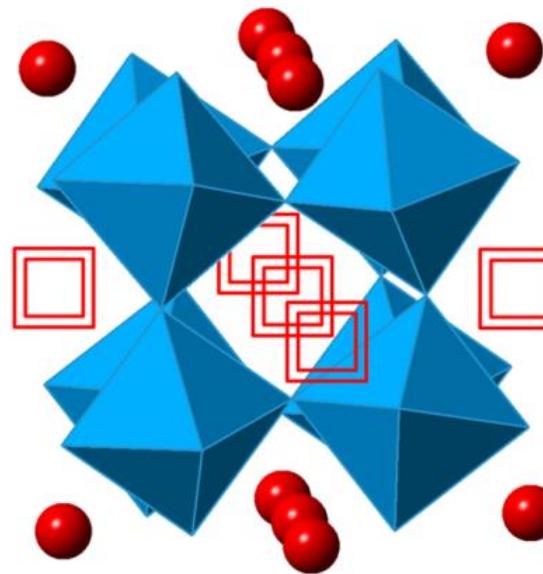
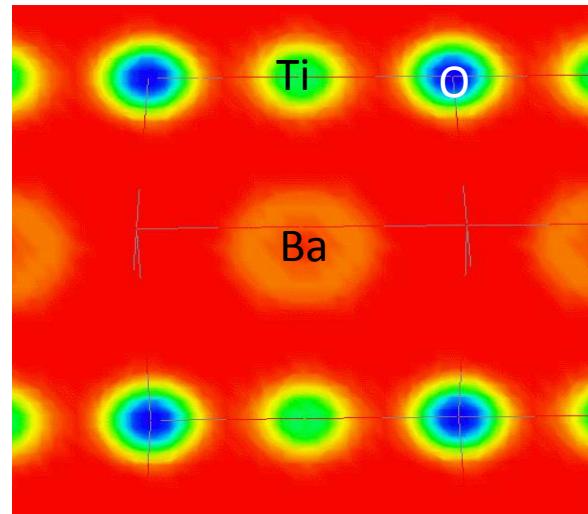


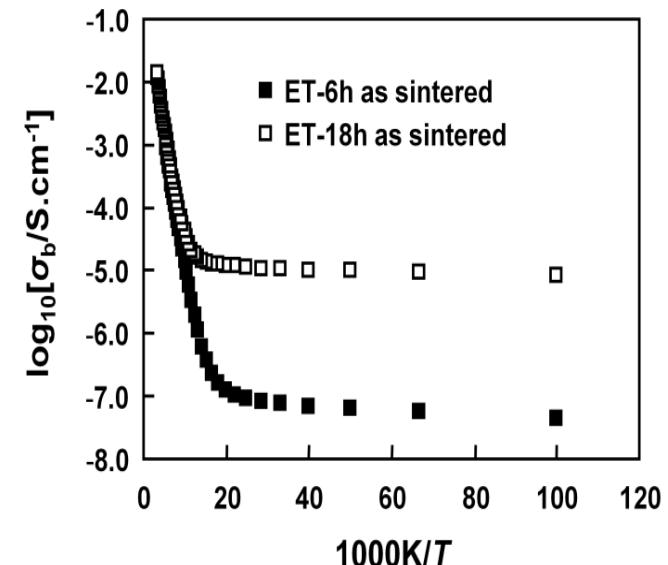
Electrical heterogeneity and anomalous conductivity behaviour in reduced titanates.



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Acknowledgements

La-doped (Sr,Ba)TiO₃

Zhilun Lu, Huairuo Zhang, Ian Reaney; Finlay Morrison, Anthony West,
Colin Freeman, James Dawson, John Harding

EuTiO₃

Matthew Ferrarelli, Julian Dean

Funding: EPSRC

Topics

- **Background:** Doping Mechanisms
- **Topic 1:** La-doped ATiO₃ (A= Ba, Sr) Influence of doping mechanisms and metal vacancies on reduction characteristics.
- **Topic 2:** EuTiO₃ (and related titanate-based perovskites) often show anomalous temperature-independent conductivity < 100 K . Origin?
- **Conclusions.**

Background

- Doping Mechanisms in $A^{2+} Ti^{4+}O_3$ perovskites.

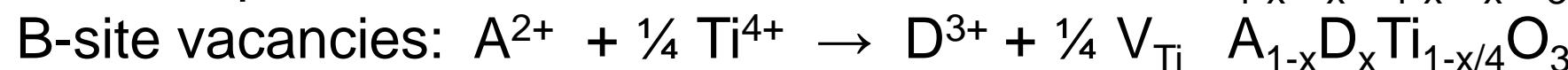
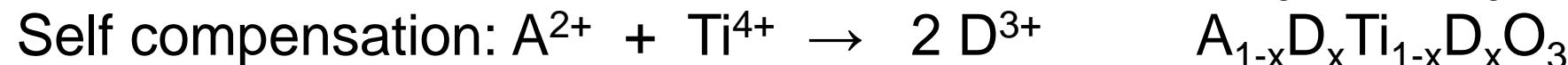
- Oxygen-loss: $O^{2-} \rightarrow \frac{1}{2} O_2(g) + 2 e^- + V_O$



- Donor doping: (eg La^{3+} for Ba or Sr)

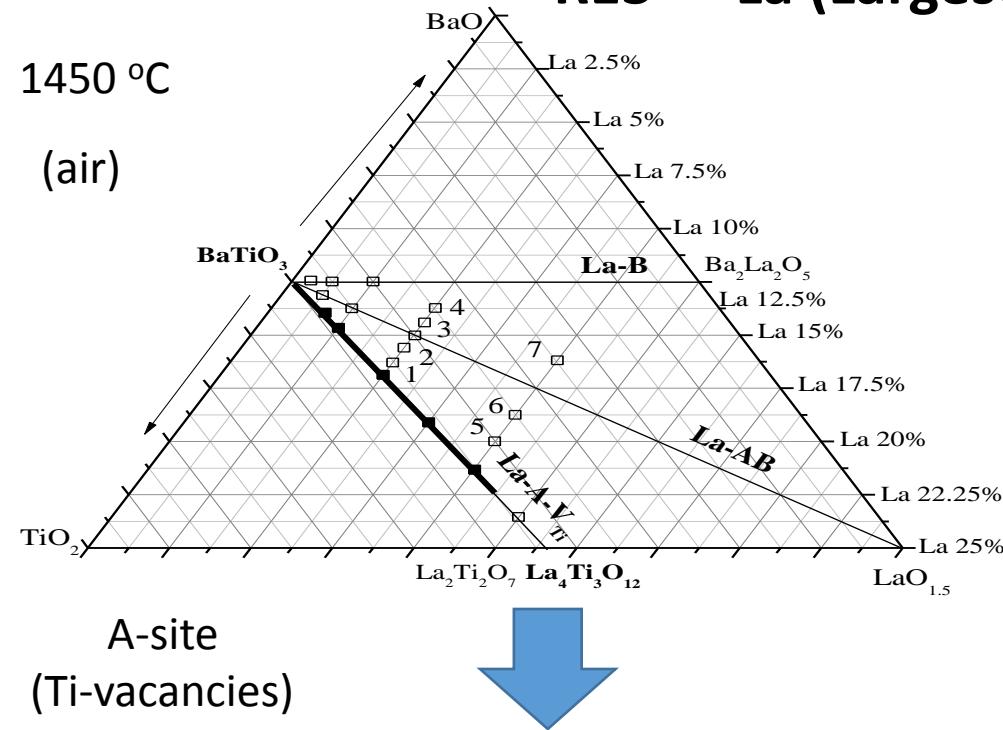


However, ionic compensation is also possible!

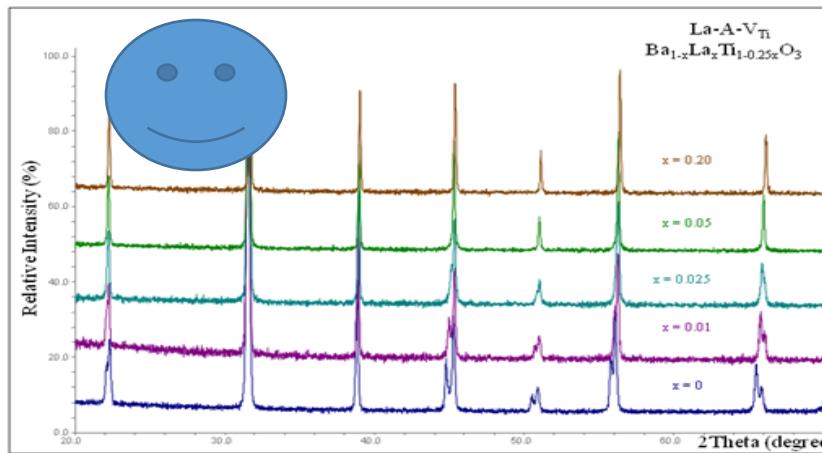


Big Question: which mechanism dominates and do we have an issue with thermodynamics versus kinetics, especially in bulk ceramics.

$\text{RE}^{3+} = \text{La}$ (Largest RE)

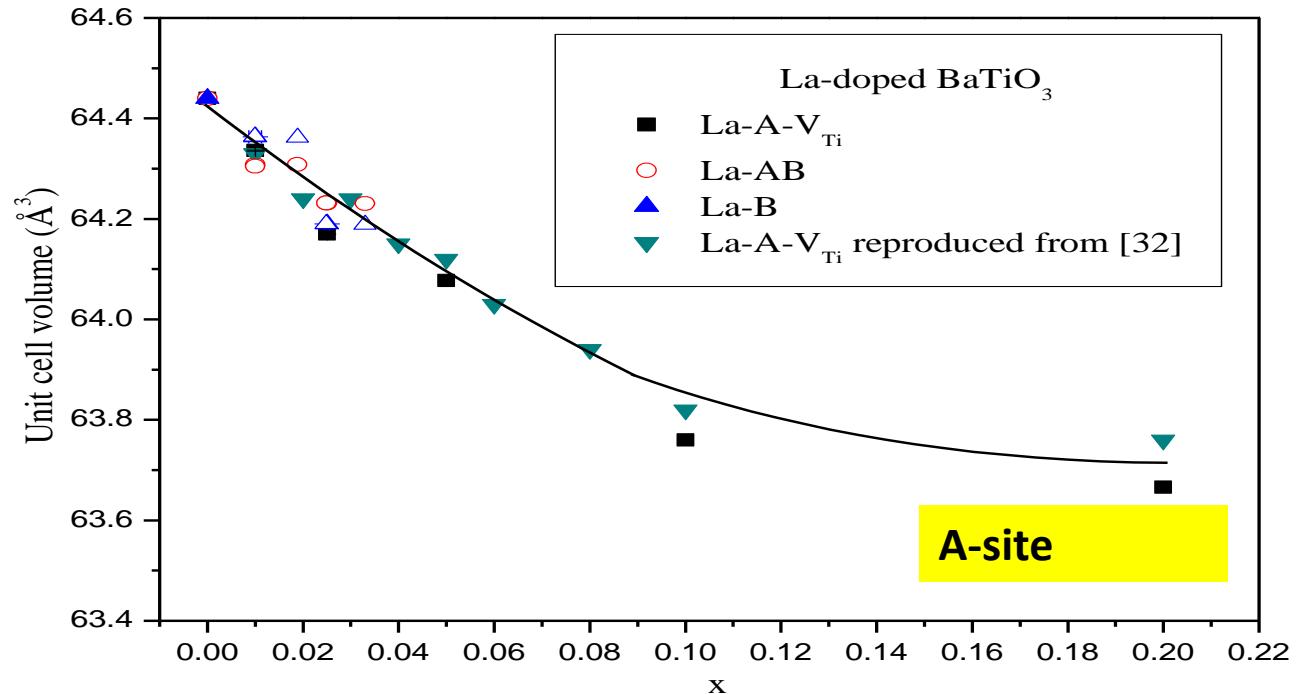


A-site
(Ti-vacancies)



