



Setting the Standard for Automation

COLLATIVE CORRELATION OF FUNCTIONAL SAFETY LIFE CYCLE

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McDermott International Pvt. Ltd.

ISA-D: "Fertilizer , Food and Pharma Symposium-2019"

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ABOUT THE PRESENTER



Having 10 years of experience in field of Functional Safety involving System consulting, Engineering Software, Safety critical and High availability systems.

Involved in various stage of Functional Safety process and have executed Functional Safety projects in different regions.

Involved in upgradation of Failure data analysis associated with Product (Final Element accessories) based FMEDA certification.

Member of ISA committee.

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DEFINITIONS:



Reliability - Probability of a system to perform its intended functions satisfactorily, here by meeting the Design intent of System.

Risk – Combination of probability of occurrence of a Hazard and severity of the hazard, resulting in failure of system.

Safety Instrumented Function – Specific single set of actions and the corresponding equipment needed to identify a single hazard and act to bring the system to safe state.

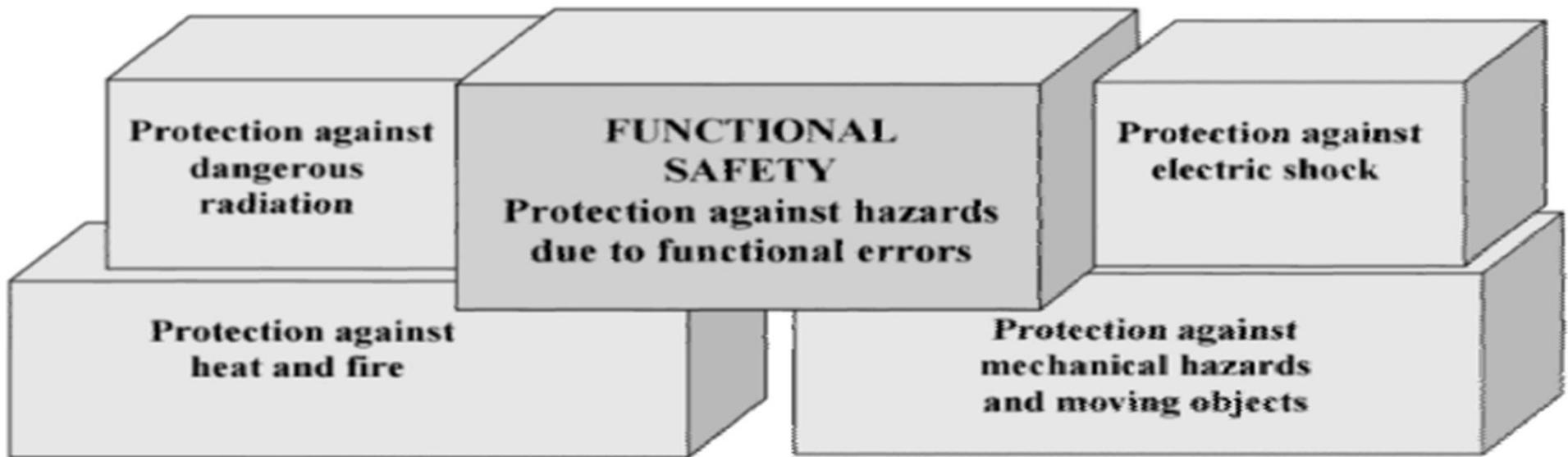
Safety Instrumented System – Instrumented Systems used to implement one or more Safety Instrumented Functions. A SIS is composed of any combination of Sensors, Logic solver, Final element (s).

Safety Integrity Level –Discrete level for specifying the probability of SIS satisfactorily performing SIF under all stated conditions and within stated time period.

