



**SMARCA**

Roseville, MN – Wednesday, January 2, 2019

## **NRCA technical issues update**

presented by

**Mark S. Graham**

Vice President, Technical Services  
National Roofing Contractors Association



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### **Topics**

- Moisture in concrete roof decks
- Steel roof deck concerns
- MN building code
- An electrical code (NFPA 70) issue
- ASCE 7-16 (wind design)
- Polyiso. insulation issues
- FM VSH (hail)
- Metal stud-framed parapet walls
- “Fully” adhered
- Questions

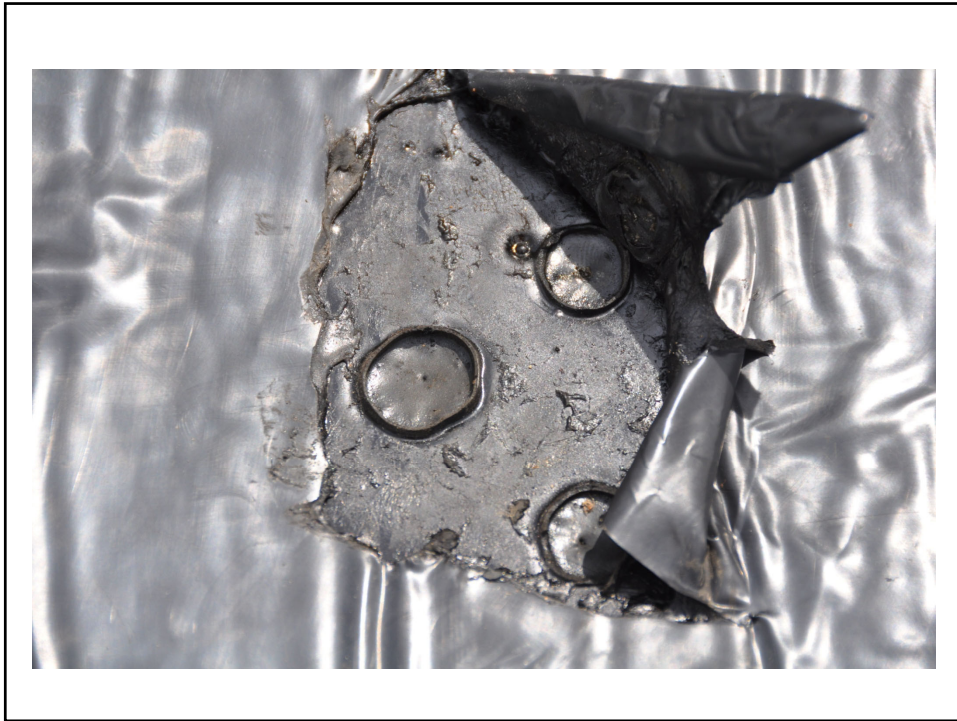
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**Moisture in concrete roof decks**

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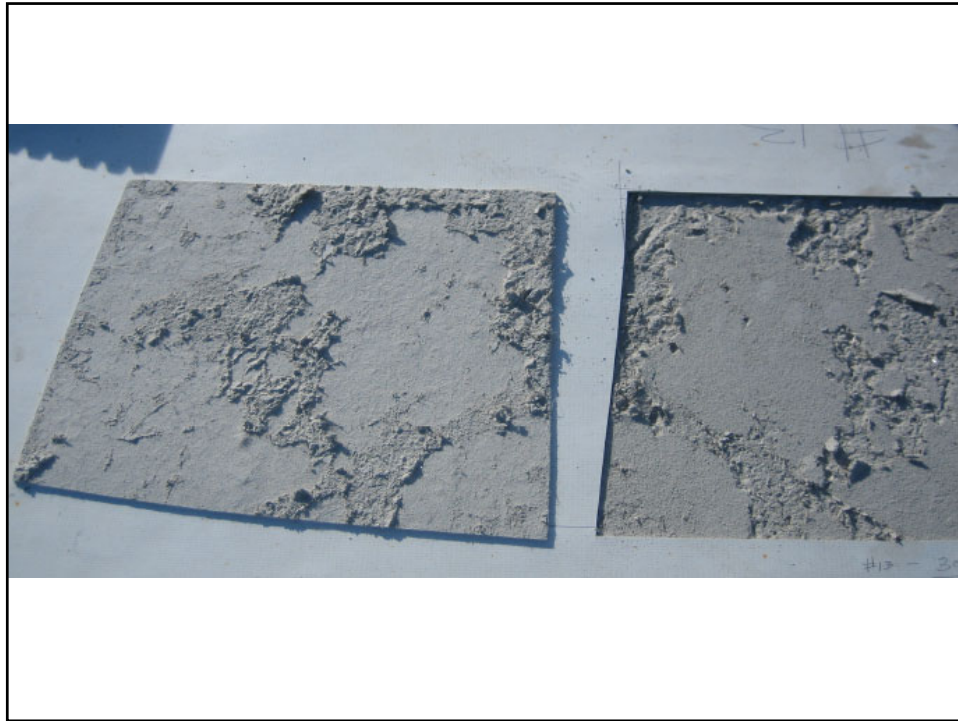
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*All of these are problems related to moisture  
in concrete roof decks...*

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### Some terminology

- **Structural concrete (normal weight)**
  - 150 lbs/ft<sup>3</sup>
- **Lightweight structural concrete**
  - 85–120 lbs/ft<sup>3</sup>
- ~~Lightweight insulating concrete~~
  - 20–40 lbs/ft<sup>3</sup>

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### Concrete mix design

- **Aggregate:**
  - Large aggregate
  - Fine (small) aggregate
- **Portland cement**
- **Water**
- **Admixtures:**
  - Fly ash
  - Air entrainment
  - Curing compounds
  - Etc.

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## **Concrete Aggregates**

60-80% of Concrete Mix Design

- Normal-weight aggregates (stone):
  - Dense
  - Absorb about 2% by weight
- Light-weight aggregates (expanded shale):
  - Porous
  - Absorbs from 5 - 25% by weight

***Lightweight structural concrete  
inherently contains more moisture***

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## **When is it OK to roof?**

Historical guidelines

- After 28 days
- Application of hot bitumen
- Plastic film test
  - ASTM D4263, “Standard Test Method for Indicating Moisture in Concrete by the Plastic Sheet Method”

***These are not appropriate for  
current generations of concrete mixes***

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## Concrete Floors and Moisture, 2<sup>nd</sup> Edition

Howard M. Kanare, CTL Group

75% internal RH can be achieved:

- Normal weight structural concrete
  - Less than 90 days
- Lightweight structural concrete
  - Almost 6 months

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## NRCA Industry Issue Update, August 2013

**INDUSTRY ISSUE UPDATE**

NRCA Member Benefit

**Moisture in Lightweight Structural Concrete Roof Decks**  
Concrete Moisture Presents Challenges for Roofing Contractors

**NRCA** Technical Services Section is receiving an increasing number of inquiries relating to the application of roof systems over concrete roof decks. These inquiries can be separated into two general questions: When is a concrete roof deck dry enough to apply a roof covering? And why is a roof system applied over a concrete roof deck showing signs of moisture infiltration when the roof covering isn't leaking?

**CONCRETE BASICS**  
There are three general types of concrete: normal-weight structural concrete, lightweight structural concrete and lightweight insulating concrete.

Normal-weight structural concrete is what most people think of as concrete. It has a density of about 150 pounds per cubic foot (pcf). Lightweight structural concrete has structural load-carrying capabilities similar to normal-weight structural concrete. It has a density in the range of 85 to 130 pcf. Lightweight insulating concrete, which many roofing professionals are familiar with as an insulating, slope-in-place deck topping, typically has a density in the range from 20 to 40 pcf.

Structural concrete—normal-weight structural concrete and lightweight structural concrete—is produced by mixing large and small aggregates, Portland cement, water and, in some instances, admixtures such as fly ash or various chemical additives. Admixtures can add moisture into the concrete, accelerate concrete's setting, retain concrete's excess moisture and/or lengthen concrete's finishing time. Use of admixtures typically is not visually identifiable in the field; microscopic analysis usually is needed for post-application identification of admixtures.

The primary difference in the composition of normal-weight structural concrete and lightweight structural concrete is the large aggregate type. Normal-weight structural concrete contains normal-weight aggregates such as stone or crushed gravel, which are dense and typically will absorb no more moisture than about 2 percent by weight. Lightweight structural concrete uses lightweight,

porous aggregates such as expanded shale, which will absorb about 5 to 25 percent moisture by weight. Lightweight aggregate needs to be saturated with moisture—its often stored in ponds—before mixing. As a result, lightweight structural concrete inherently contains much more water than normal-weight structural concrete.

Lightweight structural concrete is used in roofing-related applications for cast-in-place concrete roof decks using removable form composite roof decks where a metal form deck remains in place and as a deck topping material, such as a concrete topping surface over precast concrete planks or slabs.

Once poured, lightweight structural concrete typically cures more slowly than normal-weight structural concrete.

Visual identification is possible using magnification, typically a microscope used by a trained technician.

**REPORTED PROBLEMS**  
The problems reported in NRCA associated with lightweight structural concrete roof decks include the following:


- **Moisture accumulation.** Excessive moisture from a concrete deck can be pressure-differential driven into and condensed within a roof system.
- **Adhesive loss.** The presence of moisture can result in deterioration of moisture-sensitive roofing materials and adhesive bond lines between adjacent material layers.
- **Adhesive issues with water-based and non-solvent organic compounds.** Excessive moisture can affect adhesive curing and drying rates. Also, moisture can result in adhesive "bleeding," resulting in bond strength loss.
- **Mold and fungus corrosion.** Excessive moisture can contribute to and accelerate metal component corrosion, including fastener corrosion.
- **Insulation R-value loss.** The accumulation and presence of moisture in most insulation products will result in reduced thermal performance (lower effective R-value).
- **Microbial growth.** The presence of prolonged high-moisture

[Link](#)

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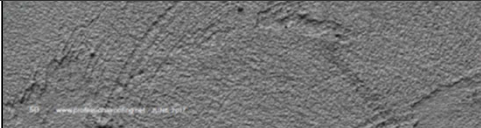
## Professional Roofing

June 2017



ASTM E96 calculated perm				
Lightweight structural concrete			Normal weight concrete	
Age	Wet cup	Dry cup	Wet cup	Dry cup
28 days	1.48	0.78	3.42	1.05
60 days	1.45	0.47	2.03	1.13



The figure shows results of ASTM E96 water vapor transmission testing. Note the lightweight structural concrete has about half of the permeability of regular weight concrete. Considering lightweight structural concrete arrives with more than twice the evaporable water of regular weight concrete, this explains why lightweight structural concrete retains moisture for so long.