$\text{Ba}_{1-x}\text{La}_x\text{Ti}_{1-x/4}\text{O}_3$ $0 \leq x \leq 0.20$

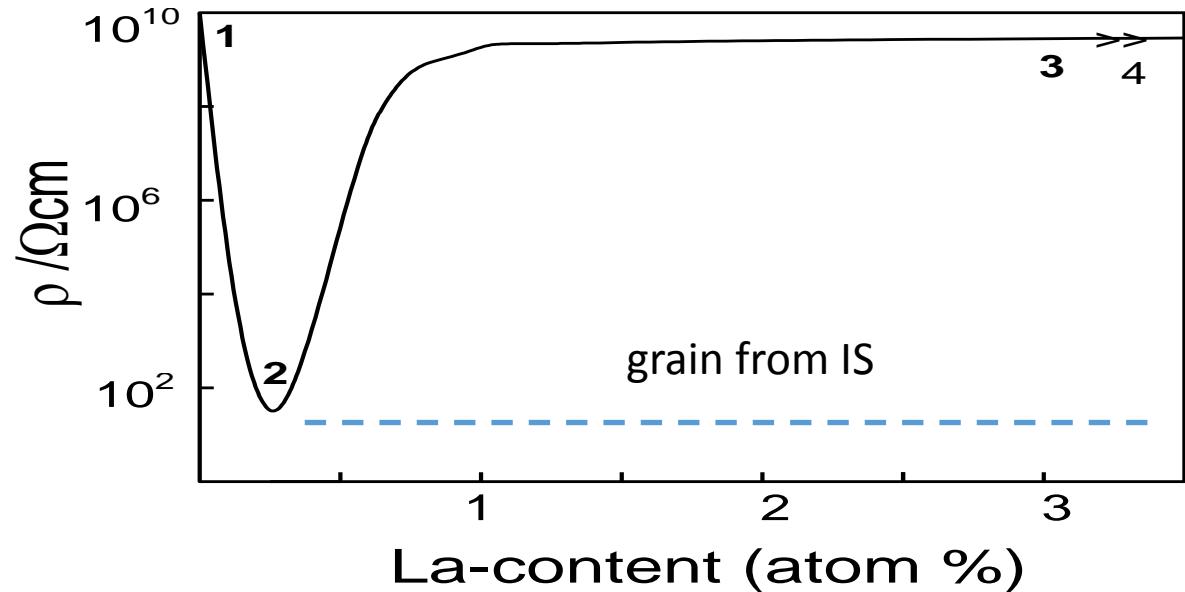
$\text{Ba}_{1-x}\text{La}_x\text{Ti}_{1-x/4}\text{O}_3$ $0 \leq x \leq 0.20$



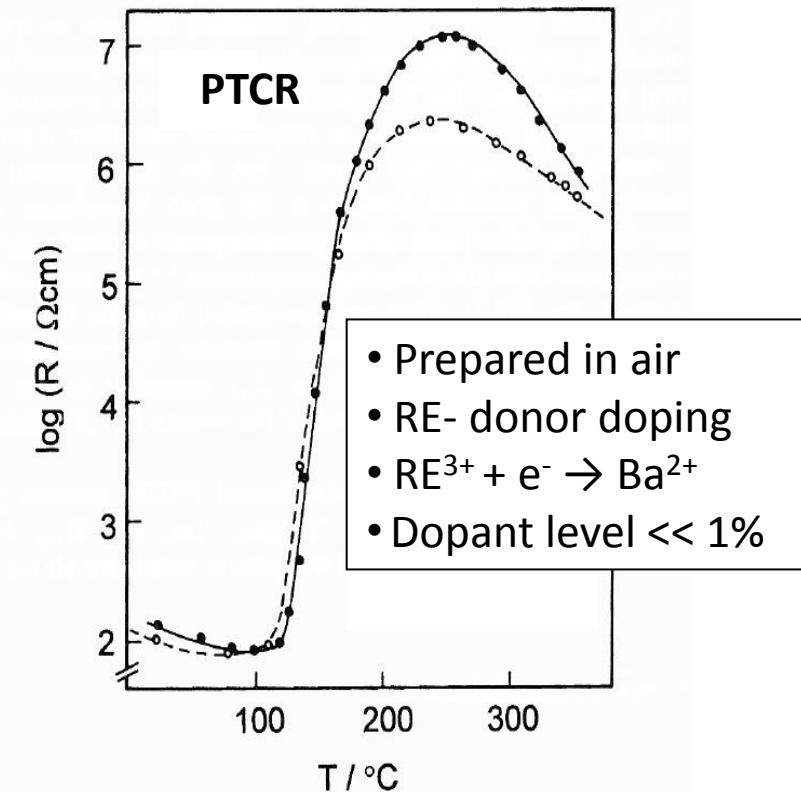
A-site

- r_{12} $\text{Ba} = 1.61 \text{\AA}$ and $\text{La} = 1.36 \text{\AA}$
- r_6 $\text{Ti} = 0.605 \text{\AA}$ and $\text{La} = 1.032 \text{\AA}$
- $\Delta A = r_{\text{Ba}} - r_{\text{La}} = 0.25 \text{\AA}$
- La substitutes exclusively on the A-site.
- No evidence for extensive ss via electronic compensation (donor-doping) mechanism for samples prepared in air or O_2 at 1350°C .

The doping mechanism in La-BaTiO₃



R_{\min} is obtained for 0.3 -0.5 atom % doping (ptcr devices) heated in air > 1350 °C followed by rapid cooling.



Is there a change in doping mechanism with La-content?

Low x : donor (electronic) doping, $\text{La}^{3+} + e^- \rightarrow \text{Ba}^{2+}$

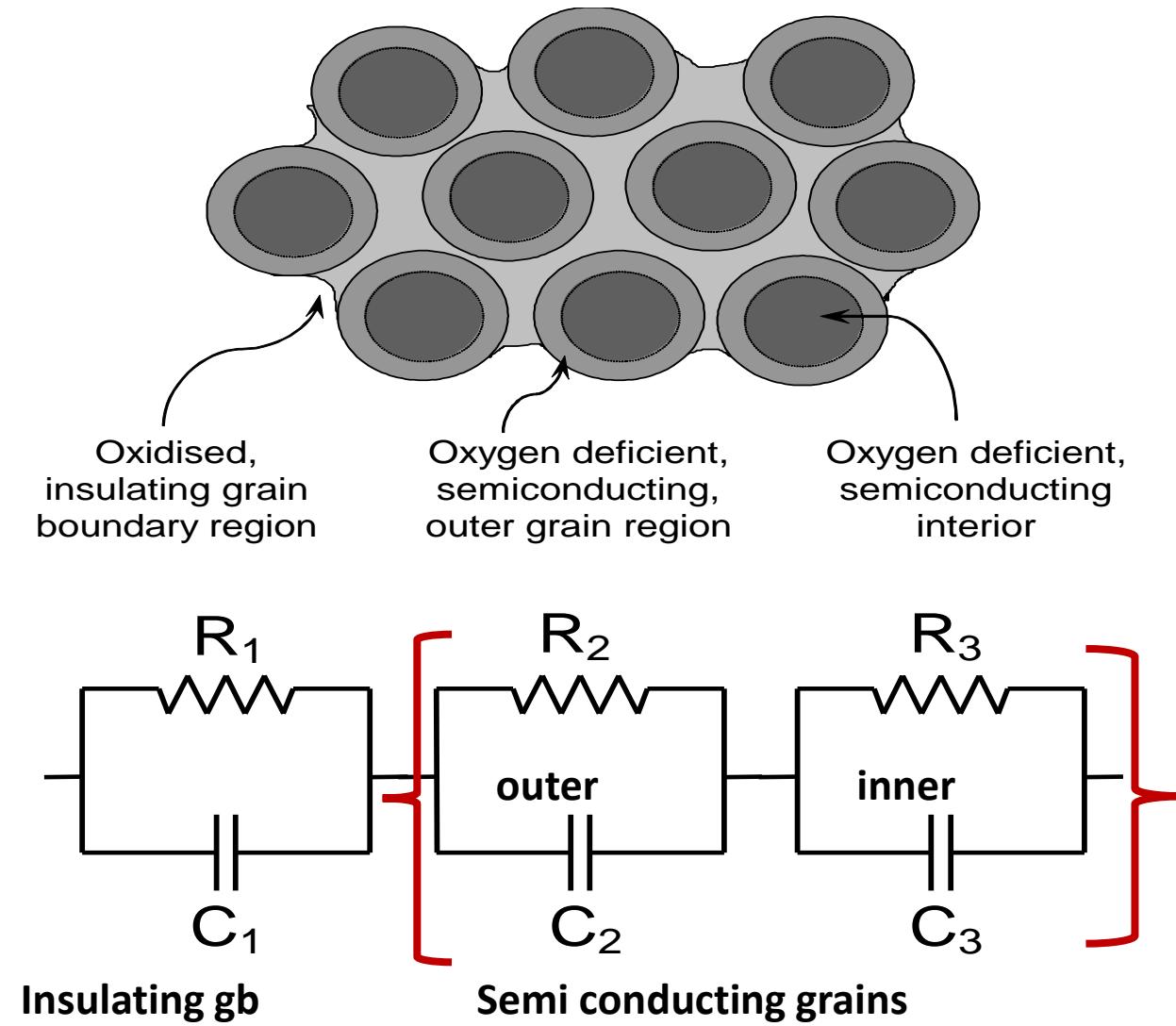
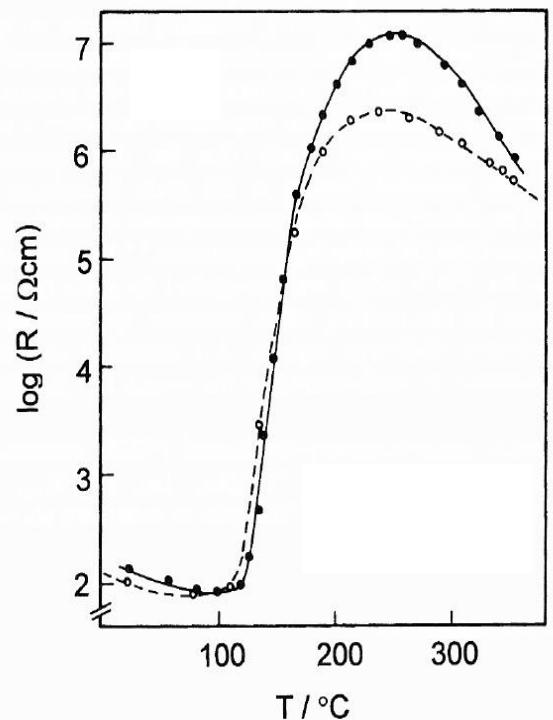
High x : Ionic compensation, $\text{La}^{3+} \rightarrow \text{Ba}^{2+} + \frac{1}{4} \text{Ti}^{4+}$

• RE used to induce semiconductivity

Atomistic simulations from Lewis and Catlow (1986) suggested donor doping to be energetically more favourable

Electrical microstructure for $x = 0.003$ (La) prepared in air at $1350\text{ }^{\circ}\text{C}$

- E_a (bulk) $\sim 0.06 - 0.1\text{ eV}$
(n-type)
- E_a (gb) $\sim 0.9 - 1.2\text{ eV}$



BaTiO₃ Model Development

Objectives

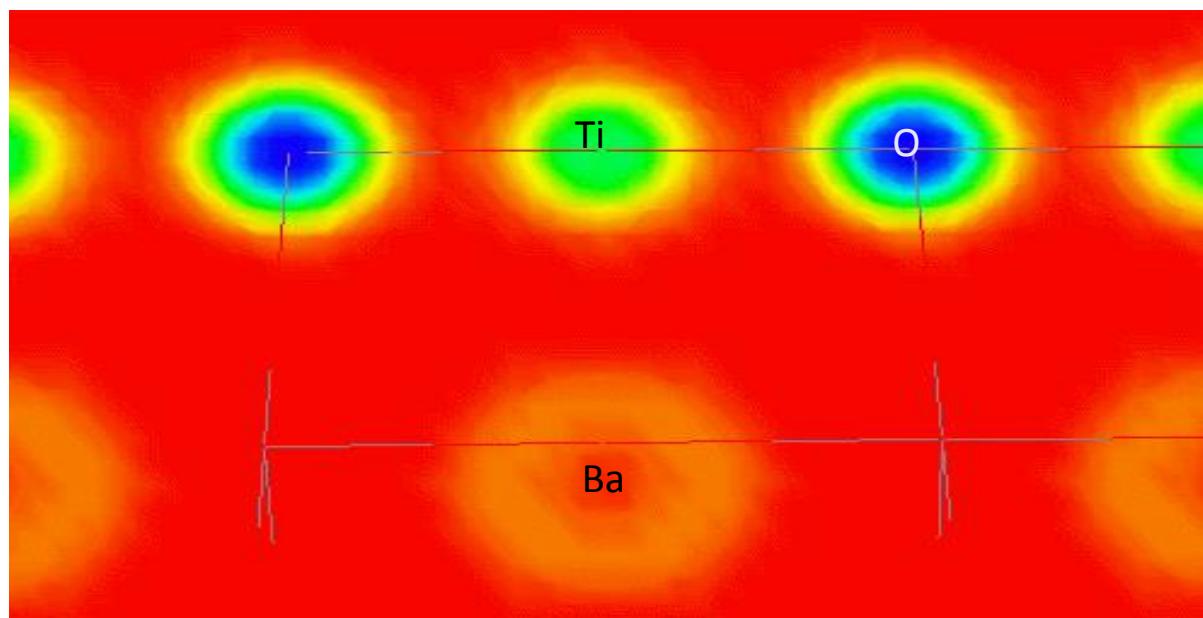
Previous simulations fail to describe defect chemistry because end members (BaO, TiO₂) are not energetically correct. Therefore the energetic balance for solution chemistry of defects is wrong. Design potential that models the entire range.