FUNCTIONAL SAFETY:



Overall Safety is seen as part of overall safety

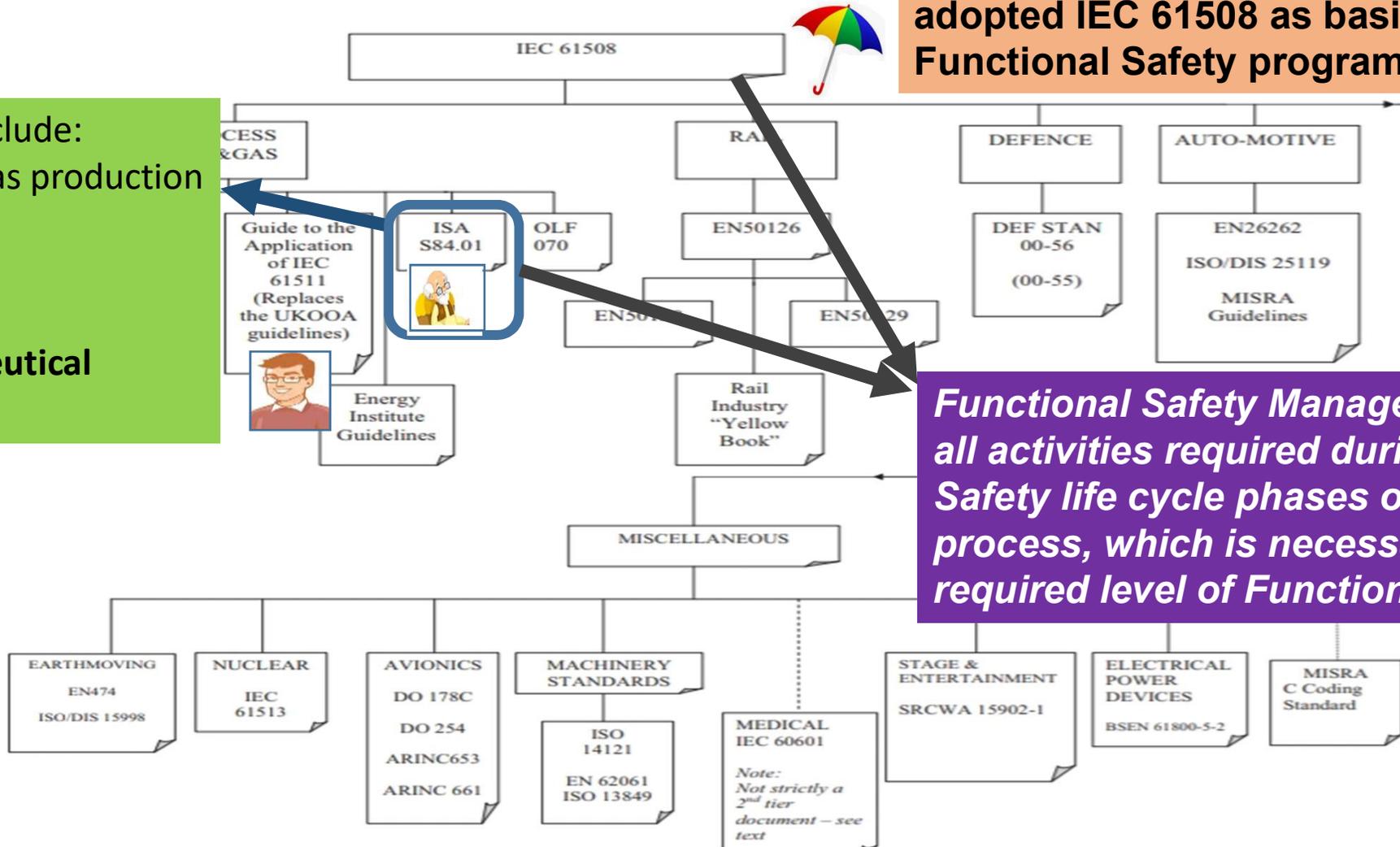


Purpose of Functional Safety – Automatic Safety function to perform the intended function correctly or the system will fail in a predictable (safe) manner.