[Link](#)

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## Moisture on concrete roof decks

**Moisture in concrete roof decks**  
Normal-weight and lightweight structural concrete cause some concern  
by Mark S. Givens

**N** NRCA continues to receive a significant number of reports of moisture-related problems associated with concrete roof decks. Following years of background information and NRCA-based recommendations for addressing the issue, we've reported:

The issue of moisture in concrete roof decks is not new. Since 2006, NRCA has received numerous reports of moisture-related problems with roof systems installed on concrete roof decks. Such lightweight structural and normal weight structural concrete. Reported problems include roof system moisture accumulation, excessive heat, delamination with water-based and low-volatility organic compound coatings, mold and bacteria growth, moisture to vapor rise and structural damage.

Since the 2005 publication of the NRCA Building Waterproofing Manual, 4th Edition, NRCA no longer considers the plastic sheeting method as a viable assessment to determine a concrete roof deck's dry-moisture and vapor resistance. Also, due to the close correlation between concrete DR (dry-cup) and wet-cup test results:

**Professional Roofing,**  
Sept. 2017

[Link](#)

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## Moisture vapor reduction admixtures (MVRAs)

Some examples:

- Barrier One
- ISE Logik MVRA 9000
- SPG VaporLock

*NRCA still has not seen an MVRA perform successfully in concrete roof deck applications*

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## Moisture vapor reduction admixtures (MVRAs)

RESEARCH+TECH



**Are admixtures the answer?**  
Moisture in concrete roof decks continues to be problematic  
by Mark S. Graham

**NRCA Technical Services Section** has been searching together regarding the use and effectiveness of specific concrete mix additives and special treatments to address moisture related concerns with concrete roof decks. Such admixtures usually are referred to as moisture vapor reduction admixtures (MVRAs) or permeability reducing admixtures. NRCA provides recommendations regarding their use.

**MVRAs**  
Concrete admixtures intended as MVRAs are specific chemicals added during concrete's heating and setting to provide an additional chemical reaction during the concrete's hydration and curing process. MVRAs on the concrete's surface cause water and chloride to create a calcium silicate hydrate gel within the concrete. The gel is said to fill the small pores and capillary openings in curing concrete, assisting the concrete's ability to pass and reduce moisture vapor. The gel is intended to be permeable and integral throughout the concrete's entire thickness.

24 www.professionalroofing.net DECEMBER 2018

**Professional Roofing**  
December 2018

[Link](#)

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*The roofing industry needs to re-think  
the concept of concrete roof deck “acceptance”*

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**Steel roof deck concerns**

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### **Steel roof deck design**

- SDI Design Manual
- AISI S100, “Specifications for the Design of Cold-formed Steel structural Members”
- ANSI/SDI RD1.0-2006, “Standard for Steel Roof Deck”
- ANSI/SDI RD-2010, “Standard for Steel Roof Deck”
- *SDI Roof Deck Design Manual, First Edition* (Nov. 2012)

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### **Steel roof deck design**

Wind uplift resistance

- Minimum 30 psf uplift (uniform loading)
- Minimum 45 psf uplift (uniform loading) at roof overhangs

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## SDI bulletin

2009

STEEL DECK INSTITUTE  
Position Statement

**ATTACHMENT OF ROOFING MEMBRANES TO STEEL DECK**

This document has been published by the Steel Deck Institute (SDI) as a position paper in response to discussions taking place in the roofing community about the screw attachment of roofing membranes to steel deck following line patterns with large spacing. The impetus for this paper is in response to testing carried out by the Special Interest Group for Dynamic Evaluation of Roofing Systems (SDIGERS) at the Institute for Research in Construction, National Research Council of Canada. The mandate of the SDIGERS joint research program is to carry out generic, joint competitive research on the performance of flat roofing systems subjected to dynamic wind loading. The objective is to develop improved roofing systems and design methods.

The SDIGERS research is looking at roofing systems that incorporate wide membranes sheets attached to the steel deck following line patterns spaced at up to 12 ft (3.66 m). While the membrane itself has the performance characteristics to accommodate this size of tributary loading, the existing design methods for steel deck under wind uplift are typically based on the uniform application of the wind suction to the deck. The large majority of the steel roof deck used for commercial buildings in North America is profiled with 1 1/4" (31.8 mm) flutes, with the structural supports usually spaced between 5' 0" (1.52 m) and 6' 0" (1.83 m). Under uplift conditions, the attachment of the roofing membrane along lines with large spacing could produce localized loads that can exceed the capacity of the deck, whereas those same loads applied uniformly on the surface of the deck would be acceptable.

The strength of screwed connection between the membrane and the steel deck, as well as the strength of screwed, nailed, or welded attachment of the steel deck to the structural supports can be computed according to the North American Specification for the Design of Cold-Formed Steel Structural Members. These design values are based on the specified minimum mechanical properties (i.e. base steel thickness and yield strength) specified for the steel sheet roof deck, and should be lower than the strength determined by field testing. The use of field test results for properties such as the pull-out strength of a screw into a steel deck needs to recognize that the properties of the steel deck can be higher than the minimum limits required by the steel specifications. Therefore, field testing results must be adjusted accordingly to account for the difference between the actual properties of the deck and the minimum properties of the steel according to the material specification used in design.

The screw fastening of wide roofing membranes (up to 12 ft) and the corresponding spacing of the lines of screws holding the membrane on the deck, will have a very different effect on the deck and structural supports than a membrane that is adhered over its entire surface. The screws will produce a line load along the deck instead of a uniform load of the entire deck surface. The line loads can be perpendicular or parallel to the deck flutes depending on the orientation of the membrane; each condition can have different implications of the loading that is applied to the deck.

If the roofing membrane seam is perpendicular to the flutes of the deck, as illustrated in Figure 1, there are two special conditions that need to be considered:

1. If the membrane seam occurs at the mid-span of the steel deck; and
2. If the membrane seam occurs at the structural support (joist).

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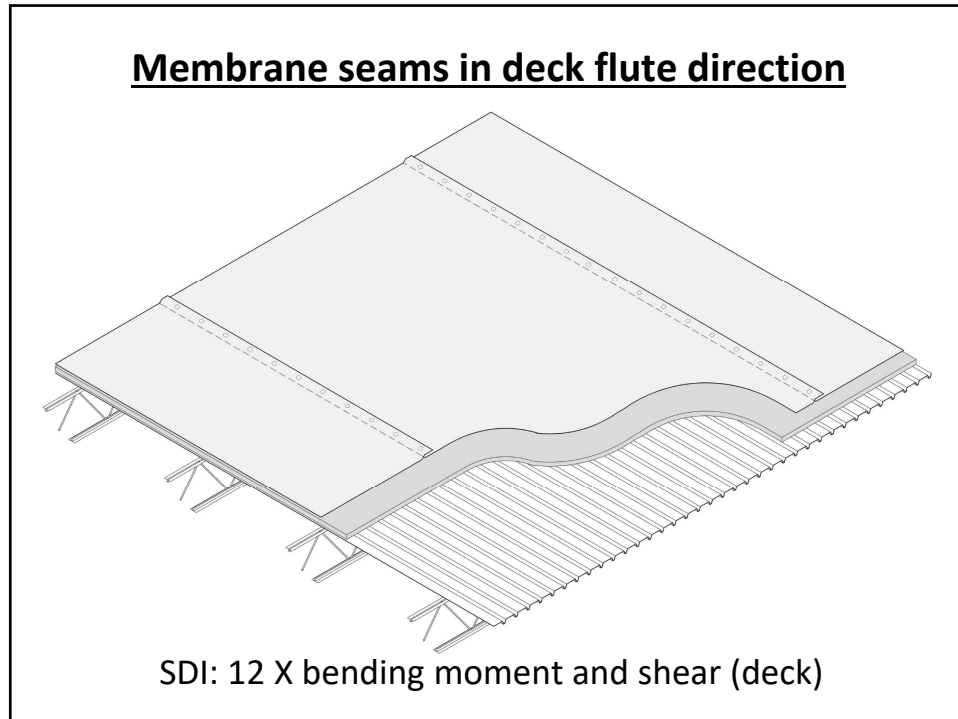
- Decks designed for joist spacing between 5' and 6' 8" o.c.
- Decks designed for uniform loading
- Seam-fastened single-ply membranes are a concern

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## Membrane seams across deck flutes

**SDI: 3.8 X moment (deck); 2 X load (joists)**

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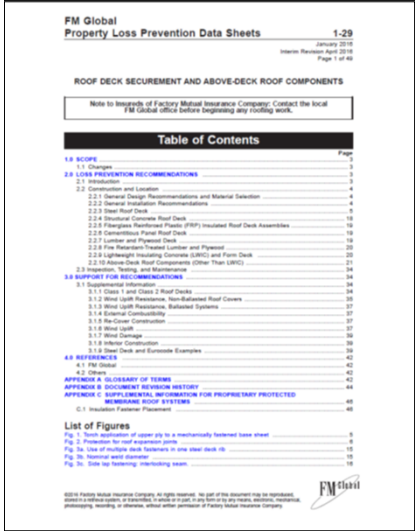
**SDI bulletin -- Conclusion**

“...SDI does not recommend the use of roofing membranes attached to the steel deck using line patterns with large spacing unless a structural engineer has reviewed the adequacy of the steel deck and the structural supports to resist to wind uplift loads transmitted along the lines of attachment. Those lines of attachment shall only be perpendicular to the flutes of the deck.”