New Model Features

Ab initio methods have shown that the Ti-O bond has a degree of covalency. It is now represented with a partially bonding term (Lennard-Jones) rather than a full ionic description.

Angular (three-body) terms added for the O-Ti-O interaction to account for strain effects in the TiO₆ octahedra.

Structure	Cohesive Energy (eV)	
	Experiment	Lewis and Catlow [1]
TiO ₂ (rutile)	-125.5	-112.47
BaO	-31.90	-34.57
c-BaTiO ₃	-159.86	-148.02
h-BaTiO ₃	-159.73	-147.69



[1] G. V. Lewis and C. R. A. Catlow, J. Phys. Chem. Solids, **47** (1986) 89-97

BaTiO₃ Model Development - Results

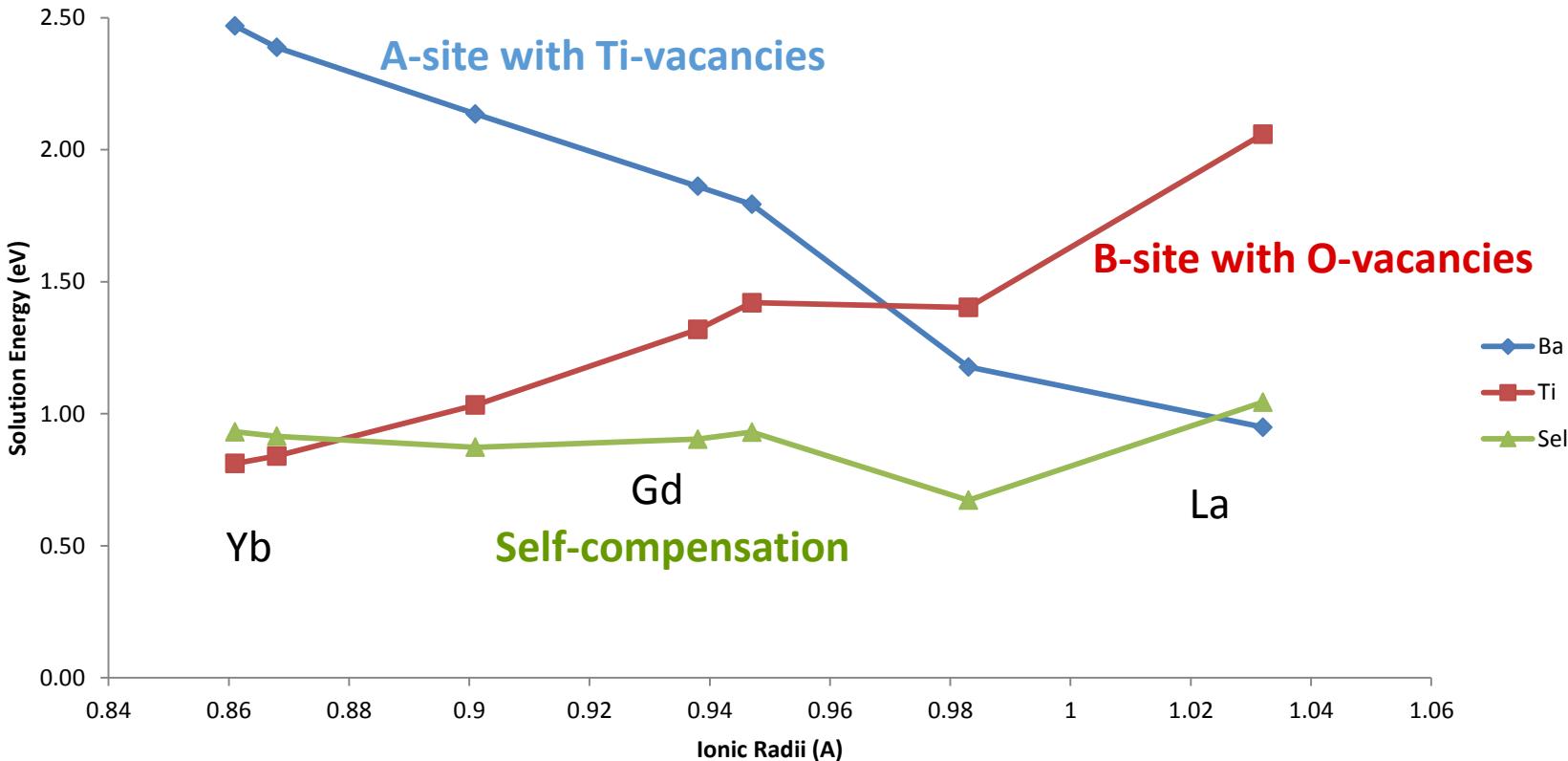
Structure	Lattice/Cohesive Energy (eV)		
	Experiment	Lewis and Catlow [1]	This work [2]
TiO ₂ (rutile)	-125.5	-112.47	-129.49
BaO	-31.90	-34.57	-31.72
c-BaTiO ₃	-159.86	-148.02	-160.02
h-BaTiO ₃	-159.73	-147.69	-160.85

Structure	Lattice parameters		
	Experiment	Lewis and Catlow [1]	This work [2]
c-BaTiO ₃	4.012\90.0	3.960\90.0	4.105\90.0
h-BaTiO ₃	5.724\13.965\90.0\120.0	5.669\14.008\90.0\120.0	5.962\14.550\90.0\120.0

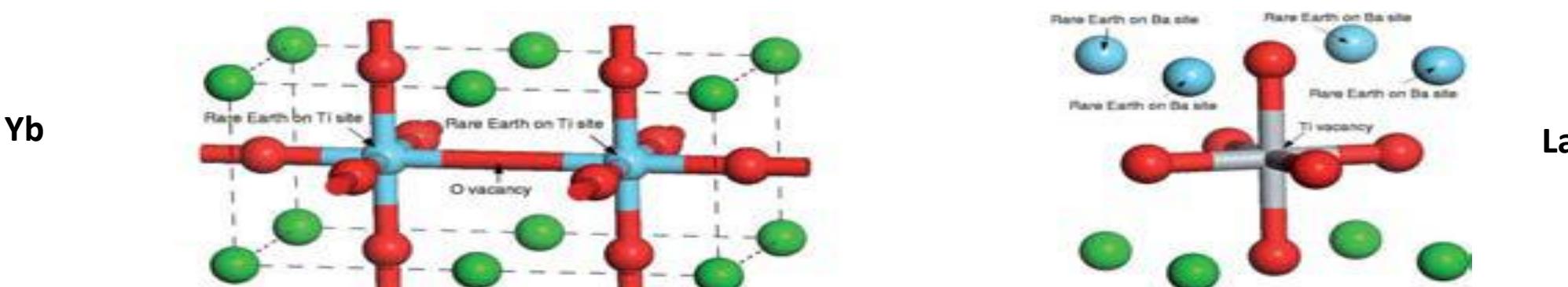
[1] G. V. Lewis and C. R. A. Catlow, J. Phys. Chem. Solids, **47** (1986) 89-97

[2] C.L. Freeman, J.A. Dawson, H-R Chen, J.H. Harding, L. Ben and D.C. Sinclair, . J. Mater. Chem., **21** (2011) 4861–4868.

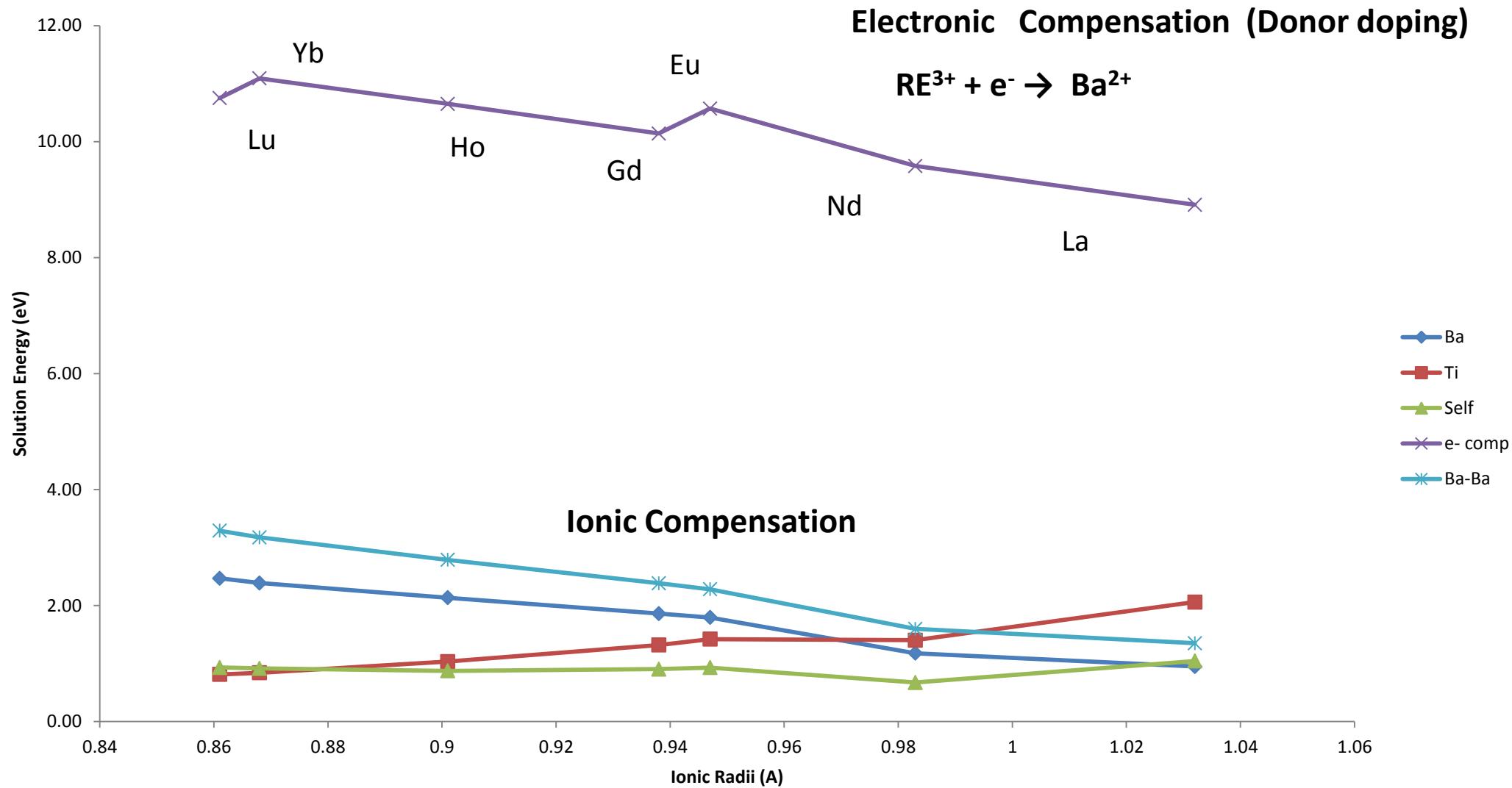
Sheffield Model : ionic compensation mechanisms



- Excellent agreement between experimental results and simulations.



Revised Model: Colin Freeman (Sheffield) Potentials



- Donor doping on A-site is very unfavourable : $\text{RE}^{3+} + \text{e}^- \rightarrow \text{Ba}^{2+}$

Electron Compensation – Sheffield model vs. Lewis & Catlow model

Dopant	Solution Energy (no binding) (eV)	
Dopant	Lewis & Catlow model	Sheffield model
La ³⁺	0.22	9.06
Gd ³⁺	0.70	10.21
Er ³⁺	0.97	-
Yb ³⁺	-	11.2

Why??

Ti_{Ti}[•] Ti³⁺ substitution at Ti⁴⁺ site requires more energy in Sheffield model (48.03 eV) compared to the L&C model (36 eV)

Alternative mechanism for semiconductivity is required!!

Suggestion: is oxygen loss the source of semiconductivity for samples processed in air?

Calculations for La from the Freeman (Sheffield) model.