STANDARDS:

Companies around the world adopted IEC 61508 as basis of Functional Safety programs.

include:
 Gas production
 Chemical
 Pharmaceutical

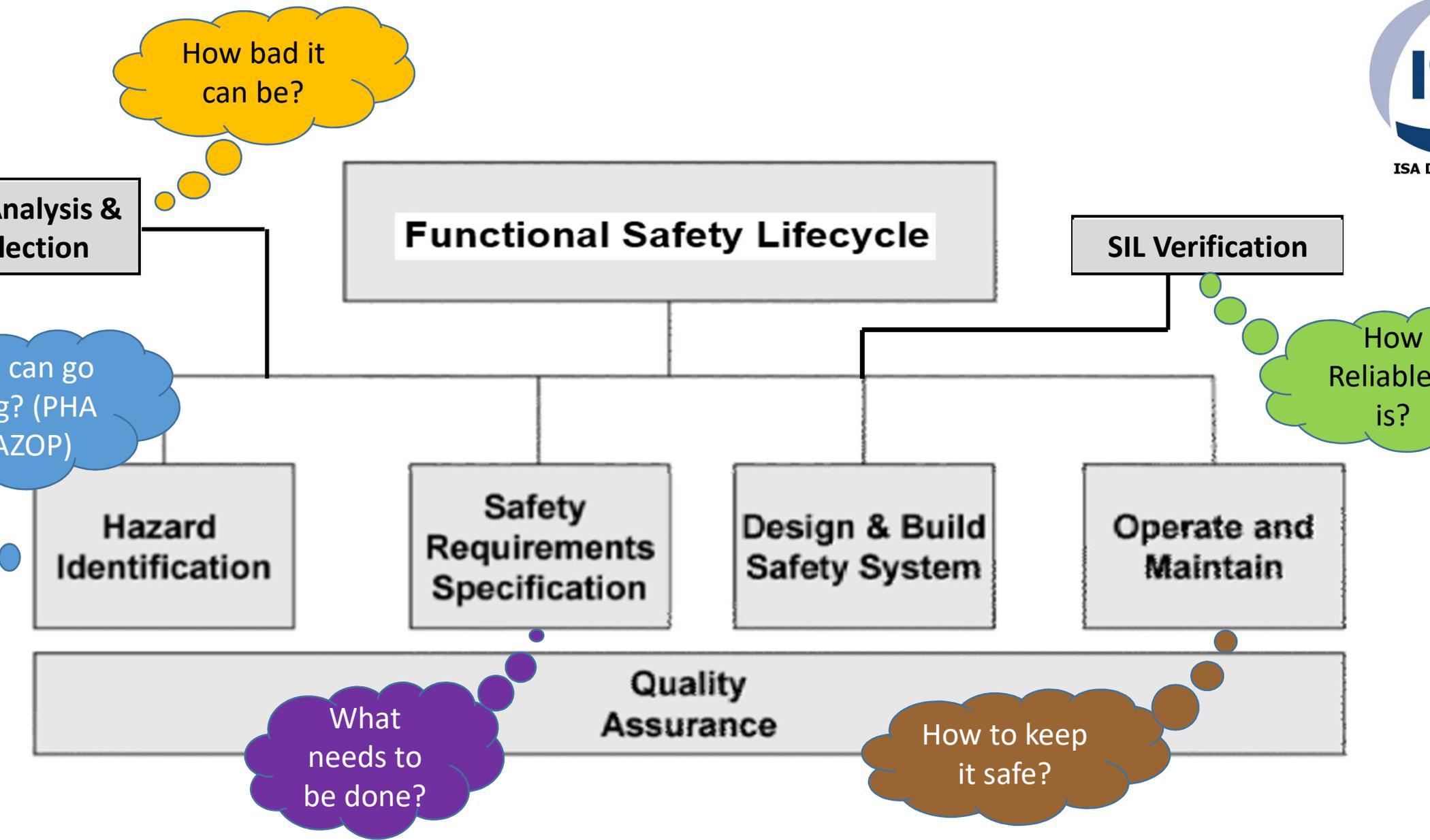


Functional Safety Management governs all activities required during Functional Safety life cycle phases of a product / process, which is necessary in achieving required level of Functional Safety.