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## FM 1-29 updated

www.fmglobaldatasheets.com



The image shows the cover and table of contents of the document 'FM Global Property Loss Prevention Data Sheets 1-29'. The cover includes the title, version number (1-29), date (January 2018), and a note to consult the local FM Global office before engineering any roofing work. The table of contents lists sections such as 'ROOF DECK SECURITY AND ABOVE-DECK ROOF COMPONENTS', '1.0 SCOPE', '2.0 LOSS PREVENTION RECOMMENDATIONS', and '3.0 SUPPORT FOR RECOMMENDATIONS'.

New criteria for steel roof deck uplift:

- Uniformly-distributed loading
- Concentrated loading

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## An example

Hypothetical analysis using FM 1-29

- Adhered (uniform loading) roof system:
  - 6 ft. joist spacing → Class 165
- Seam-fastened (nonuniform, linear load) roof system:
  - 6 ft. seam spacing → Class 90 (33 ksi steel deck)
  - 9.5 ft. seam spacing → Class 90 (80 ksi steel deck)
  - 6 ft. seam spacing → Class 165 (80 ksi steel deck)

***Seam spacing wider than joist spacing is problematic***

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**THE SITUATION WITH STEEL DECKS**

Steel roof deck design can affect roof system selection and design

by Mark S. Graham

**Professional Roofing**  
March 2017  
www.professionalroofing.net

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**CONSTRUCTION ISSUES**

discussion of construction issues and techniques

**Are Your Roof Members Overstressed?**

By James M. Fisher, Ph.D., F.E., D. ASCE and Thomas Spun, Ph.D., F.E., S.E., F.AISC

**Structure magazine**  
March 2017  
www.structuremag.org

Membrane roof systems installed on steel roof decks traditionally result in a uniform transfer of wind uplift loads from the roof membrane to the steel roof deck and underlying supporting structure (e.g., steel joists). For example, in a built-up membrane roof system... which has been used commonly in the U.S. roofing industry for more than 125 years... the built-up membrane is continuously adhered to rigid board insulation. The rigid board insulation, which is used to span the steel deck's Bata, is mechanically attached to the steel roof deck in a closely-spaced pattern (e.g., 1 fastener per every 2 square feet, resulting in a near uniform uplift load path. Polymer-modified bitumen roof systems and adhered single-ply membrane roof systems are installed in similar configurations and result in a similar uniform uplift load path.

In the 1960s, single-ply membrane roof systems were first introduced into the U.S. roofing market. By the late 1970s, the seam-fused, mechanically attached method of installation was first introduced. With this installation method, the single-ply membrane sheet is mechanically attached along its raised edges into the roof deck, which results in a larger tributary uplift load per fastener and placement of fasteners in lines, non-uniform loading configurations of the roof deck and underlying supporting structure. When first introduced, membrane sheet widths in seam-fused single-ply membrane roof systems typically were five feet wide, resulting in rows of mechanical fasteners spaced at feet on-center. Since the early 2000s, single-ply membrane sheet widths have become wider, with 16-foot-wide sheets now commonplace - resulting in rows of mechanical fasteners spaced at 10-foot on-center.

Currently, single-ply membrane roof systems have clearly evolved as conventional built-up and polymer-modified bitumen membrane systems in market share. The seam-fused, mechanically attached method of installation also has overtaken traditionally adhered methods of application. The National Roofing Contractors Association (NRCA) annual market survey shows seam-fused, mechanically attached single-ply membrane roof systems make up the majority of all membrane roof systems currently installed.

With the present emphasis on wind resistance in design, a closer look at how seam-fused, mechanically attached single-ply membrane roof systems interact with steel roof deck and joint construction is in order.

A common method of single-ply membrane sheet layout is shown in Figure 1. A common placement of mechanical fasteners is shown in Figure 2. These concentrated line loads can severely overstress the steel deck and may also cause the steel joint before the deck to be overstressed under uplift loading. The behavior of such fastening systems, when the roof system is subjected to uplift loadings, is shown in Figure 3. The current trend in construction is for the membrane installer to mechanically fasten the membrane to the deck only along the edge of the sheet with its spread by the roof installation, thereby lowering installation costs. Unfortunately, the Structural Engineer of Record, and the steel deck and joint supplier, are usually unaware of the concentrated load pattern of the roof membrane attachment. In fact, the architect of record may not be aware of the modifications of such attachments. The Architectural roofing specifications may simply state that the roof membrane shall be installed per manufacturer's recommendations. The roofing installers themselves are the one who generally decides on the exact layout of the membrane sheets on the roof. This decision is made based on what layout can be installed in the fastest and least expensive

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### **Fastener pull-out tests...**

*There is little correlation between fastener pull-out resistance and a steel roof deck's yield strength and uplift (bending) strength*

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*Although roofing contractors sometimes are given the responsibility of inspecting and accepting steel roof decks to receive a new roof system, determining a roof deck's design adequacy is beyond the expertise of most roofing contractors.*

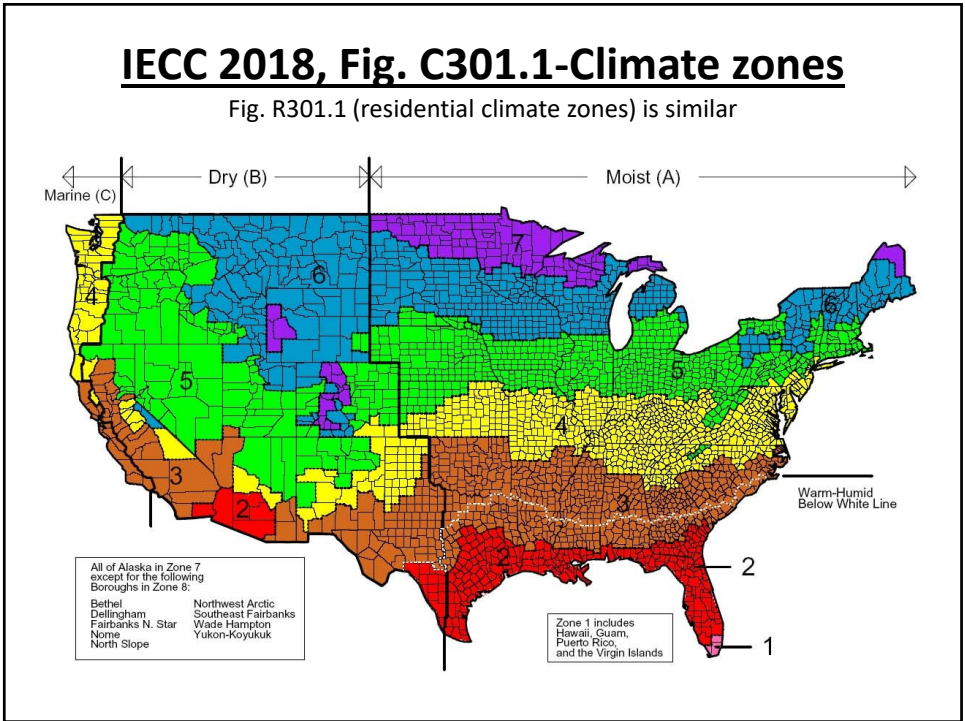
*This determination is best made during a project's design phase.*

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**Minnesota state building code**  
Based on 2012 I-codes

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### Comparison of IECC's various editions

Commercial Buildings (Insulation component R-value-based method)

Climate Zone	IECC 2003	IECC 2006	IECC 2009	IECC 2012*	IECC 2015*	IECC 2018*
1	R-12 ci	R-15 ci	R-15 ci	R-20 ci	R-20 ci	R-20 ci
2	R-14 ci		R-20ci		R-25 ci	R-25 ci
3	R-10 ci				R-30 ci	R-30 ci
4	R-12 ci	R-20 ci	R-25 ci	R-25 ci	R-30 ci	R-30 ci
5	R-15 ci					
6	R-11 ci	R-25 ci	R-25 ci	R-30 ci	R-35 ci	R-35 ci
7	R-15 ci					
8	R-15 ci	R-25 ci	R-25 ci	R-30 ci	R-35 ci	R-35 ci

\* Applies to roof replacement projects  
ci = continuous insulation

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Keeping an eye on  
**I-CODES:**  
Part one

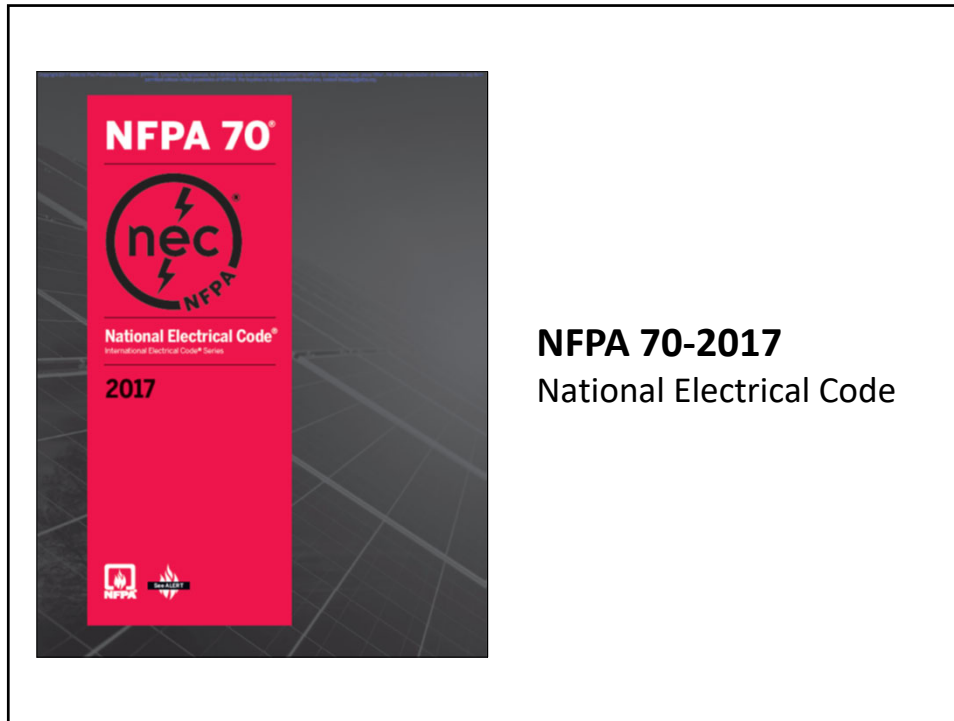
Professional Roofing, December 2017  
[Link to access this article](#)