Solution energy

- (1) Donor doping of RE $(RE^{3+} + e^- \rightarrow Ba^{2+})$ **9.06 eV**
- (2) Ti-vacancy formation $(RE^{3+} \rightarrow Ba^{2+} + \frac{1}{4} Ti^{4+})$ **1.01 eV**
- (3) Oxygen-loss after Ti-vacancy formation $(O^{2-} \rightarrow \frac{1}{2} O_2 + 2e^-)$ **4.59 eV**

(1) $Ba_{1-x}La_xTiO_3$ **9.06 eV**

(2) + (3) = $Ba_{1-x}La_xTi_{1-x/4}O_{3-\delta}$ **5.60 eV**

- No need to invoke a change in doping mechanism at low levels of doping for s
- The process of oxygen-loss from samples containing Ti-vacancies is still energetically favorable over direct donor-doping.
- This reconciles our electrical data and the phase diagram studies.

Doping mechanisms in La-doped SrTiO₃

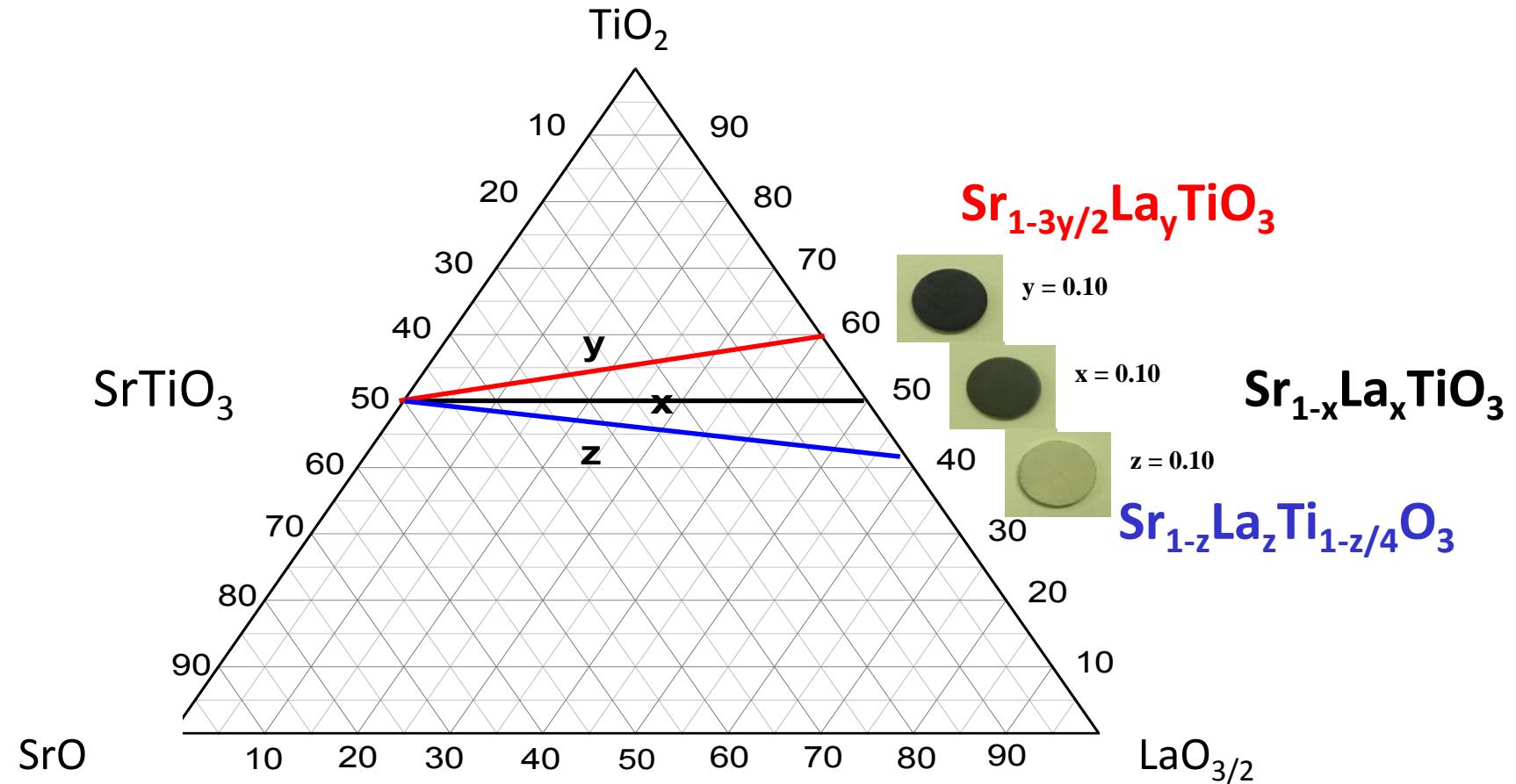
A-site vacancy



Electronic (Donor doping)



B-site vacancy



Solid solution limits in air (1500 °C)

$$0 \leq x \leq 0.30; \quad 0 \leq y < 0.65 \quad (\sim \text{full solid solution}); \quad 0 \leq z \leq 0.15$$

All single-phase ceramics (x, y, z = 0.10) sintered in flowing O₂ at 1500 °C

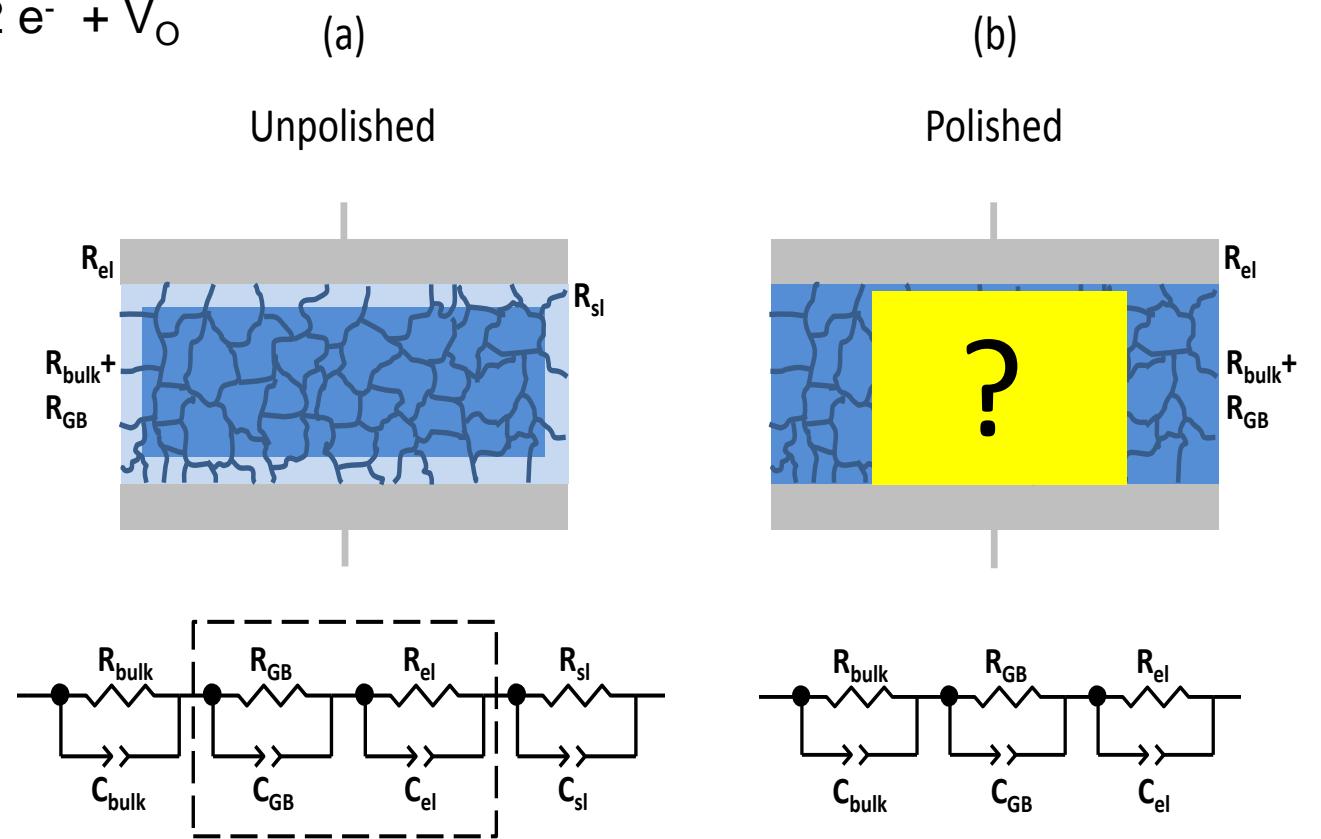
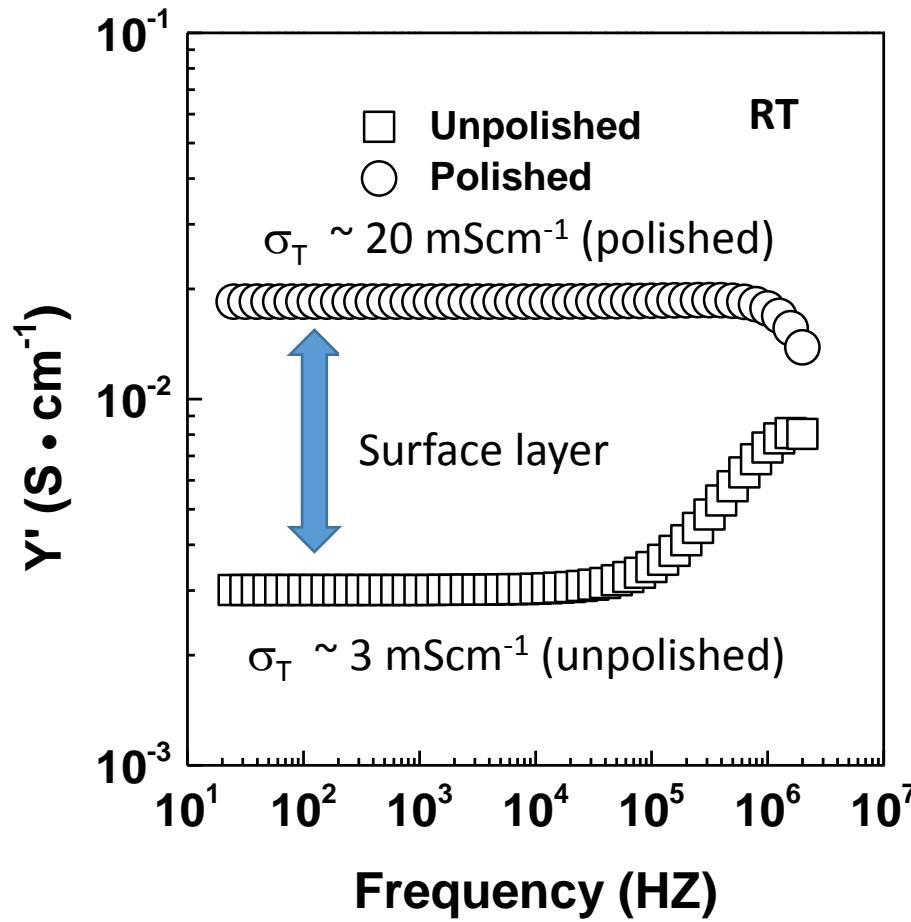
Bulk conductivity is highest for A-site vacancy (y = 0.10) sample!

Note: electrical properties are very dependent on processing conditions

Resistive surface layers and non-ohmic contact problems: Impedance Spectroscopy (IS)

Undoped $\text{SrTiO}_{3-\delta}$ ceramic processed in 5 % H_2 /95% H_2 at 1500 °C for 6 hrs

- Oxygen-loss: $\text{O}^{2-} \rightarrow \frac{1}{2} \text{O}_2 (\text{g}) + 2 \text{e}^- + \text{V}_\text{O}$



Resistive surface layer that can be removed by polishing

Resistive surface layer lowers the total ceramic conductivity by one order of magnitude.

