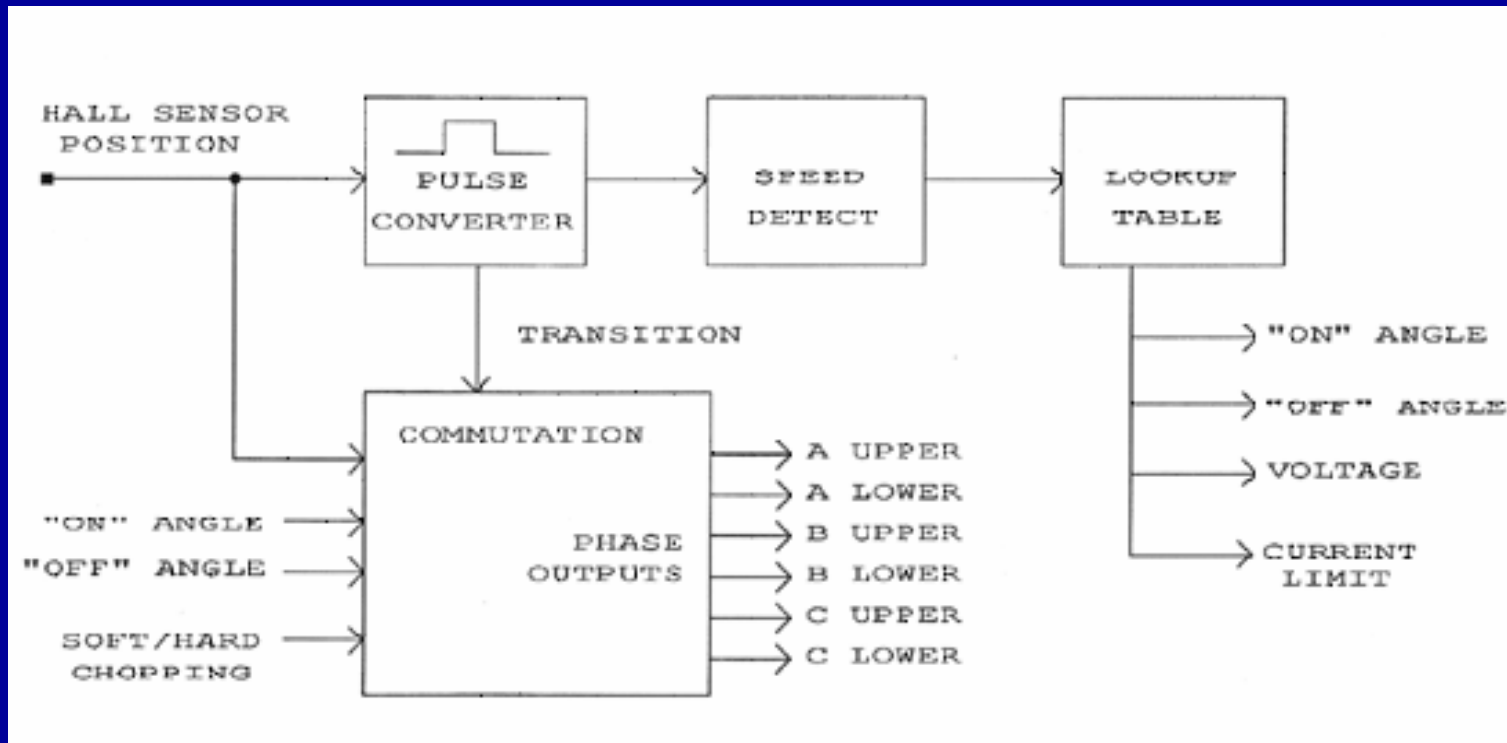


Controller design for SR motors

- drawbacks of the $2^{*(n-1)}$ power topology
 - phases can not be controlled independently
 - upper switches must be sized for a higher load
 - the system loses its fault tolerant characteristics

Controller design for SR motors

- features of the SR control logic



Sensorless control SR motors

Sensorless control SR motors

- sensors are undesirable in any motor but especially in the SR motor
 - added cost
 - contamination
 - temperature limitation
 - interconnects

Sensorless control SR motors

- multiple schemes are available for sensorless control of the SR motor
 - observer models
 - inductance measurement through active probing
 - inherent inductance measurements during normal operation

Sensorless control SR motors

- observer models
 - construct mathematical model of the motor and match the model to the motor
 - difficulties at startup, when no operating history is available
 - have only been demonstrated at low speed, variable speed operation of up to 2000 RPM