Keeping an eye on  
**I-CODES:**  
Part two

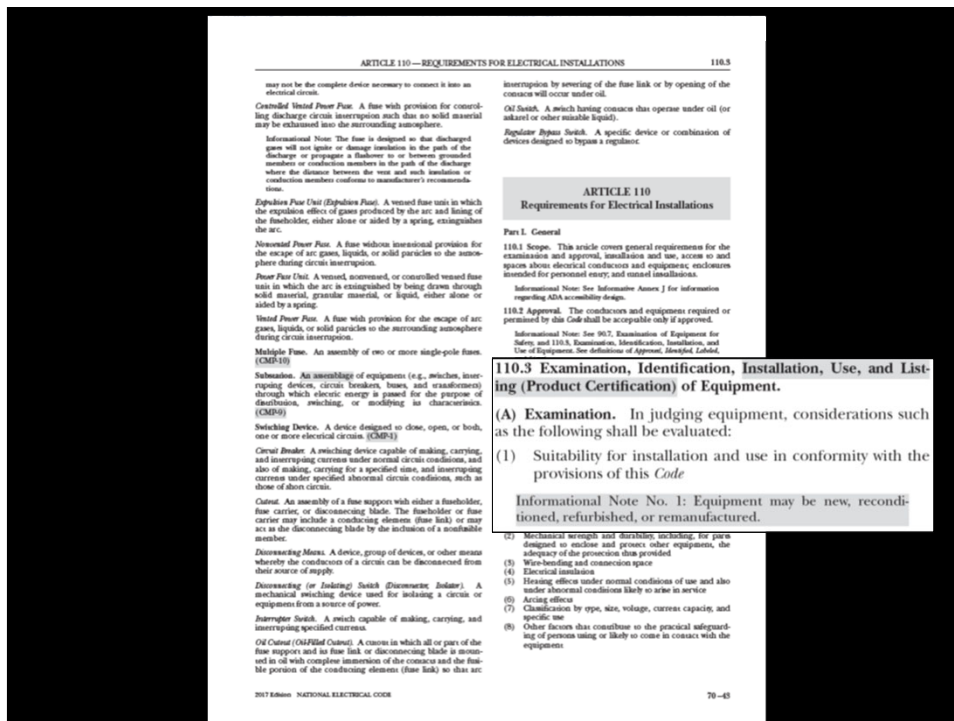
**Changes to the 2018 codes affect roof assemblies**

Professional Roofing, January 2018  
[Link to access this article](#)

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**NRLRC News**  
OSHA issues memorandum outlining enforcement of silica standard  
Contract provision to provide roofing contractor with opportunity to appeal dispute resolution decision issued by "decision maker" designated by contract  
[ More news ]

**Contract provision obligating manufacturer and seller of equipment to roofing contractor to furnish equipment that is code-compliant**

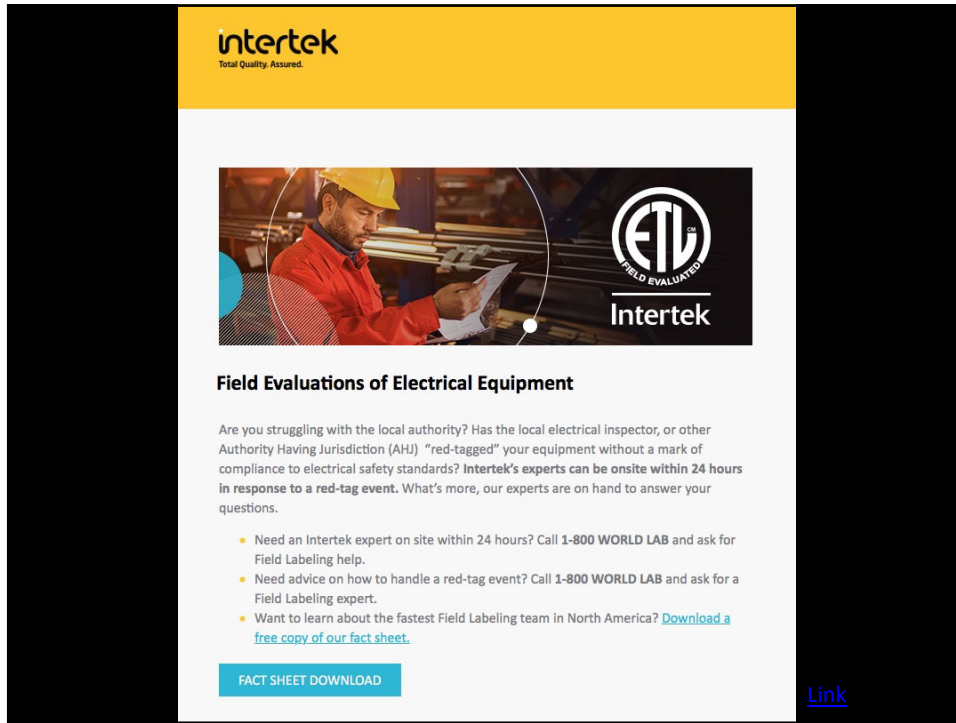
When purchasing a new piece of equipment, roofing contractors should beware of signing a seller's or manufacturer's standard purchase order agreement or agreeing to a seller's or manufacturer's standard terms and conditions. This agreement could include an express disclaimer of Uniform Commercial Code warranties of merchantability and fitness and will seek to limit the liability of the seller and the remedies available to the buyer in the event of a defect or problem with the product. Prior to making a purchase, the roofing contractor should obtain written assurance the equipment or product the contractor is purchasing complies with all codes, standards and regulations applicable to that equipment or product and its installation. Roofing contractors should be certain to include a provision to that effect in the purchase agreement.

For example, if your roofing company is in the market to purchase a sheet metal folding machine, it's important the sales agreement contain a provision such as the one above that obligates the seller to furnish a machine that will comply with all applicable codes and standards pertaining to the machine in the locality where you intend to install the machine. Such a provision is especially critical considering the 2017 edition of the NFA 70, National Electrical Code (NEC), which jurisdictions could adopt as of Jan. 1. Article 110 of the 2017 NEC contains a new provision that has been interpreted as requiring all electrical equipment installed or used in a building undergo product testing, evaluation and listing (product certification) by a recognized qualified electrical testing laboratory in accordance with applicable product safety standards recognized by the NEC. If your business is in one of the states, cities, counties or towns throughout the U.S. that has adopted the 2017 edition of the NEC, in the absence of proof your new sheet metal folding machine complies with the NEC, code officials may not permit the newly purchased machine to be used. To

**Equipment and product purchase agreement: The Seller and Manufacturer warrant to the Roofing Contractor that the equipment and product manufactured by Manufacturer and sold by Seller to Roofing Contractor will comply with all codes, standards and regulations applicable to the equipment and product in the jurisdiction where the equipment and product are delivered and intended for use, including the applicable electrical code and OSHA standards. No disclaimer or limitation of warranties of merchantability or fitness or other warranties by Seller or Manufacturer and no term or condition in the sales agreement shall cause or be interpreted to void, disclaim or reduce the obligation of the Seller and Manufacturer to furnish equipment and products that are in compliance with applicable codes, standards and regulations.**


7/31/2018 [Link](#)

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The advertisement features the Intertek logo at the top left with the tagline "Total Quality Assured." Below the logo is a photograph of a worker in a red jacket and yellow hard hat reviewing documents on a construction site. To the right of the photo is the ETL logo, which stands for "FIELD EVALUATED," and the Intertek name. The main heading is "Field Evaluations of Electrical Equipment." The text explains that Intertek experts can provide onsite assistance within 24 hours for red-tagged equipment. A list of three bullet points provides contact information and a link to a fact sheet. At the bottom left is a "FACT SHEET DOWNLOAD" button, and at the bottom right is a "Link" text.

**intertek**  
Total Quality Assured.



**Intertek**

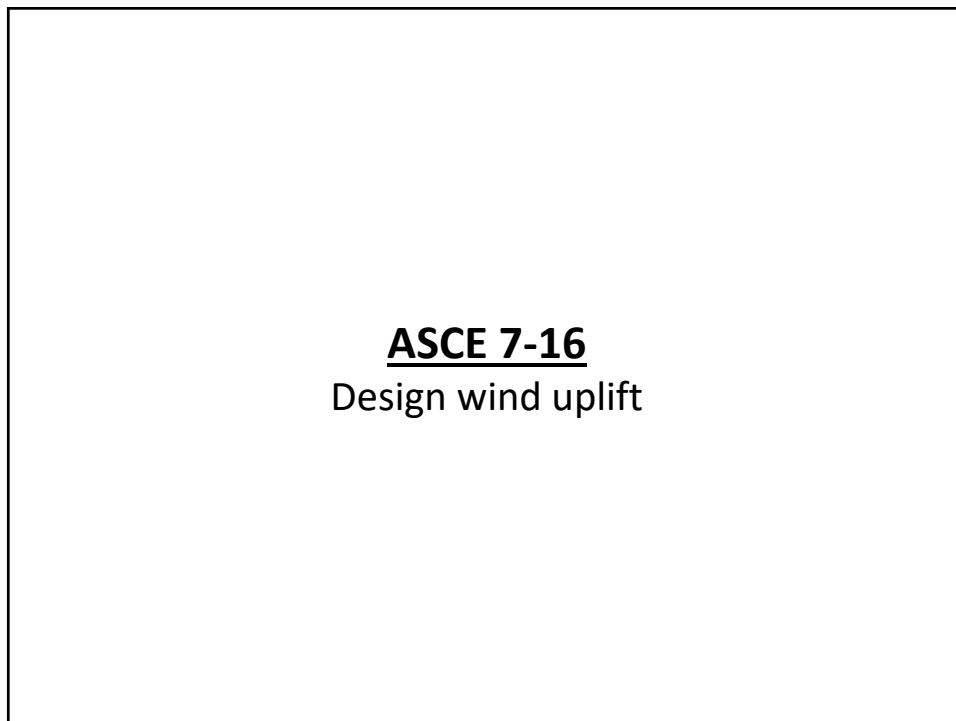
### Field Evaluations of Electrical Equipment

Are you struggling with the local authority? Has the local electrical inspector, or other Authority Having Jurisdiction (AHJ) "red-tagged" your equipment without a mark of compliance to electrical safety standards? Intertek's experts can be onsite within 24 hours in response to a red-tag event. What's more, our experts are on hand to answer your questions.