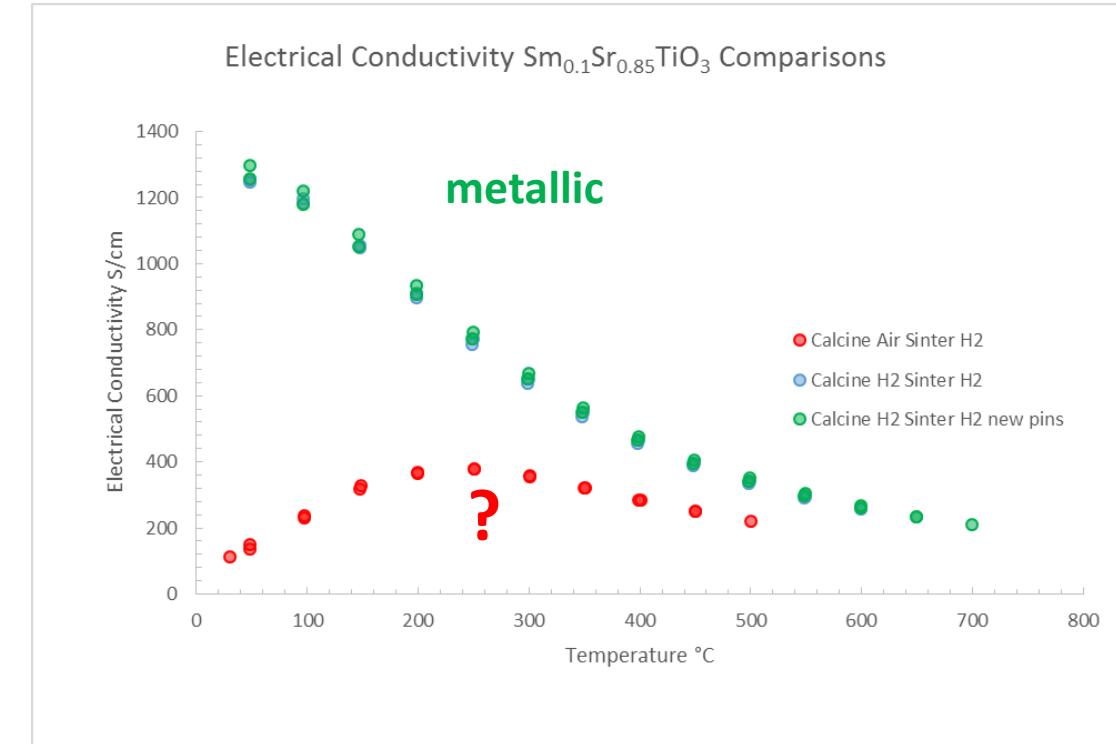
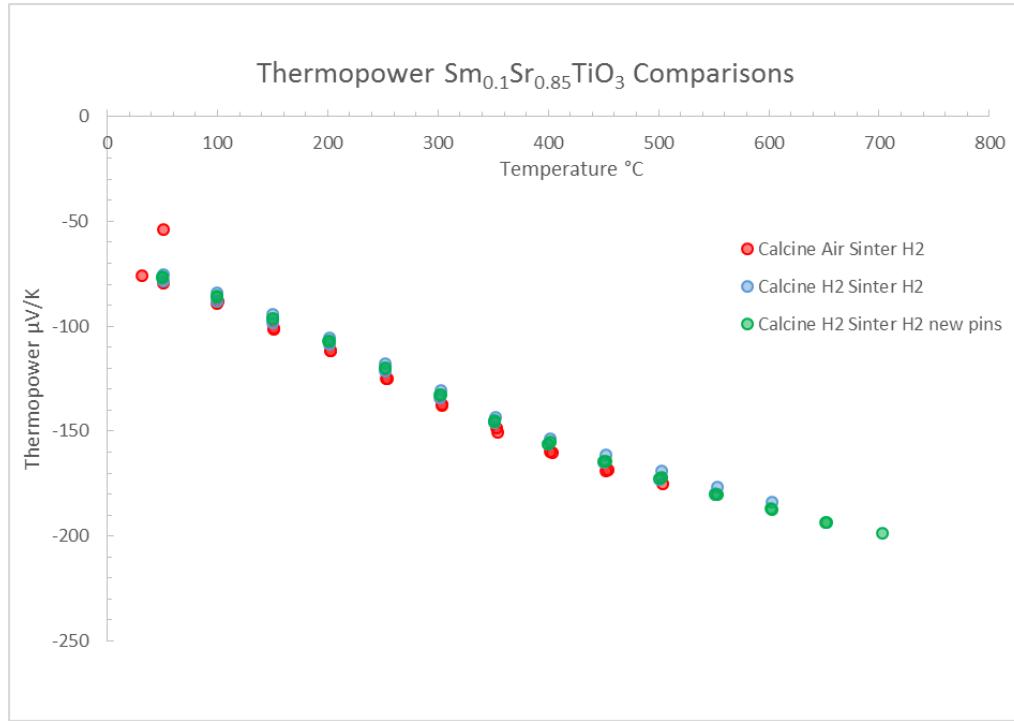
Semiconducting/metallic oxide
Non-ohmic contact

Too conductive to measure by IS,
even at 10 K

4 probe conductivity: Influence of limited reduction at grain boundaries?

$\text{Sm}_{0.1}\text{Sr}_{0.85}\text{TiO}_{3-\delta}$ ceramics :

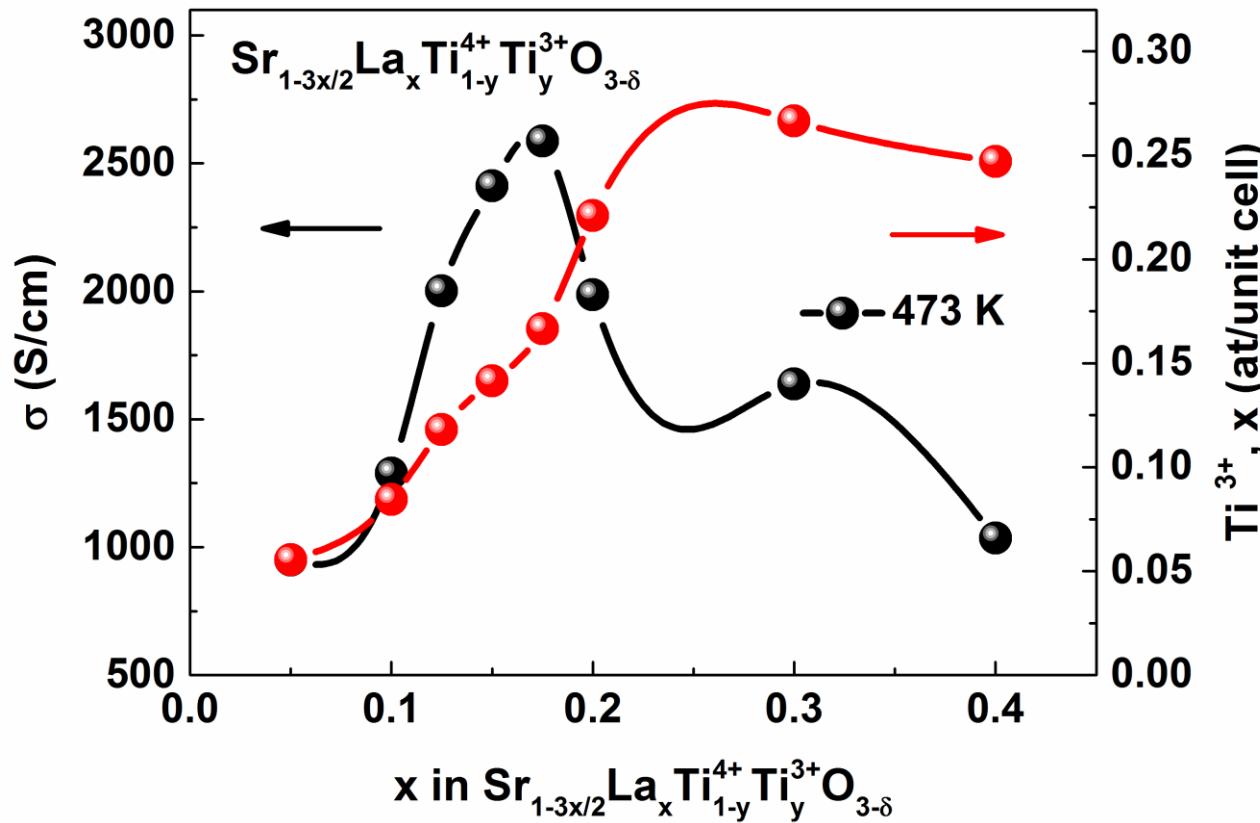
- (●) powder calcined in air (1300 °C); pressed and sintered in 5 % H₂/95% H₂ (1500 °C for 6 hrs)
- (●) powder calcined in 5% H₂ (1300 °C); pressed and sintered in 5 % H₂/95% H₂ (1500 °C for 6 hrs)



Seebeck coefficient (Thermopower) is the same for both samples

Low Temp σ is very different but high Temp σ is similar for both samples: **extrinsic effect – limited reduction/grain boundaries?**