Sensorless control SR motors

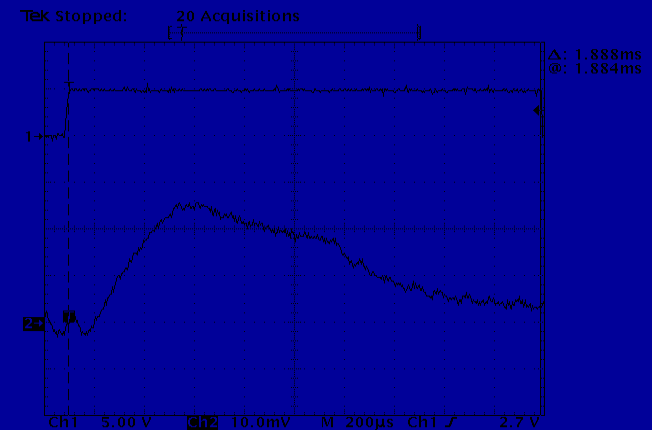
- inductance measurements through active probing
 - injects a signal (i.e. HF) into a phase (active or inactive) and measures the response
 - additional hardware is required, which increases cost
 - may be sensitive to noise pickup from switching

Sensorless control SR motors

- inherent inductance measurements during normal operation
 - comparison of the current waveform
 - measurement of the current level
 - current rise time
 - these methods will be discussed in greater detail

Sensorless control SR motors

- inherent inductance measurements during normal operation
 - comparison of the current waveform
 - typical VSR motor current waveform shows a hump in the motor current
 - determine the slope of the current and detect the peak or the shoulder
 - Problems with this approach:
 - can not be used to start the motor
 - different motors may have different waveforms
 - different loads may have different waveforms



Sensorless control SR motors

- inherent inductance measurements during normal operation
 - measurement of the current level
 - at low speeds compare the motor current to an absolute value
 - commute at a preset level
 - Problems with this approach:
 - may not work for all motors
 - does not work at startup or

Sensorless control SR motors

- inherent inductance measurements during normal operation
 - current rise time
 - measure the time it take the current to rise by a given delta
 - compare the result to a preset level to determine the motor's inductance and thus the position
 - Problems with this approach:
 - requires that a PWM signal is present
 - does not work with firing (phase) angle control

Sensorless control SR motors

- inherent inductance measurements during normal operation
 - differential derivative current measurement (patented)
 - measure the derivative of the motor current
 - compare the result to a preset level to determine the motor's inductance and thus the position

Application considerations

Application considerations

- Advantages of the SR motor
 - VSR motors are of low cost construction
 - VSR motors exhibit very high efficiencies
 - VSR motors are very efficient at very high speeds
 - VSR motor power density is equal or better than high energy product magnets
 - VSR motors are tolerant to single point failure in winding and driver power stage
 - lack of magnets makes it suited for use in hostile (corrosion), extreme (temperature), or sensitive (clean, sealed) environments

Application considerations

- Drawbacks of the SR motor
 - SR motors are often noisy
 - SR motors require more complex control and commutation than BLDC
 - most VSR motors exhibit inherent torque ripple

Application considerations

- other issues with SR motors
 - maximum efficiency is achieved at rated (full) load
 - external excitation must be provided
 - the excitation becomes part of the power equation
 - suitable for efficient very high speed operation
 - waveforms contain high harmonic content
 - requires no special shaping of the current waveform
 - turn on and turn off of the phases
 - does not require sinusoidal waveforms

Application considerations

- the cost of the SR motor
 - studies show that the VSR motor is less costly than BLDC or AC induction motors for a given framesize and power rating
 - the bearing system is more expensive than those of comparable alternatives
 - mechanical tolerances and airgaps have tighter tolerances than those of comparable alternatives

Application considerations

- the cost of the SR controller
 - the commutation for best efficiency is a function of speed, desired torque, and efficiency
 - the commutation will be different for each motor geometry and operating point
 - the discrete implementation of the VSR control section will be complex
 - the cost of the integrated (IC) implementation of the VSR control section will be comparable to that of the BLDC or AC induction motor
 - speed and torque control can often be accomplished by controlling the firing (phase) angles, rather than pulse width modulation (PWM)

Application considerations

- the cost of the SR power driver
 - Unipolar phase currents require fewer power switches
 - Firing (phase) angle control results in reduced switching losses
 - Firing (phase) angle control reduces the cost of the power stages

Application considerations

- the cost of the SR system
 - the motor costs less than BLDC or AC induction
 - the power section costs less than BLDC or AC induction
 - the control section cost equals that of BLDC and AC induction

Application considerations

- typical applications for SR motors
 - pumps (cost, size, weight, fail safe)
 - high speed compressors / fuel cells (high speed, cost)
 - traction drives (cost, fault tolerance)
 - appliances (weight, performance, cost, ruggedness)