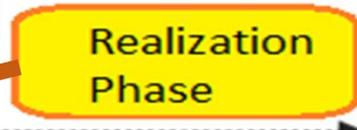
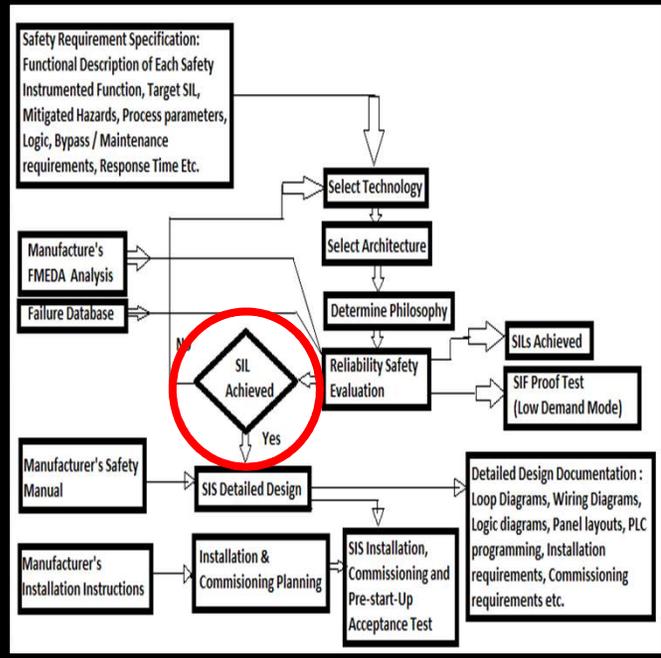


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Analysis Phase

1. Process Design – Scope Definition
 2. Identify Potential Hazards
 3. Consequence Analysis
 4. Identify Protection Layers
 5. Likelihood Analysis (LOPA)
- Decision: SIF Required?
- YES → 6. Select RRF, Target for each SIF
- NO → Tolerable Risk Guidelines
7. Develop Process Specification



* This paper focuses only on Analysis Phase and Realization phase.

In terms of SIL or RRF

SIL DETERMINATION METHODS



- ❖ Hazard Matrix
- ❖ Calibrated Risk Graph.
- ❖ Layer Of Protection Analysis (LOPA)
- ❖ Fault Tree Analysis
- ❖ Reliability Block diagrams.

SIL CLASSIFICATION TABLE

Safety Integrity Level	Risk Reduction Factor	PFD _{AVG} : Average
SIL 4	100,000 – 10,000	$>=10^{-4}$ to $<10^{-5}$
SIL 3	10,000 - 1,000	$>=10^{-3}$ to $<10^{-4}$
SIL 2	1,000 - 100	$>=10^{-2}$ to $<10^{-3}$
SIL 1	100 to 10	$>=10^{-1}$ to $<10^{-2}$



As per table, RRF / PFD avg is governing factor for SIL

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Layer Of Protection Analysis:



LOPA is a process to evaluate risk with explicit risk tolerance for specific consequences.

LOPA is a semi-quantitative method, which ranks somewhere between Risk Graph method and Markov Analysis.

LOPA method is solely dependent on values used for initiating event frequency and Independent Protection Layer (IPL).

LOPA is order-of-magnitude method, however this only reflects tolerance of error, not tolerance of uncertainty.

LOPA – METHODOLOGY



Identify initiating event (s) (IE) with potential to lead to defined Hazard scenario