- Need an Intertek expert on site within 24 hours? Call 1-800 WORLD LAB and ask for Field Labeling help.
- Need advice on how to handle a red-tag event? Call 1-800 WORLD LAB and ask for a Field Labeling expert.
- Want to learn about the fastest Field Labeling team in North America? [Download a free copy of our fact sheet.](#)

[FACT SHEET DOWNLOAD](#) [Link](#)

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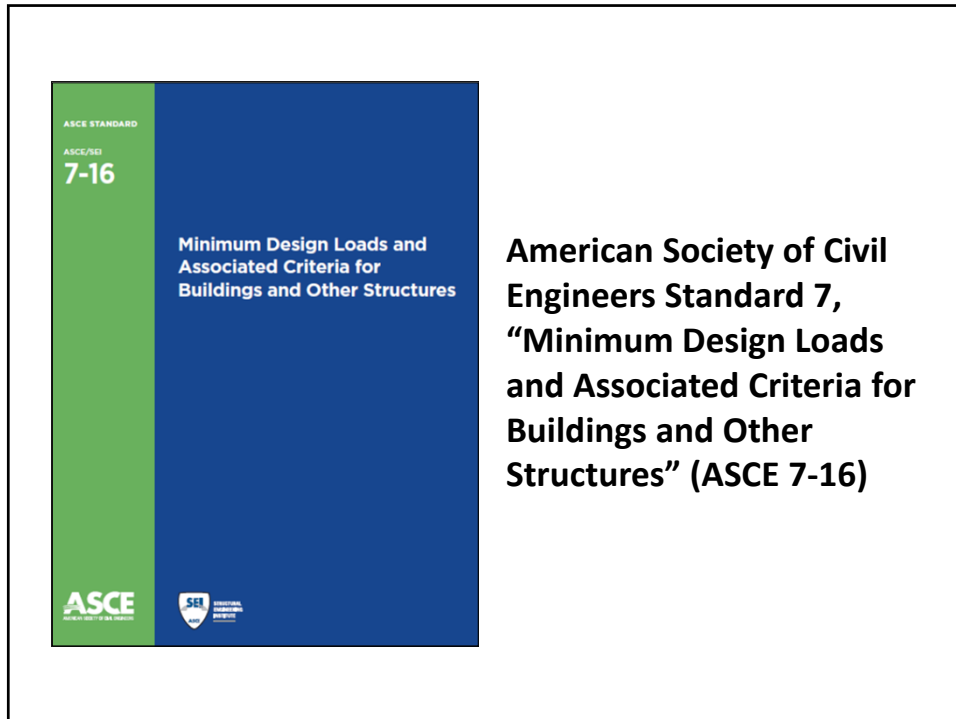


The slide contains the text "ASCE 7-16" in a large, bold, underlined font, with "Design wind uplift" centered below it in a smaller font.

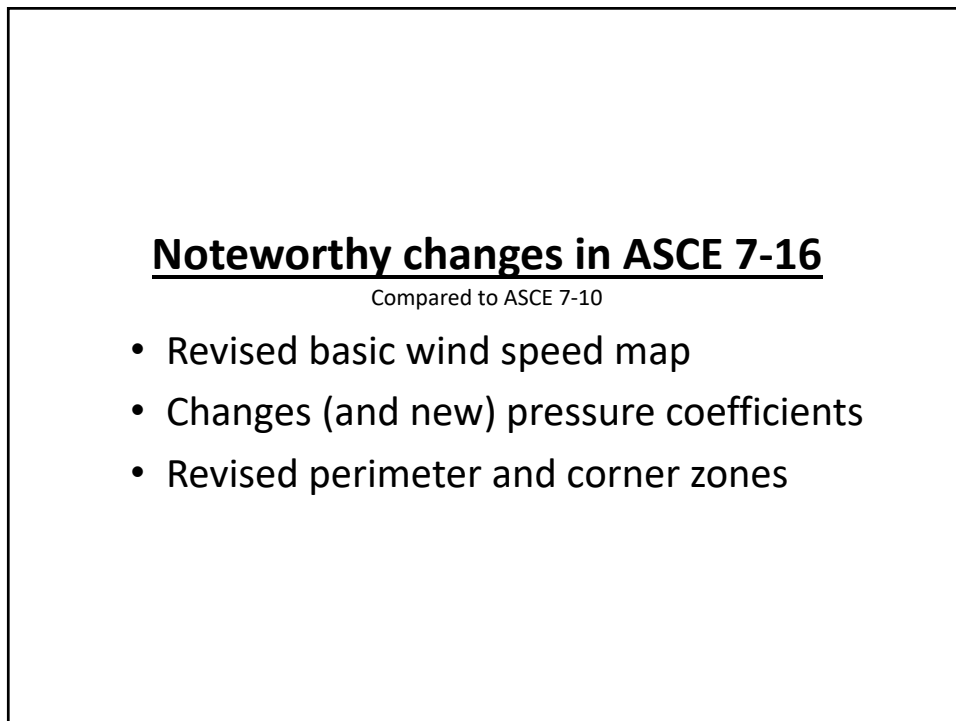
## ASCE 7-16

### Design wind uplift

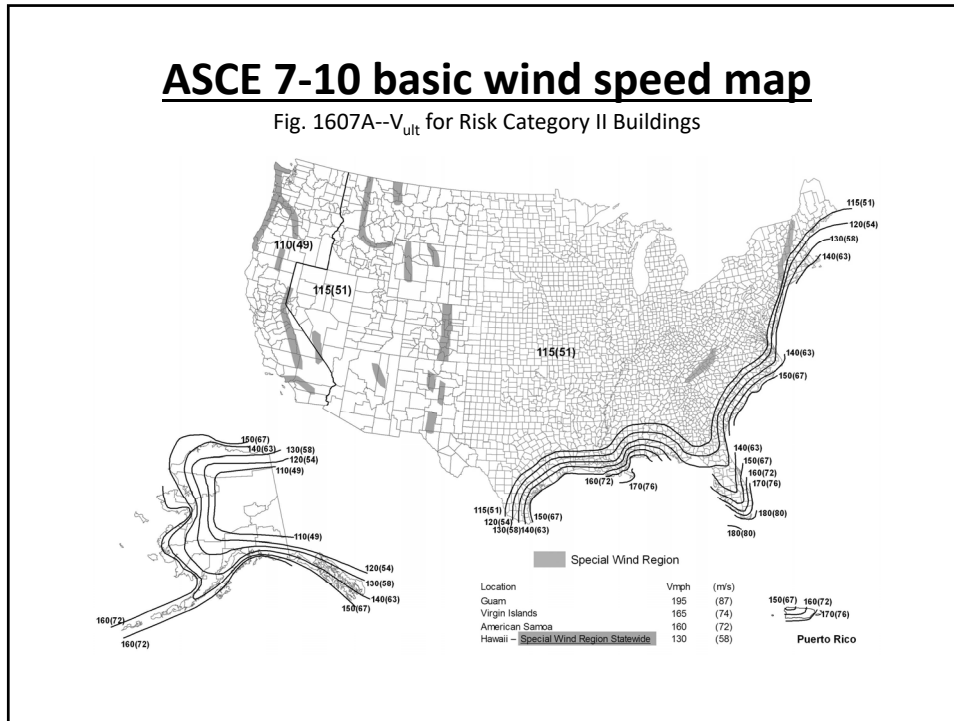
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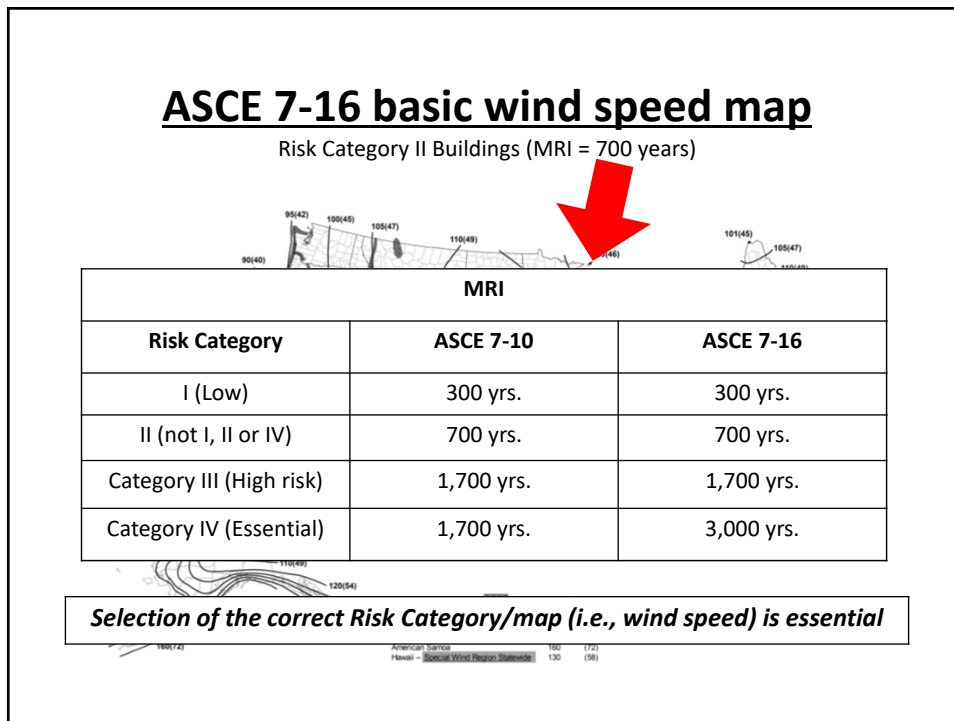
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### Comparing $GC_p$ pressure coefficients