4-probe conductivity, Ti³⁺ content and re-oxidation characteristics

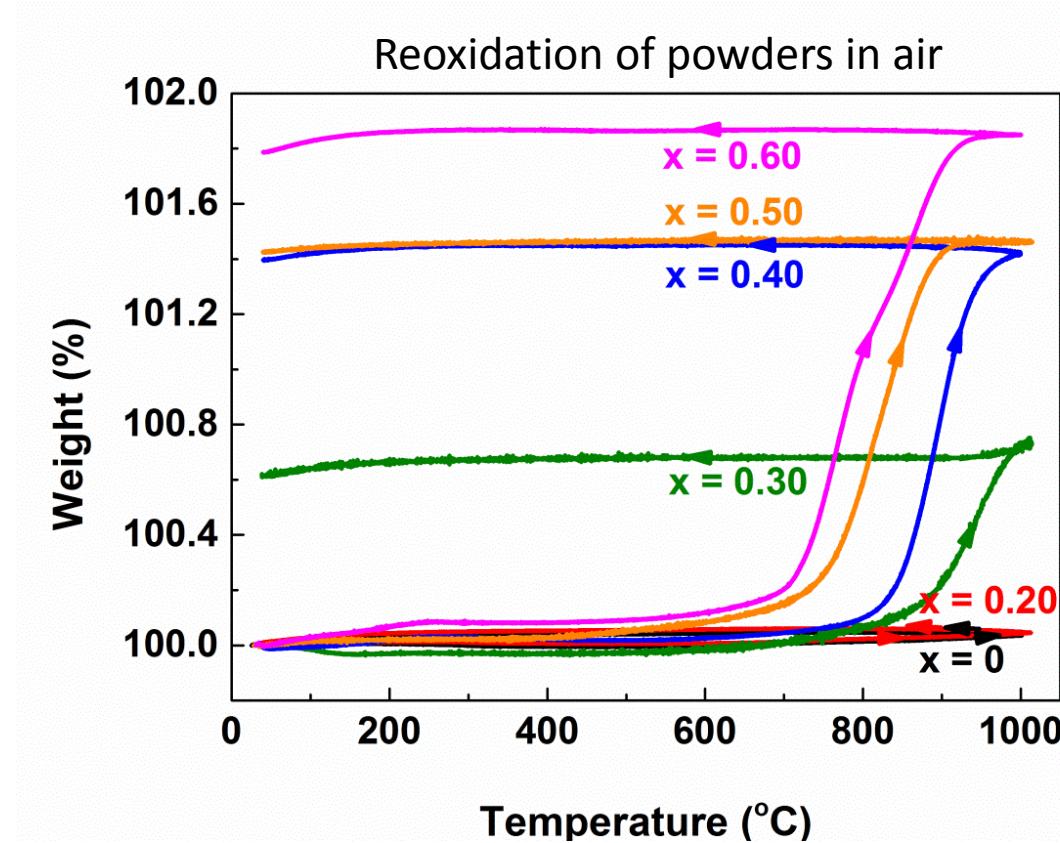


Conductivity maximum at ~ 15 % Ti³⁺

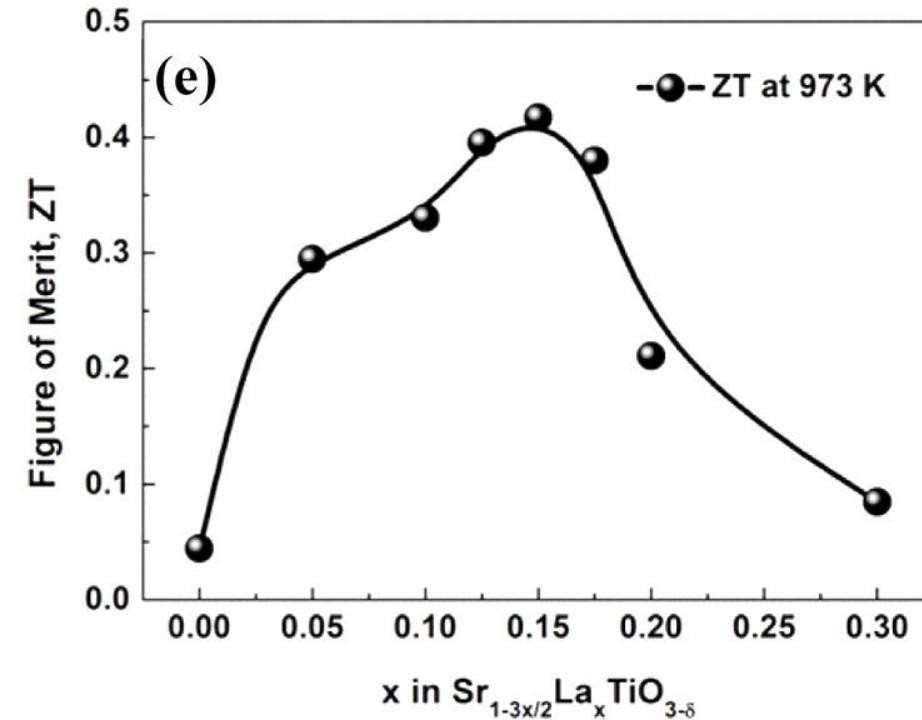
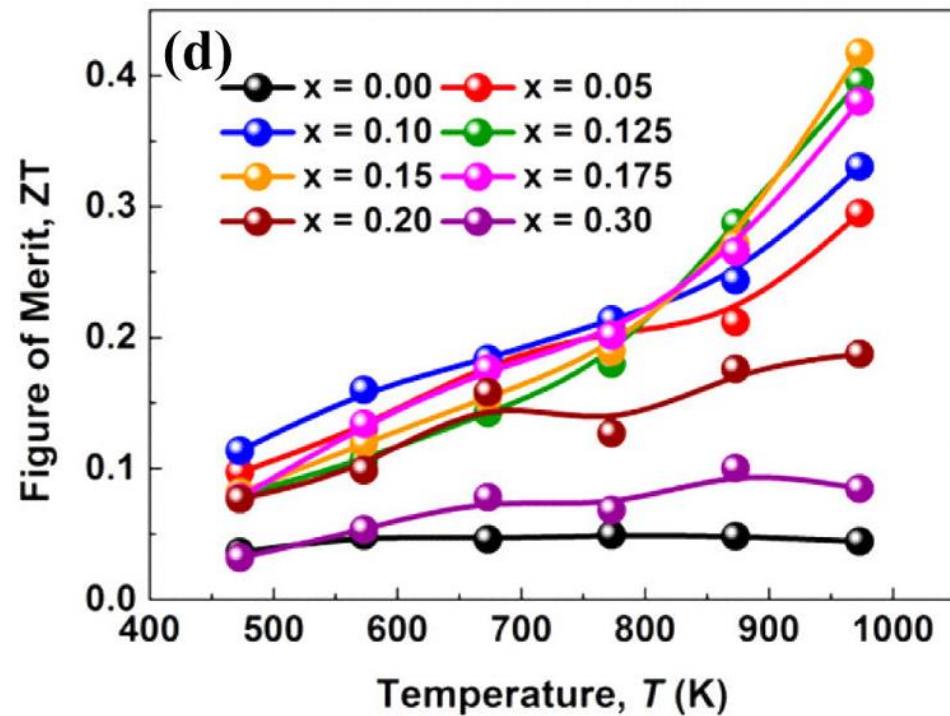
Complex conductivity behaviour: doesn't scale simply with Ti³⁺ content

Reoxidation of samples with > 20 % Ti³⁺ is rapid

Excellent n-type thermoelectric oxides (see next presentation)

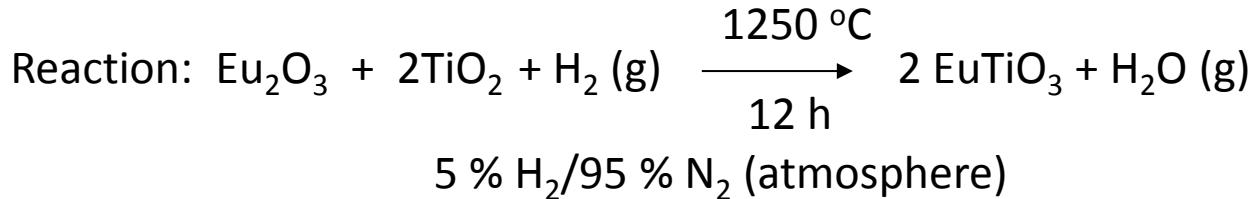


$\text{Sr}_{1-3x/2}\text{La}_x\text{TiO}_3$: Figure of Merit (ZT)



- ZT
 - Increases with increasing T
 - Increases with increasing La up to $x = 0.15$
 - Maximum thermoelectric properties at $x = 0.15$ where $ZT = 0.41$ at 973K

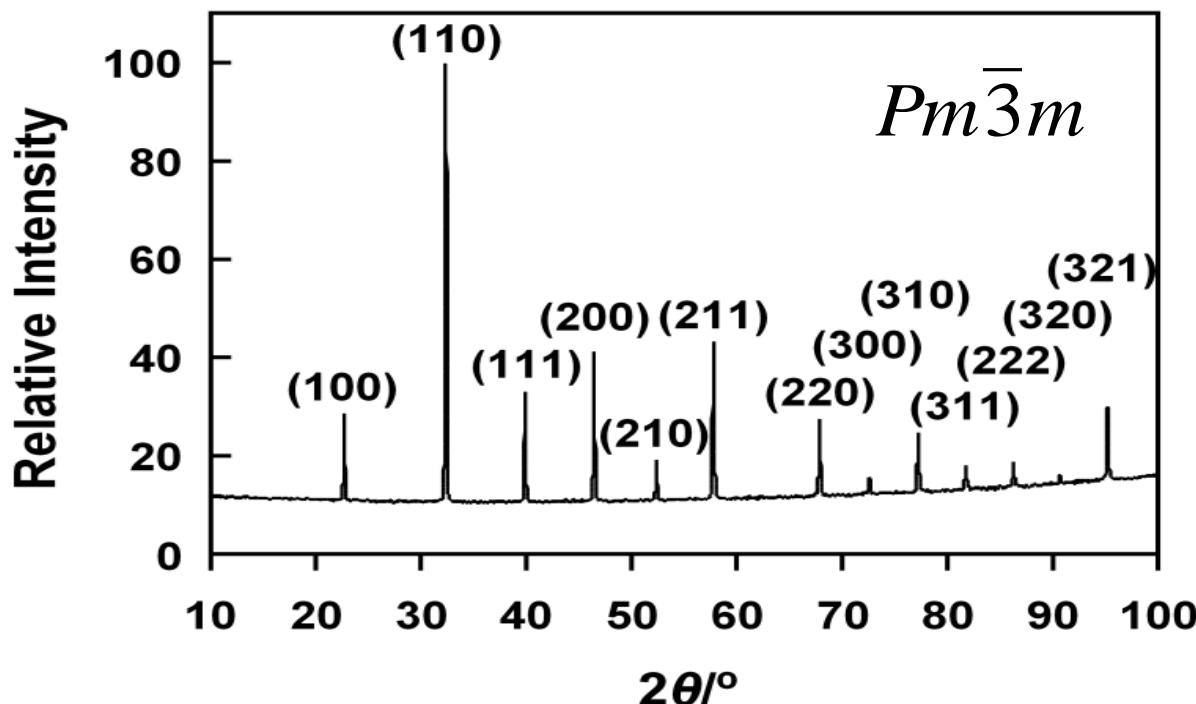
Synthesis & Stability of EuTiO₃ ceramics



Ceramics : Sinter EuTiO₃ green bodies at 1500 °C in 5 % H₂ (g) for 6 – 18 hours

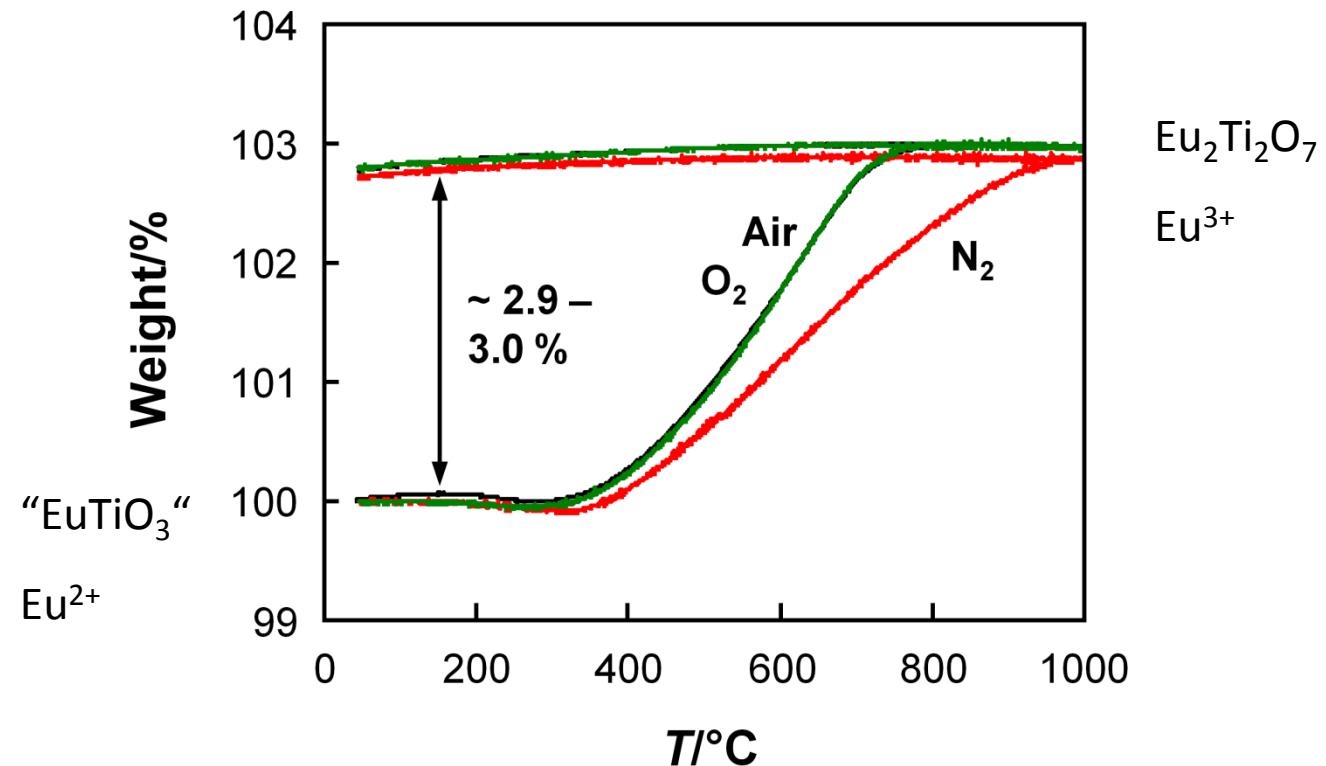
Heating/cooling rate = 5 °C/min

Annealed ceramics in Air, O₂ and N₂ at 200 °C for 24 hours



Thermogravimetric Analysis (TGA)

Crushed
powder from
6 h ceramic



- “EuTiO₃” gains weight at > 300 °C.
- Up-take of O₂ causes oxidation to Eu₂Ti₂O₇ (Eu³⁺, pyrochlore) [expect ~ 3.2 %]
- No evidence for a large amount of oxygen deficiency in as-prepared “EuTiO₃”
- Exposure to ppm levels of O₂ at T > 300 °C is sufficient for decomposition.
- ‘Safe’ working range for EuTiO₃ in air/N₂ is ~ 250 °C

Source of semiconductivity in 'Eu²⁺Ti⁴⁺O₃'

$\sigma_b \sim 15 \text{ mScm}^{-1}$ at 300 K : $\mu = 4 \text{ cm}^2.\text{V}^{-1}\text{s}^{-1}$: $n \sim 2.3 \times 10^{16} \text{ cm}^{-3}$ at 300 K

As-prepared EuTiO₃ is a lightly-doped semiconductor.

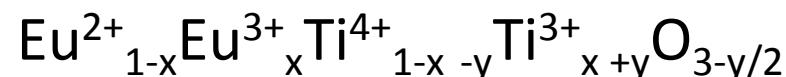
(i) Oxygen-stoichiometric but with incomplete reduction of Eu³⁺



(ii) Oxygen-deficient with partial reduction of Ti⁴⁺

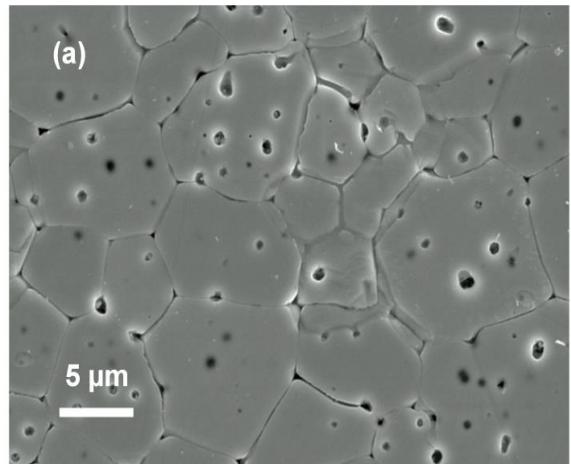


or could it be (i) + (ii) ?