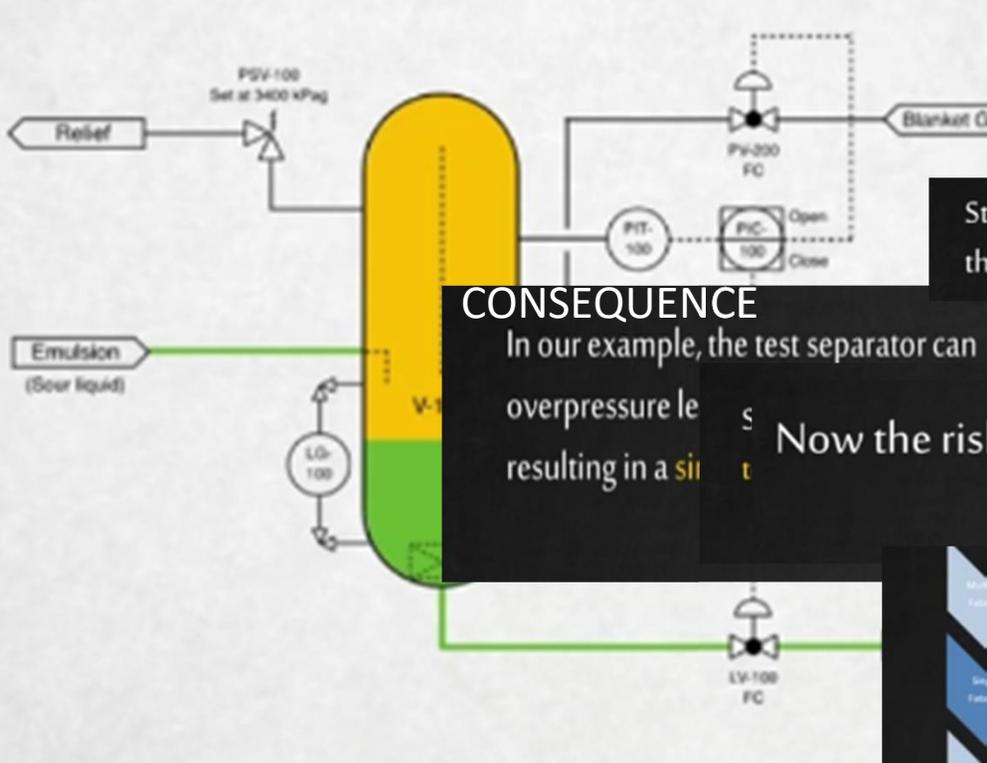
Identify Enabling conditions (EC), IPLs, Contributing conditions, and Initiating event.

Multiply each IE by probability risk reduction factors to determine scenario frequency.

Add the resulting individual scenario frequencies to determine total scenario frequency.



EXAMPLE LOPA WORKSHEET



CONSEQUENCE
 In our example, the test separator can overpressure leading to a safety valve failure resulting in a single fatality.

This safety instrumented function is SIL 2

- Probability of Failure on Demand of 0.01
- Risk Reduction Factor of 100
- Safety Integrity Level of 2

Now the risk is **acceptable**

frequency with the **new** safeguard

$$= 0.1 \text{ probability of valve failure per year} \\
 \times 0.1 \text{ probability of safety valve failure} \\
 \times 0.01 \text{ probability of the safety instrumented function failure} \\
 = 0.0001/\text{year or } 0.01\%/\text{year}$$

close

$$\text{New expected frequency of a single fatality} = 0.0001/\text{year} \\
 = \text{Tolerable frequency of a single fatality} = 0.0001/\text{year}$$

tently closed	leading to fatality.
---------------	----------------------



Protection
 ion factor
 re has a 0.1 probability of

must be independent
 and independent
 ed for this



re risk by a factor of

mand of the
 must be less

instrumented
 quirements of

TYPICAL FMEDA CERTIFICATE



The manufacturer may use the mark



Surveillance Audit Due October 31, 2022



ISO/IEC 17065 PRODUCT CERTIFICATION BODY #1004

Certificate / Certificat / Zertifikat / 合格証

MEW 1901146 C006

exida hereby confirms that the:

Diaphragm Actuator
Model 2800, 3800, 3300 and 2900
MOTOYAMA ENG. WORKS, LTD
Ohira, Miyagi, Japan

Have been assessed per the relevant requirements of:

IEC 61508 : 2010 Parts 1-7

and meets requirements providing a level of integrity to:

Systematic Capability: SC 3 (SIL 3 Capable)

Random Capability: Type A, Route 2_H Device

PFH/PFD_{avg} and Architecture Constraints must be verified for each application

Safety Function:

The Diaphragm Actuator will move to the designed safe position per the actuator design within the specified safety time.