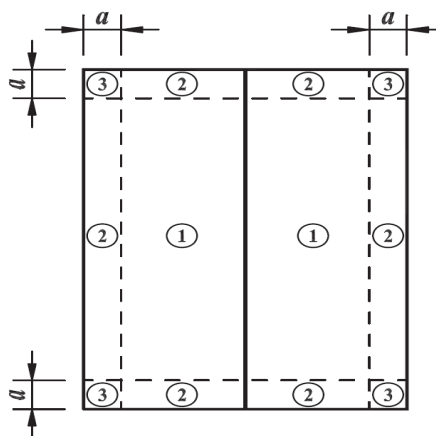
$h \leq 60$  ft., gable roofs  $\leq 7$  degrees

Zone	ASCE 7-10	ASCE 7-16	Change
1'	n/a	0.9	-10%
1 (field)	-1.0	-1.7	+70%
2 (perimeter)	-1.8	-2.3	+28%
3 (corners)	-2.8	-3.2	+14%

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### Zones

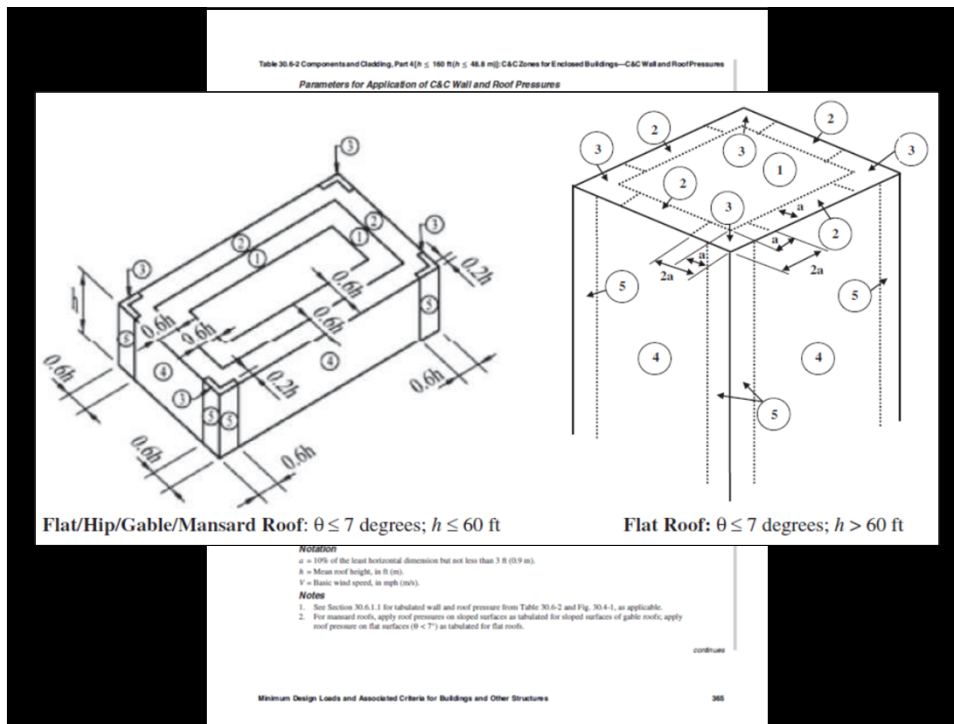
$h \leq 60$  ft., gable roofs  $\leq 7$  degrees



**ASCE 7-10**

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## Noteworthy changes in ASCE 7-16

Compared to ASCE 7-10

- Revised basic wind speed map
- Changes (and new) pressure coefficients
- Revised perimeter and corner zones

*While center field pressures may be slightly lower, field, perimeter and corner uplift pressures will generally be greater*

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*How the roofing industry will adapt to ASCE 7-16 remains to be seen....*

*FM Global has indicated they will update their FM 1-28 to be based on ASCE 7-16 (with modifications) in mid-2019.*

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**Comparing ASCE 7-05, ASCE 7-10 and ASCE 7-16**

**Example:** A office building (Risk Category II) is located in St. Paul, MN. The building is an enclosed structure with a mean roof height of 40 ft. The building is located in an open terrain area that can be categorized as Exposure Category C. An adhered, membrane roof systems is to be installed.

Document	Basic wind speed (mph)	Design wind pressure (psf)			
		Zone 1' (Center)	Zone 1 (Field)	Zone 2 (Perimeter)	Zone 3 (Corners)
ASCE 7-05	90	FM 1-60			
ASCE 7-10 Ult.	115	FM 1-75			
ASCE 7-10 ASD	89	FM 1-60			
ASCE 7-16 Ult.	110	FM 1-105			
ASCE 7-16 ASD	85	FM 1-75			

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*This comparison illustrates why it is important for Designers to include wind design loads in their Construction Documents (per IBC Sec. 1603.1)...*

*...It also illustrates why specifying a wind warrantee can create an uneven playing field. Unless the Designer indicates the wind design loads, which design method will the manufacturer use (e.g., in a competitive environment)?*

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TECH TODAY

Specifying wind design

Many roof system designers inadequately address wind loads in contract documents

by Mark S. Graham

NRCA is receiving an increasing number of reports indicating project drawings and specifications incompletely, inadequately or inaccurately address proper wind design for low-slope membrane roof systems. Some designers, according to reports, only include a specification requirement for the roof system manufacturer to provide a wind warranty. But there are minimum requirements for proper wind design of low-slope membrane roof systems.

**Code requirements**

Building codes typically provide specific requirements for specifying design loads, including wind loads, in contract documents.

**Specifying wind speed warranties is not a substitute for code-required wind design data**

The International Building Code, 2012 Edition (IBC, 2012), Chapter 16-Structural Design, Section 1603-Contract Documents, indicates contract documents need to include a roof system's low wind snow load data, wind design data and any special loads.

Required wind design data includes identifying the ultimate design wind speed, nominal design wind speed, risk category wind exposure and applicable internal pressure coefficient. For component and cladding systems that are not specifically designed by a registered design professional, design wind pressures in terms of psf (pounds per square foot) also are required. Roof systems typically are considered component and cladding systems. Design wind pressures in the field, perimeter and corner regions

of roof areas should be noted in contract documents.

IBC's previous editions include similar contract document requirements.

For new construction projects, design loads most commonly will be identified on structural drawings to the project drawing set. For projects without specific structural drawings, design loads may be provided on architectural drawings or drawing sets or in project specifications.

**ANSI/SPRI ES-1**

ANSI/SPRI ES-1, "Wind Design Standard for Edge Systems Used with Low-Slope Roofing Systems," which is referenced in IBC 2012, includes two primary alternate determination of design wind loads at roof edges (flats, copings) and eaves for resistance loads of copings and flats.

Designers should not simply specify compliance with ANSI/SPRI ES-1 in project specifications; they should determine and clearly indicate design wind loads at roof edges in contract documents.

IBC 2012 includes in Section 1505.5-Edge Structures for Low-Slope Roof-Design wind loads should be determined using the ultimate design wind speed and IBC 2012's Chapter 16, which is based on ASCE 7-10, "Minimum Design Loads for Buildings and Other Structures."

IBC 2012 references ANSI/SPRI ES-1-03, ANSI/SPRI ES-1-03 is based upon ASCE 7-02, which is not an ultimate design wind speed based method. Therefore, the design wind load determination method contained in ANSI/SPRI ES-1 does not satisfy IBC 2012's requirements for design wind loads at roof edges.

Design wind loads at roof edges should be determined using IBC 2012's Chapter 16 and be clearly noted in contract documents.

**Responsibilities**

Designers should not place the responsibility for determining roof system or individual component design wind loads on manufacturers, component suppliers or installers, or roofing contractors.

Also, designers' sole reliance on specifying wind speed warranties is not a substitute for well-considered wind design data. Such warranties typically do not address consideration of ultimate and eventual design wind speeds, building height, risk category, wind exposure and internal pressure coefficients applicable to the specific building necessary for properly determining roof system design wind loads.

Responsibility for properly determining and clearly identifying wind design data, including design wind loads for roof systems, is required by the building code and is clearly that of roof system designers. Designers may retain a structural engineer or qualified consultant to help them fulfill their design responsibilities.

To help designers determine wind loads for commonly encountered low-slope roof systems, NRCA, the Metal Roofing Construction Association and NorthStar Roofing Contractors Association have developed and offer a free online application, Roof Wind Designer. Roof Wind Designer is a web application that allows users to determine design wind loads using ASCE 7's, "Minimum Design Loads for Buildings and Other Structures," 2005 or 2010 edition.

Roof Wind Designer is accessible at [www.nrcawinddesign.com](http://www.nrcawinddesign.com).

**MARK S. GRAHAM** is NRCA's executive vice president of technical services.

Professional Roofing

March 2014

[Link](#)

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Sheet Metal, Air Conditioning and Roofing Contractors Association

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The screenshot shows the website **roofwinddesigner.com** with the subtitle "ASCE 7-05, ASCE 7-10 and ASCE 7-16". A red-bordered box contains the following text:

**Roof Wind Designer has been updated based upon ASCE 7-16:**

- **Part 2: Low-rise Buildings (Simplified) [h ≤ 60 ft.]**
- **Part 4: Buildings with 60 ft. < h ≤ 160 ft. (Simplified)\***

\* Does not include hip and gable roofs h > 60 ft. and all roof slopes over 7 degrees (about 1.5:12)

Below the box, it says: "To register for a new account [click here](#). If you already have an account, [click here](#) to login."

At the bottom of the screenshot is the NRCA logo (National Roofing Contractors Association).