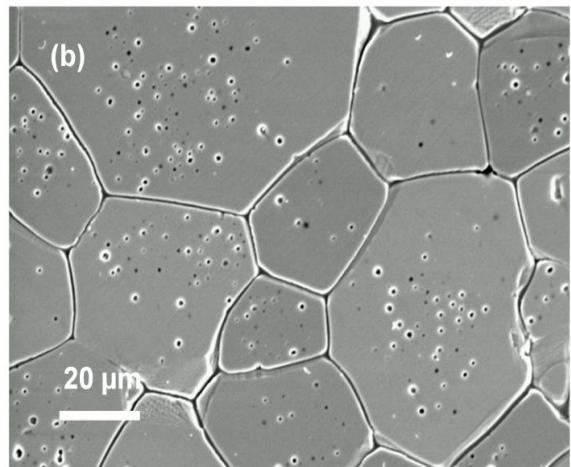


Difficult to establish mechanism (ii) via 'conventional methods such as TGA

Dense ceramics



6 hr
sinter

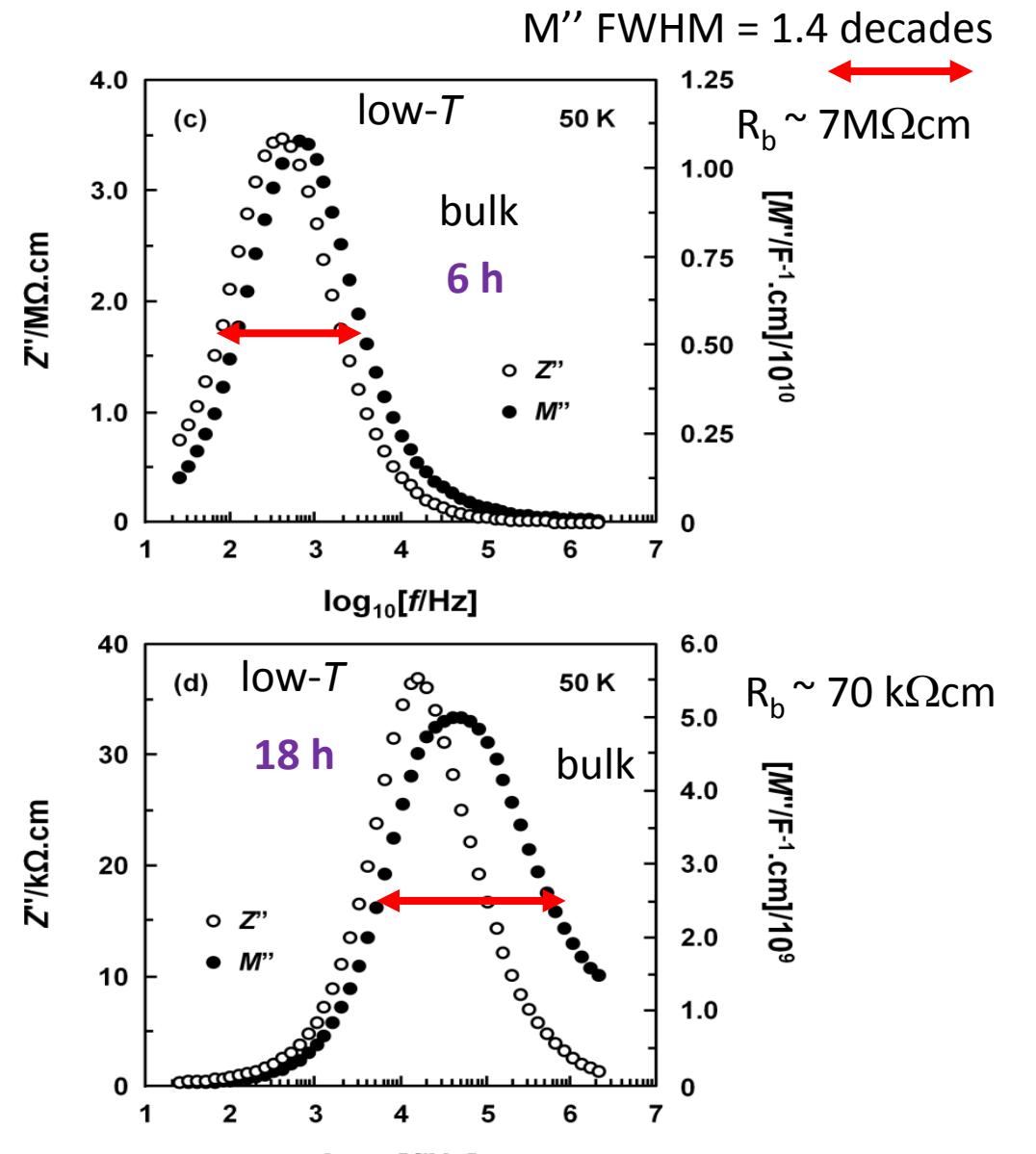


18 hr
sinter

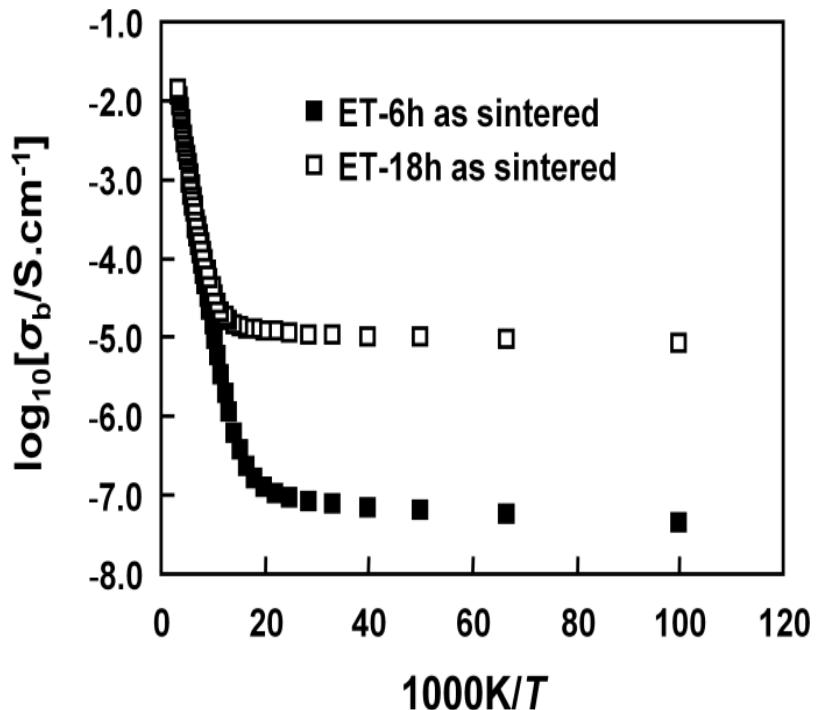
Grain growth increases with sintering time

- Both ceramics are heterogeneous : R_b is similar for $T > 100 \text{ K}$
BUT

below 100 K 18 hr sinter is more conductive and grains are more heterogeneous



Bulk conductivity = $1/R_b$



Two regions.

(High- T) 100 - 300 K $E_a \sim 80$ meV

R_b (6 h) $\sim R_b$ (18 h)

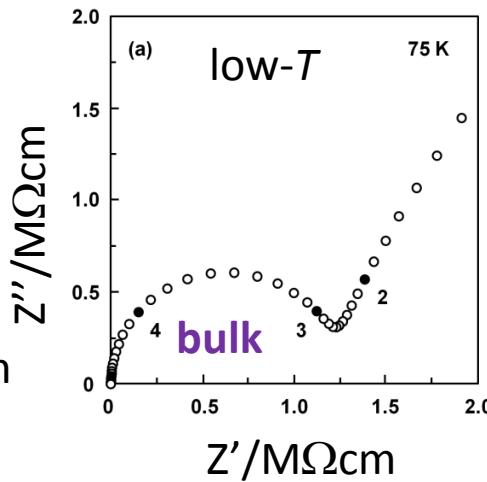
(Low- T) 10 - 100 K $E_a \sim 0$ eV

R_b (18 h) $\ll R_b$ (6 h)

Annealed ceramics at 200 °C (air, O₂, N₂, 5 % H₂/95 % N₂)

6 hr

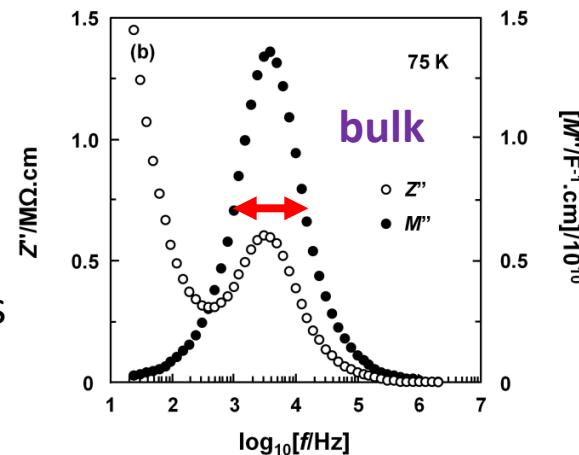
$$R_b \sim 1.2 \text{ M}\Omega\text{cm}$$



6 hr

$$\begin{aligned} M'' \text{ FWHM} \\ = 1.21 \text{ decades} \end{aligned}$$

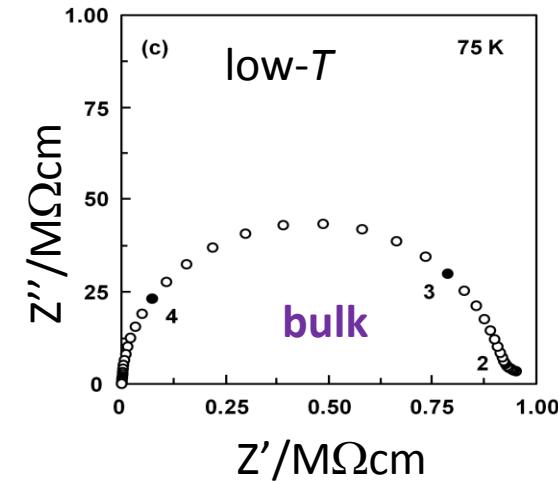
↔



R_b is resistive and grains are electrically homogeneous

18 hr

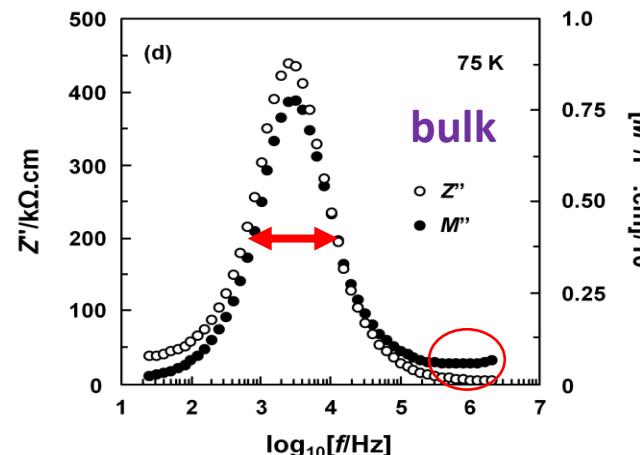
$$R_b \sim 0.8 \text{ M}\Omega\text{cm}$$