Application Restrictions:

The unit must be properly designed into a Safety Instrumented Function per the Safety Manual requirements.



Kiyoshi Takai
 Evaluating Assessor
Kiyoshi Takai
 Certifying Assessor

Model 2800, 3800, 3300 and 2900
Diaphragm Actuator



50 N Main St
 Sellersville, PA 15950

Certificate / Certificat / Zertifikat / 合格証

MVG 1901146 C006

Systematic Capability: SC 3 (SIL 3 Capable)

Random Capability: Type A, Route 2_H Device

PFH/PFD_{avg} and Architecture Constraints must be verified for each application

Systematic Capability:

The product has met manufacturer design process requirements of Safety Integrity Level (SIL) 3. These are intended to achieve sufficient integrity against systematic errors of design by the manufacturer.

A Safety Instrumented Function (SIF) designed with this product must not be used at a SIL level higher than stated.

Random Capability:

The SIL limit imposed by the Architectural Constraints must be met for each element. This device meets exida criteria for Route 2_L.

IEC 61508 Failure Rates in FIT*

2800, 3800, 3300 Direct Acting

Device	ASD	ASU	ADD	ADU
Spring Return	0	506	0	121
Spring Return with PVST	501	5	86	35

2800, 3800, 3300 Reverse Acting

Device	ASD	ASU	ADD	ADU
Spring Return	0	578	0	147
Spring Return with PVST	572	6	104	43

2900 Diaphragm Actuator

Device	ASD	ASU	ADD	ADU
Spring Return	0	506	0	160
Spring Return with PVST	501	5	122	38

* FIT = 1 failure / 10⁹ hours

† PVST = Partial Valve Stroke Test of a final element Device

SIL Verification:

The Safety Integrity Level (SIL) of an entire Safety Instrumented Function (SIF) must be verified via a calculation of PFH/PFD_{avg} considering redundant architectures, proof test interval, proof test effectiveness, any automatic diagnostics, average repair time and the specific failure rates of all products included in the SIF. Each element must be checked to assure compliance with minimum hardware fault tolerance (HFT) requirements.

The following documents are a mandatory part of certification:

Assessment Report: MEW 1901146 R012 V1 R4 (or later)

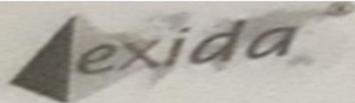
Safety Manual: MSE-B9002B (or later)

SIL Verification:

$$PFD_{SIF} = PFD_{PT} + PFD_{in} + PFD_{PLC} + PFD_{pw} + PFD_{out} + PFD_{sol} + PFD_{act} + PFD_{valve}$$

Element	PFD
Pressure transmitter	0.010518
PLC – input	0.004388
PLC – main processor	0.000051
PLC – power supply	0.000002
PLC – output	0.002194
Solenoid	0.010254
Actuator	0.005995
Valve	0.046975

$$PFD_{SIF} = 0.080376$$



1.3.2 Safety Requirements Specification

The key objective of writing the safety requirements specification is to make sure that the specification is complete and understandable. The safety requirements specification will be the primary input for the conceptual design of the Safety Instrumented Functions. If the specification is not complete the Safety Instrumented Functions may not be designed correctly and the achieved safety integrity may not be enough (under design) or too much (over design).

The IEC 61511 standard provides a clear list of issues to be addressed in the safety requirements specification. The use of a template or templates is highly suggested to assure completeness and for consistency purposes.

1.3.3 SIL Verification

The objective of calculating the Achieved Safety Integrity Level is to determine the amount of risk reduction a Safety Instrumented Function, in its conceptual design, provides. If the achieved Safety Integrity Level meets or exceeds the Target Safety Integrity Level the conceptual design can be passed on to the detail design phase where the Safety Instrumented Functions are implemented.