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**Polyisocyanurate insulation**  
 Knit line, thickness and dimensional stability concerns

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**Knit line depressions -- continued**



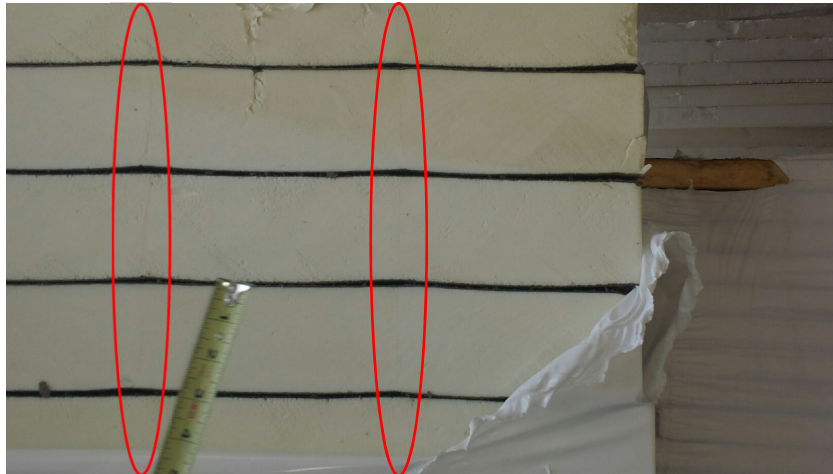
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Photo from manufacturer's product literature

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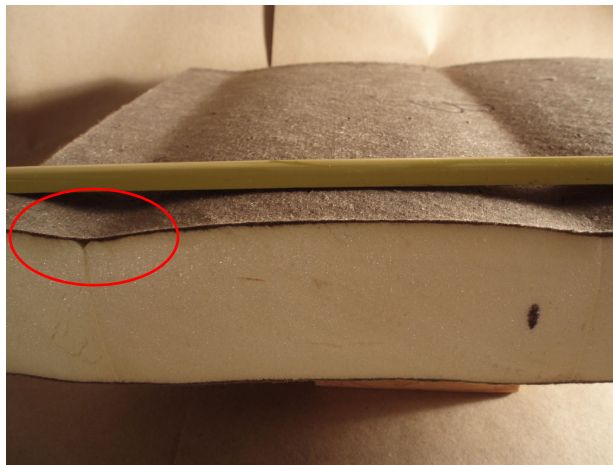
### Thickness and knit lines



As delivered by manufacturer.

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### Knit lines -- continued



After conditioning: 158 ± 4 F and 97 ± 3% RH for 7 days

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**Knit lines -- continued**



Knit line and V-groove close-up (after conditioning)

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“NRCA recommends the use of a suitable cover board layer over polyisocyanurate insulation before the installation of roof membrane.”

*-The NRCA Roofing Manual: Membrane Roof Systems-2019*

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## Additional interim recommendations

Polyiso. knit line, thickness and dimensional stability concerns

- Measure polyiso. thickness upon delivery
- Look for knit lines and board unevenness
- Contact manufacturer and NRCA if you see any issues

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## Thickness variations in polyiso. insulation

RESEARCH+TECH



**Not quite measuring up**  
Polyisocyanurate insulation thicknesses seem to vary

by Mark S. Graham

NRCA has received a handful of reports of hard, rigid board polyisocyanurate insulation with thicknesses less than what was specified and indicated on the manufacturer's package labeling being delivered from manufacturers to distributors and job sites. Following up information about these reports, as well as information about recognized allowable thickness tolerances and NRCA recommendations to roofing contractors for resolving this situation.

NRCA has received reports of some installed polyisocyanurate insulation showing uneven density from polyisocyanurate insulation manufacturer with thicknesses notably less than nominal dimensions. Reports have been received from the Gulf Coast to the Rocky Mountains and as far north as Wisconsin and south to Texas.

Reports have been received about various specified nominal thicknesses of polyisocyanurate insulation, however, the problems appear to be more common with thicker polyisocyanurate insulation products than thinner ones. For example, NRCA has received multiple reports of 30 1/2 inch nominal thickness polyisocyanurate insulation measuring

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July 2017

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## Thickness variations

Polyisocyanurate insulation

- Measured thicknesses notably less than nominal
- Reports from throughout the U.S.
- More common with thicker product
  - For example, 3.5 inch (nominal) measures less than 3¼-inch thick
- Most reports specific to one manufacturer
  - Multiple plants from the one manufacturer
  - Limited reports from other manufacturers

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3.5 inch (nominal)



2.0 inch (nominal)

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## Allowable tolerances

ASTM C1289 (Polyisocyanurate insulation)

**8. Dimensions**

**8.1 Dimensional Tolerances**—The length and width tolerances shall not exceed  $\pm 1/4$  in. (6.4 mm), the thickness tolerance shall not exceed  $1/8$  in. (3.2 mm), and the thickness of any two boards shall not differ more than  $1/8$  in. (3.2 mm) when measured in accordance with Test Method C303.

<p><b>1. Scope</b></p> <p>1.1 This specification covers thermal insulation boards of polyisocyanurate, polyurethane, and organic applications.</p> <p>1.2 This specification covers structural panels of polyisocyanurate.</p>	<p><b>8.3 Edge Trueness in the <i>xy</i> Direction</b>—Unless otherwise specified, the thermal insulation board shall be furnished with straight edges and edges shall not deviate more than <math>1/2</math> in./ft (2.6 mm/m) when examined in accordance with Practice C550.</p> <p><b>8.4 Shiplap Edges</b>—When specified, the insulation board shall be fabricated with shiplap edges along its longest dimensions.</p> <p>8.4.1 The nominal depth of each shiplap shall be the sum of its thickest facer dimension plus one half the thickness of its core foam dimension.</p> <p>8.4.2 For boards 2 in. (50.8 mm) or greater in nominal thickness, the width of the shiplap shall be 1 in. (25.4 mm). For boards less than 2 in. (50.8 mm) in thickness, the nominal width of the shiplap shall be one half the thickness of the faced board product.</p>	<p>Notes: 1. The values in this table are in inches unless otherwise indicated. 2. The values in this table are in millimeters unless otherwise indicated.</p>
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**8.5 Face Trueness**—The thermal insulation boards shall not depart from absolute flatness more than  $1/8$  in./ft (10 mm/m) of length or width when examined in accordance with Practice C550.

<p>1.4 The values in this table are in inches unless otherwise indicated. The values in millimeters are for information only and are not controlling.</p>	<p><b>8.6 Available Sizes</b>—The thermal insulation boards are normally supplied in sizes of 4 by 4 ft (1.22 by 1.22 m), and 4 by 8 ft (1.22 by 2.44 m) for use in roofing applications. For sheathing applications the thermal insulation boards are normally supplied in sizes of 4 by 8 ft (1.22 by 2.44 m), 4 by 9 ft</p>	<p>Notes: 1. The values in this table are in inches unless otherwise indicated. 2. The values in this table are in millimeters unless otherwise indicated.</p>
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**8.7 Crushings and Depressions**—The thermal insulation boards shall have no crushed or depressed areas on any surface exceeding  $1/8$  in. (3.2 mm) in depth on more than 10 % of the total surface area.

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### **The issues...**

Thickness variations in polyiso. insulation

- Most physical properties are thickness related
- R-value loss:
  - R-value decreases about 0.7 per 1/8-inch thickness loss (assuming an LTTR of 5.6 per inch)
- Insulation thickness does not match established wood blocking heights

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### **NRCA's recommendations**

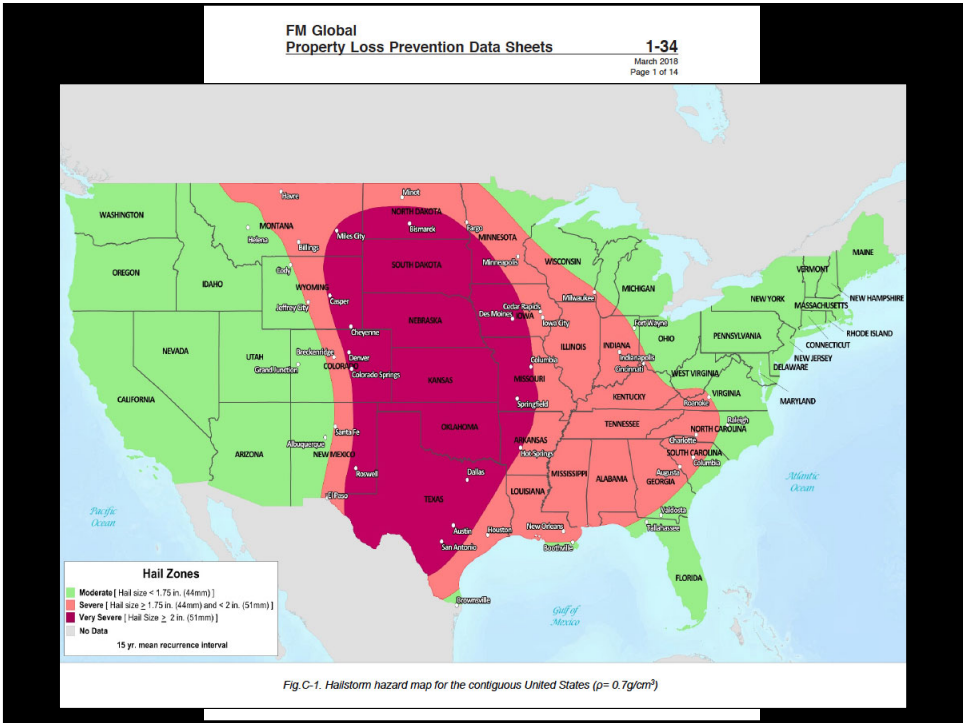
Thickness variations in polyiso. insulation

- Distributors and contractors should measure board edge thicknesses upon delivery, preferably while the insulation still is on the truck
- Contact the manufacturer or distributor if thicknesses are less (or more) than specified
- Also contact NRCA Technical Services

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## FM's very severe hail (VSH) classifications

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**Of the 915,537 roof assemblies in FM’s RoofNav,  
only 316 have a VSH classification**

As of January 1, 2019

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**RESEARCH+TECH**



**Understanding FM VSH**  
FM has implemented a new impact-resistance classification  
by Mark S. Graham

**Commercial and industrial leaders** FM Global and its code-approved testing agency subsidiaries, FM Approvals, have implemented a Very Severe Hail (VSH) impact-resistance classification that could affect some of the work you do.

**FM Global guidelines**  
FM Global traditionally has recommended its insured building owners use non-ferrous hail (NH) and severe hail (SH) classified roof systems for buildings located in areas FM Global considers to be susceptible to moderate or severe hail impacts. FM Loss Prevention Data Sheet 1-24 (FM 1-24), "Hail Damage," provides a map identifying these regions.