18 hr

$$\begin{aligned} M'' \text{ FWHM} \\ = 1.25 \text{ decades} \end{aligned}$$

↔

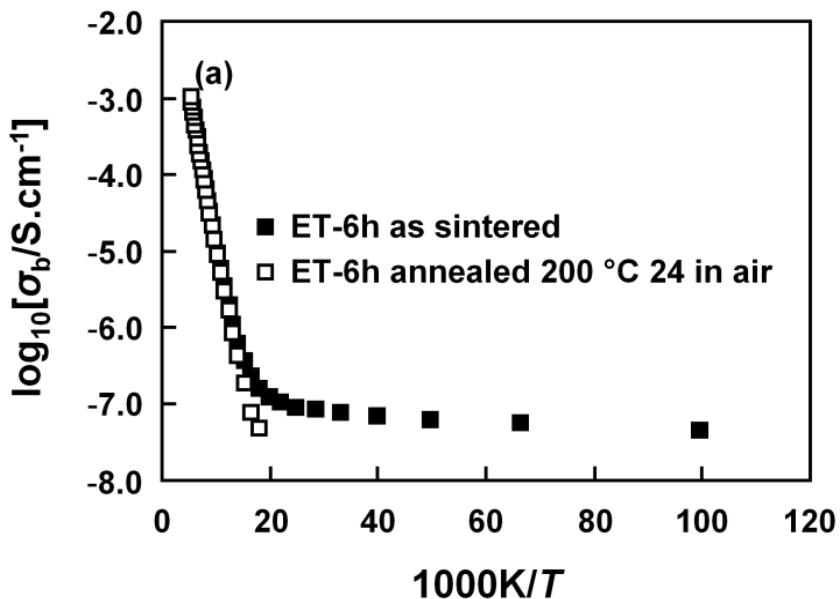


R_b is resistive but grains show evidence of electrical heterogeneity

Sintered v's Annealed Ceramics

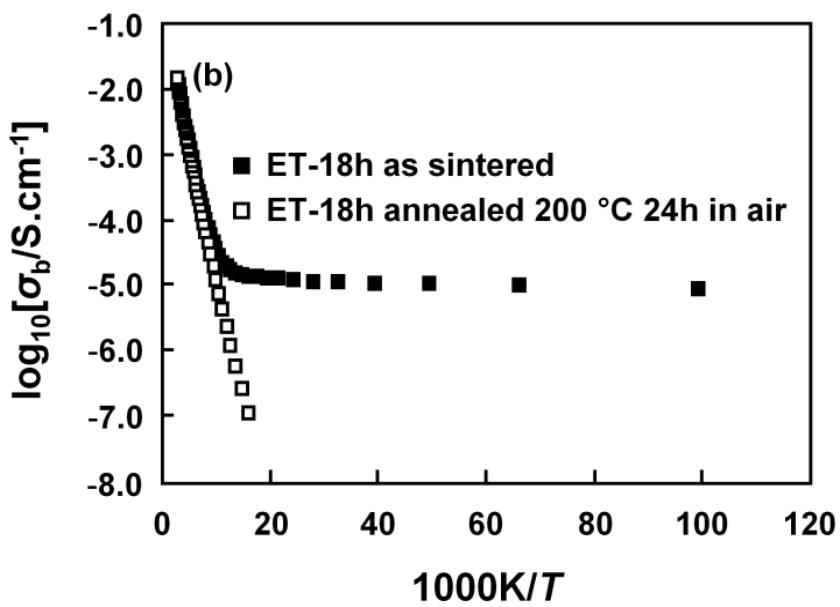
Bulk conductivity

6 hr

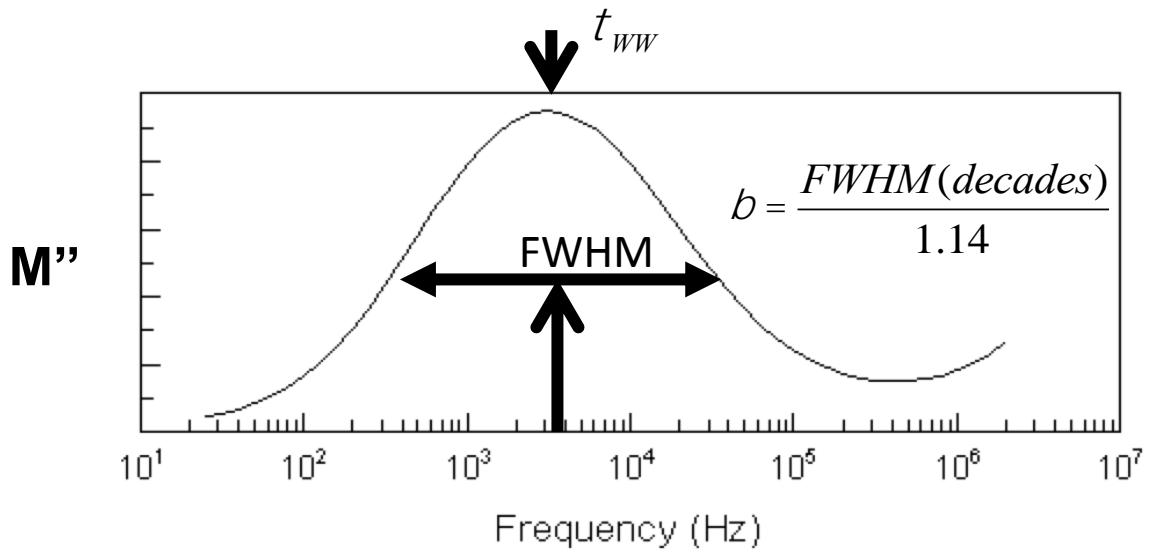


Annealing at 200 °C removes the low T conductive state for both samples.

18 hr



This annealing is ~ 100 °C below the decomposition temperature.



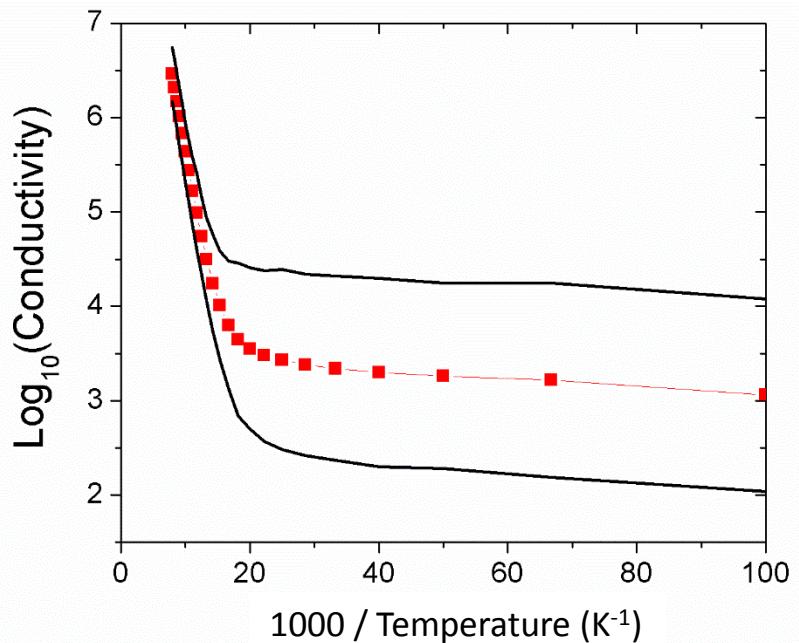
Non ideal behaviour

$$f(t) = \exp\left(-\frac{t}{t_{WW}}\right)^b = \frac{1}{n} \sum_{i=0}^n \exp\left(-\frac{t}{t_i}\right)^b$$

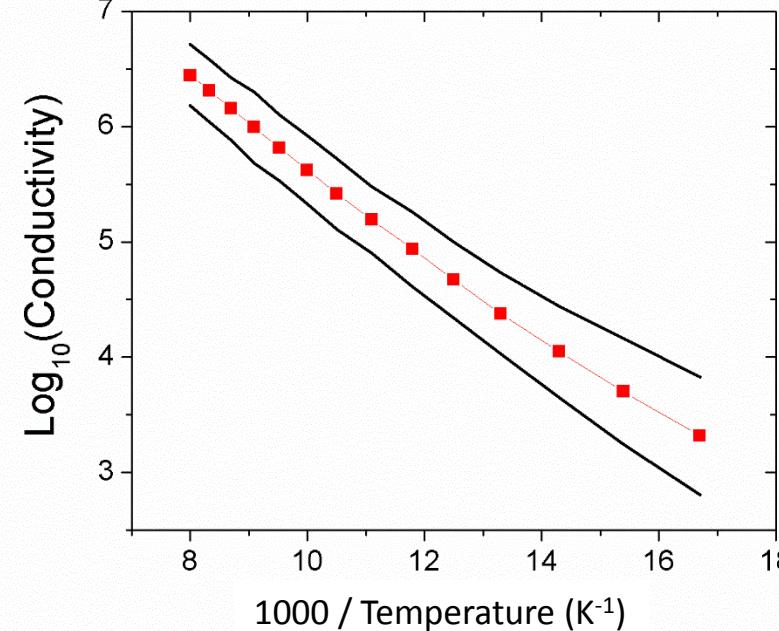
The non-exponential conductivity relaxation can be described by a Kohlrausch–Williams–Watts (KWW) function $\varphi(t)$, which represents the distribution of relaxation times

The peak gives the average τ and the FWHM over 1.14 decades gives beta

EuTiO_3 sintered at 1500 °C for 6h in 5 % H_2



EuTiO_3 sintered at 1500 °C for 6h in 5 % H_2 and annealed at 200 °C for 24h in Air

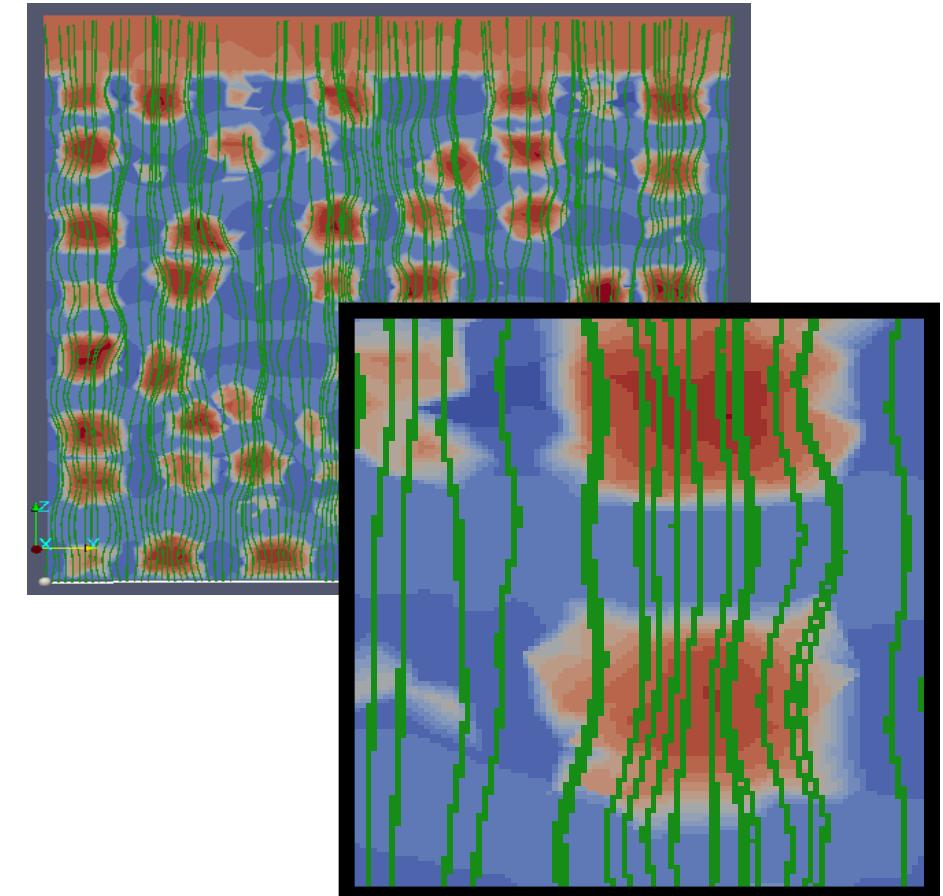
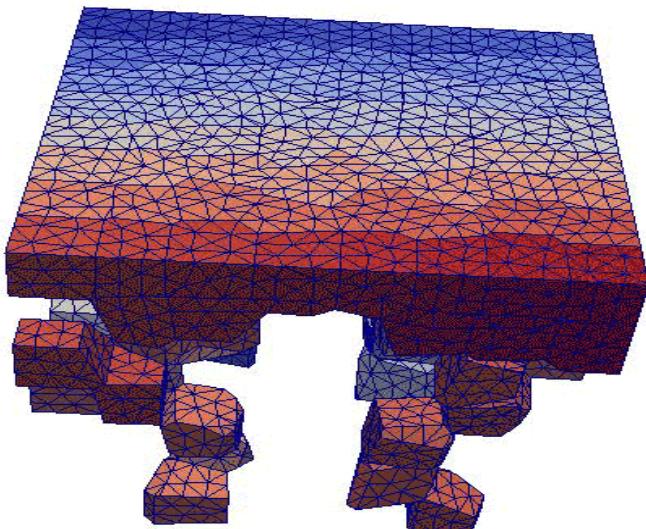


Finite Element modelling at Sheffield (Julian Dean)

The electrical microstructure lead to paths which are more favourable

Electrical response primarily made of these, with small contributions from parallel ones

In some cases (e.g. 10% change in resistance) only 50% of the grains make up the observed response!



Conclusions

- **La donor-doping in BaTiO_3 : A site doping with B-site vacancies (ionic compensation)**

The semiconductivity in La-doped air-fired samples and the ptc effect is linked to oxygen loss related to the presence of V_{Ti} .

- **La-doping in SrTiO_3 : A-site, B-site vacancies and electronic compensation are all possible.**
A-site vacancy samples have the highest σ of all samples processed in air and in 5 % H_2 and are excellent n-type thermoelectric oxides
- **EuTiO_3 : High levels of intra & inter grain heterogeneity can result in anomalous temperature independent σ at low T.**

There are some unusual low temperature conduction mechanisms in reduced perovskite-type titanates