The functional safety standards reference various methods that can be used to perform the reliability analyses from which the Achieved SIL is obtained. The most popular reliability analysis techniques listed in an increasing order of accuracy are:

- Simplified equations
- Fault tree analysis
- Markov modeling

There have been many debates and publications [8], [9] on what technique should be used for the reliability analysis with regard to Safety Instrumented Functions especially since different techniques may yield different results. Detailed analysis has shown, however, that the different techniques are based on different assumptions, consequently leading to different results [10]. Therefore, the user of any of these techniques should be aware of the assumptions inherent to the technique.

Another key issue in the reliability calculations is the reliability data to be used in the SIL verification [11], [12]. Especially when comparing results from different calculations it is key that the data source used in the calculations is identical. Data sources may vary by orders of magnitude with respect to equipment failure rate data.

1.4 Market Drivers

The release and adoption of new functional safety standards provide a means for manufacturers of equipment to qualify them for safety applications. These provide a framework for both equipment vendors and end users to justify the use of standards for safety. Many operating companies have also found that adopting a lifecycle approach as recommended by these functional safety standards has had the effect of reducing both capital and operational expenditure [13].

IMPACTS :



...n SIL level i.e. between Target and
...sibility of excluding Higher order
...nce between A...

I did HAZOP & LOPA, but still
possibility of EXPLOSION exists?

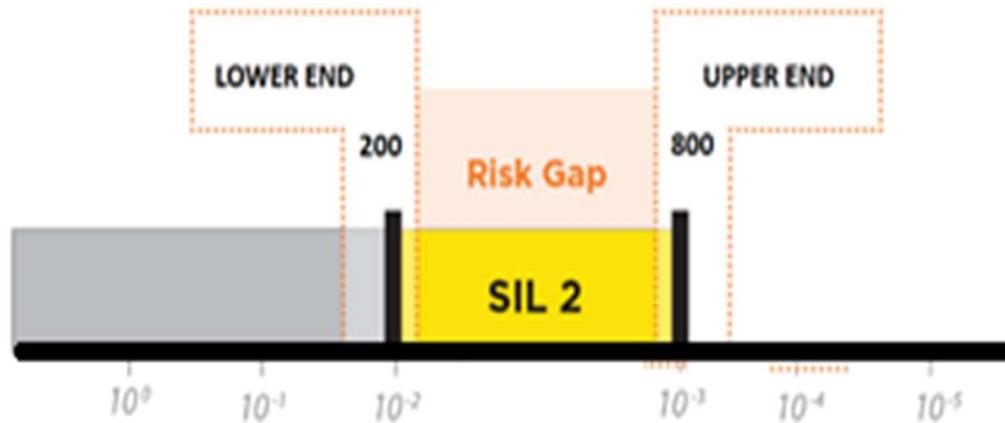


la
e
olerable

Design of SIF shall suffer because of existing uncertainties
(mainly RRF) of SIL assessment process.

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RECOMMENDATION:



SIL Level	RRF		PFDavg	
	Lower End	Upper End	Lower End	Upper End
SIL 1	NA			
SIL 2	200	800	5.00E-03	1.25E-03
SIL 3	2000	8000	5.00E-04	1.25E-04

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REASON FOR CONSIDERING TOLERANCE IN LOWER END OR UPPER END



type of technique employed in SIL determination and SIL verification.

tolerance of error in LOPA due to Initiating event frequency estimates, Risk reduction for each Protection layers, enabling conditions and conditional modifiers and true independence of each or those values from all of other members. Approximate % of error tolerance limits estimated is around +/- 30%

data that are been collected for calculating Risk Tolerability criteria for plant level data and FMEDA analysis, proven-in-use method for Product based certification.

CONCLUSION



If No Explosion has been occurred in a Plant, doesn't means Plant is Safe & "Reliable". Even though occurrence of such incidents may be rare, but it should not occur. Always it is better to safeguard a plant from future awaited catastrophic events, if higher level of functional safety has been followed.

Thank You!

Any Questions?



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