In recent years, the U.S. insurance industry has experienced increases in losses from hail in terms of the number of claims reported and costs of those claims. A majority of the hail damage occurs in roof systems and other roofing components.


In the latest version of FM 1-24, dated October 2014, FM Global has identified a new "VSH" region, encompassing Oklahoma, Kansas and some northern counties in Texas. FM 1-24's Table 3 identifies the specific northern Texas counties.

To access FM Global Data Sheets, including FM 1-24—"Hail Damage," go to [www.professionalroofing.net](http://www.professionalroofing.net).

22 [www.professionalroofing.net](http://www.professionalroofing.net) DECEMBER 2017

*Professional Roofing, December 2017*  
[Link to access this article](#)

**RESEARCH+TECH**



**Designing for hail resistance**  
Did you know FM Global has updated its hail design guidance?  
by Mark S. Graham

**In March, property and building loss leader** FM Global updated its Property Loss Prevention Data Sheet 1-24, "Hail Damage" (FM 1-24). If you work on buildings insured by FM Global, you should be aware of its latest hail-resistance guidelines and the effects they may have on roof system selection and design.

**FM 1-24**  
FM 1-24 provides best practices guidelines to maintain the potential for hail damage to buildings, roof-associated equipment and other outdoor equipment. FM Global intends FM 1-24 and its other Property Loss Prevention Data Sheets to apply to its insured buildings. However, some designers use the Property Loss Prevention Data Sheets as design guidelines for buildings (and/or equipment) other than those insured by FM Global.

FM Global controls hail damage in an widespread, harmful affecting many areas of the world that can severely damage building roof systems, roofing HVAC units and skylights. Cooling towers and exposed glass and plastic components of outdoor equipment also can be

20 [www.professionalroofing.net](http://www.professionalroofing.net) MAY 2018

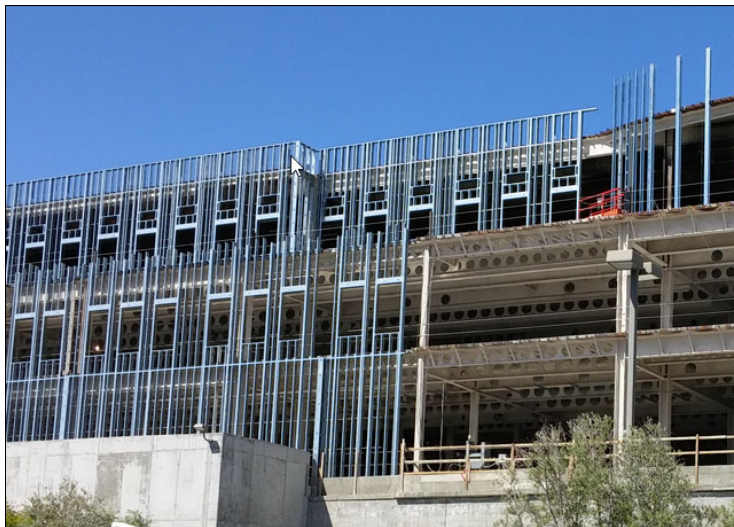
*Professional Roofing, May 2018*  
[Link to access this article](#)

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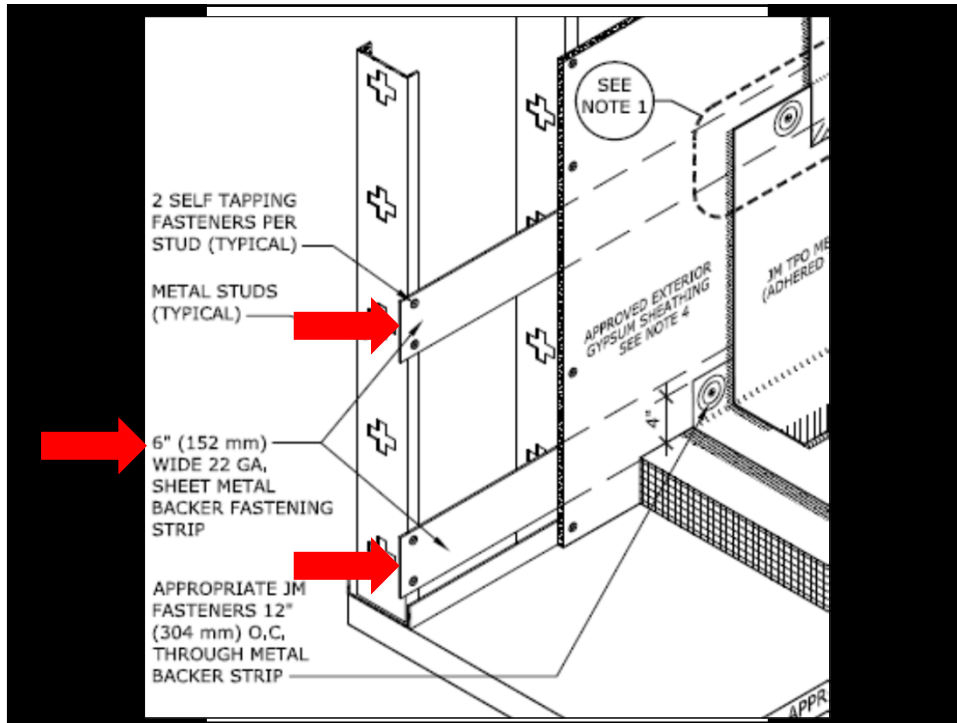
**Metal stud-framed parapet walls**

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**Metal stud-framed parapet walls**



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**“Fully” adhered**

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**TECH TODAY**

**The fully adhered misnomer**  
Terminology can create unrealistic expectations within the roofing industry  
by Mark S. Graham

**NRCA recommends the term "fully adhered" be avoided**

defined, the 100 percent or more.

professionals apply adhesive in a single, rigid board fully cannot be

one, complete membrane and use to improve membrane and joints.

in insulation, it is needed to be U.S. product insulation, verification requirements require a board to be installed in such a depth accuracy.

Because these tend to lap roof membrane and remain exposed, irregular, non-smooth roof deck surfaces create similar situations. Because board type insulation is relatively rigid, it generally will not readily conform to irregularities in roof deck substrates. Individual rigid boards tend to rest on the high points in a roof deck finished surface and span the low points.

As a result, rigid board insulation seldom is completely adhered to roof deck substrates. It generally is adhered at the relative high points in the roof deck's surface and may be partially or marginally adhered and even unadhered at the relative low points. Specifying smaller insulation board sizes (4 by 4 feet instead of 4 by 8 feet) generally is suggested to minimize rigid insulation boards from spanning substrate low-point irregularities.

**In practice**

The concept of lacking 100 percent, complete adhesion between two adhered surfaces is not new to the roofing industry; it has long been recognized in the application of built-up roof membranes where weak between-plies can occur. To address this, NRCA's Quality Control Guidelines for the Application of Built-up Roofing indicates interply overlapping joints should be continuous; however, weak or limited size are permitted provided overlapping joints do not occur between two or more plies. NRCA has maintained this position since the late 1970s, and it has become well-accepted by the roofing industry.

As it applies to adhering rigid board insulation to continuously applied adhesive applications, actual adhesion rates of about 60 to 70 percent are common (even less in some specific instances) in successfully performing adhered roof systems.

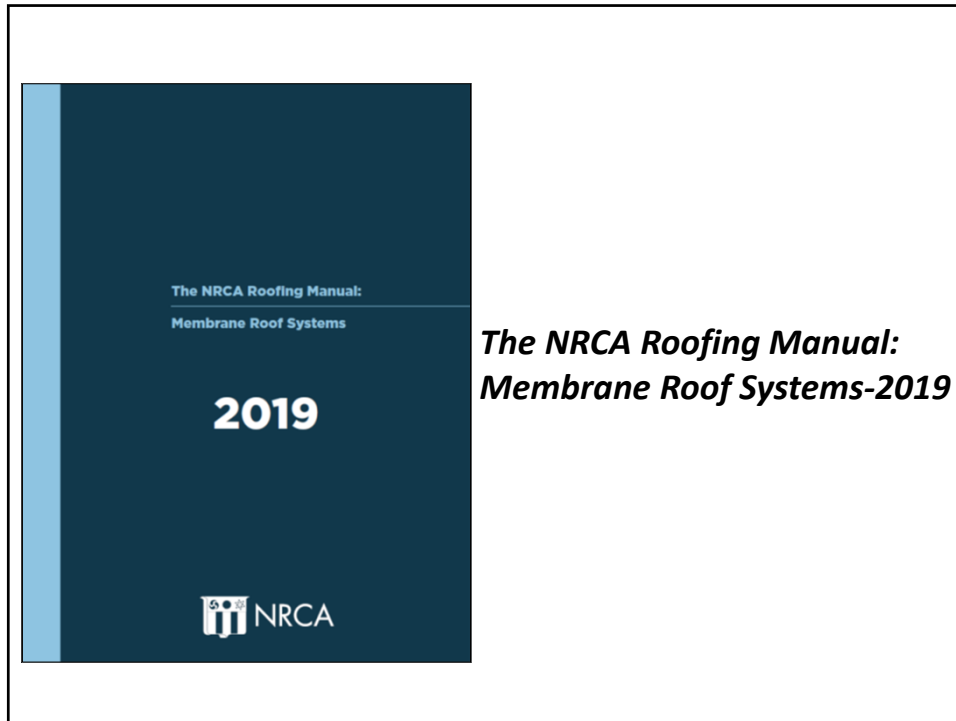
On this basis, NRCA recommends the term "fully adhered" be avoided and suggests the term "adhered" for field applications because it is more realistic. ■■■

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**Questions... and other topics**

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### NRCA App

- NRCA App available on the Apple Store and Google Play Store for tablets
- iPhone App also available
- Register within App as being an NRCA member
- The NRCA Roofing Manual is viewable to NRCA members
- Favorite and send pages features

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## Manual online

[www.nrca.net](http://www.nrca.net)

- Available to all NRCA member registered users (multiple users per member company)
- “Members only” section, click on “My account”, the “Electronic file”
- View, download and print

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## NRCA website

[www.nrca.net](http://www.nrca.net)

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