Mitigation Techniques for Capacitor Bank Switching Transients

Rahul Deshmukh¹, Prof. V.R. Aranke²

¹ PG Student, ²Assistant Professor

¹²MCOE&RC, Nashik

¹²Savitribai Phule Pune University, Pune, Maharashtra, India

Abstract- The quality of electric power has been a constant topic of study, mainly because inherent problems to it can bring great economic losses in industrial processes. Among the factors that affect power quality, those related to transients originated from capacitor bank switching in the primary distribution systems must be highlighted. In this thesis, the characteristics of the transients resulting from the switching of capacitor banks are analysed, as well as factors that influence there intensities. It presents a new application of the singled reactor-type fault current limiter to suppress the three-phase low-voltage capacitor switching transients. During the capacitor switching DC reactor provides the high impedance and at the steady state limiter free-wheels. The limiter will not cause a voltage rise at the capacitor's terminals or a distortion of the capacitor's current waveform in the steady state.

Keywords- Power quality, Transients, Capacitor bank, Singled reactor type fault current limiter.

I. INTRODUCTION

Shunt capacitors are widely used in power systems to improve the voltage profile in reducing existing voltage variations or those occurring from time to time. They provide the reactive power close to where the lagging loads are connected and, in turn, help reduce network losses. Normally, they are not connected to the network all of the time and are switched on and off several times during the course of a typical day. This switching, if not specially controlled, isoften by overvoltage transients that compromise the supply quality. This issue is becoming more important due to theincreasing use of sensitive electronic loads that are easilydisrupted or even damaged bysuch over-voltages[1].

Various approaches have been presented for restraining capacitor switching transients, such as the use of a series current limiting reactor, a switch pre-insertion resistor/inductor, and zero-voltage closing control. These approaches may cause problems with series resonance, voltage rises at the capacitor's terminals during the steady state, need for an additional control circuit, and complexity of the setup and control strategy [2].

In the recently developed approaches [3], a DC-reactor has been utilized to mitigate the capacitor switching transients. In [3-4], single-phase DC-reactor type capacitor transient limiters are studied. These single-phase devices must be separately installed in different phases, which in turn lead to increase in the number of the electric components and lower reliability of the system. Besides, when a single-device failure occurs, the

voltage imbalance across the capacitor bank terminals has negative impacts on the operation of the system. A three-phase single-DC reactor-type limiter is proposed in [2]. In this method, a DC-reactor provides high-impedance through a three-phase coupling transformer at the energizing instants, through which the transients are suppressed.

II. LITERATURE SURVEY

A paper on Identification of Capacitor Switching Transients with Consideration of Uncertain System and Component Parameters by H. Y. Zhu and S. Chen, mentioned that capacitor switching transient is one of the most commonly encountered power quality disturbances. Measuring and identifying these transients remains a challenge as the characteristics depend on the system parameters, capacitor ratings and makeup of the connected loads. This paper describes a systematic approach to design an automated system for identifying such transients. It relies on the belief that some of the system and component parameters are either known or can be determined, and thus can be used to develop the necessary pattern for identification and discrimination. However, identification also needs to be robust against uncertainties in these parameters. The proposed method combines the techniques of wavelet transform, rank correlation and fuzzy logic to account for the uncertainties. Dynamic simulations were undertaken to verify the method and to illustrate its robustness when dealing with various uncertain transient characteristics. It is shown to be capable of identifying transients caused by switching of both isolated and back-to-back capacitors.

Analysis and Control of Large-Shunt-Capacitor-Bank Switching Transients by J C Das, it is mentioned in this paper, the Large capacitor banks at medium-voltage levels are finding applications and greater acceptability in industrial distribution systems. However, these can give rise to current and voltage transients, stress the switching devices and insulation systems, and can be detrimental to the sensitive loads, i.e., drive systems. The paper discusses the methodology of the analysis and control of the switching transients.

Transient studies for an industrial distribution system are not normally performed, and when needed, capacitor switching accounts for most of these investigations consequent to the failure of equipment or the shutdown of a process. Even in these study cases, analysis can be indirect, without rigorous calculations or computer modeling. The switching transients originate from:

- a) switching of a shunt-capacitor bank, which may include switching on to a fault
- b) back-to-back switching, i.e., switching of a second capacitor bank on the same bus in the presence of an already energized bank
- c) Tripping or de energizing a bank under normal operation and under fault conditions
- d) possible secondary resonance when the capacitors are applied at multi-voltage level(i.e., at the 13.8-kV level as well as at the 480-V level) in a distribution system; and
- e) Restrikes and prestrike in the switching devices

Shunt Capacitor Bank Switching Solutions for Transient Mitigation - Design Approach and EMTP Simulations by Jayanth R. Ramamurthy and Doug Mader, this paper presents an overview of switching transients commonly encountered with single and multiple shunt capacitor bank installations and describes the evaluation of transient concerns for single and multiple shunt capacitor bank switching, followed by a step-by-step procedure for application of transient mitigation measures. Mitigation of shunt capacitor bank switching transients is an important consideration at HV/EHV level. The step by step design approach described in this paper can help in streamlining the process of choosing an appropriate solution for mitigation of capacitor bank switching transients and can easily be integrated during planning and design stage.

III. PROBLEM DESCRIPTION

A. Problem definition

For the switching of capacitor several conventional methods are being used. Fixedreactor or pre inserted reactors are creating the resonance problem. Capacitor voltagelevels are also needs to increase due to series reactor. Hence the DC series reactor isproposed to avoid the above mentioned issues. DC reactor provides the high impedancethrough a three phase coupling transformer during energizing instants. However during the steady state operation, DC reactor charges and discharges continuously. This creates the continuous steady-state power loss. Apart from this the cost of DC reactor type limiter is high for high power applications and medium for low voltageapplications. So it is required to bypass the reactor after steady state operation. And send out the better solution to reduce the cost at high power applications.

B. Methodology

In this paper, discussion of the transient mitigation methods, full time inductor, pre-insertion inductor, zero-crossing breaker and pre-insertion resistor to mitigate current transients is presented. And the devices with resistance provide the added advantage of reducing voltage transients. Proper selection of the resistance value can significantly reduce voltage transients. Zero-crossing switching shows good transient mitigation but transients will increase if timing calibration drifts.

Capacitor energizing transient limiter for mitigating capacitor switch-on transients by Tseng, S.-T., Chen, J.-F, This study proposes a rectifier type capacitor energizing transient limiter (CETL) for mitigating the isolated capacitor and back-to-back

ISSN: 2393-9028 (PRINT) | ISSN: 2348-2281 (ONLINE)

capacitor switch-on transients. The operating condition of the proposed circuit can be divided into two states: the charging suppressive mode and the steady state with its initial transient. During the charging suppressive mode, a pair of diode strings conducts automatically and then the DC reactor provides high impedance at the instant of switching on in order to suppress the capacitor energizing transients. During the steady state with its initial transient, all diodes of the bridge rectifier conduct simultaneously and the limiter freewheels; therefore the limiter acts as a short circuit and has no effect. Thus, it is not necessary to increase the capacitor-rated voltage when the CETL is used. In this study, experiments and simulations are carried out to demonstrate the feasibility of the proposed limiter circuit.

Single-DC Reactor-Type Transient Limiter for Reducing Three-Phase Power Capacitor Switching Transients by Hsu-Ting Tseng and JiannFuh Chen, This paper presents a new application of the singled reactor-type fault current limiter to suppress the three-phase low-voltage capacitor switching transients. The proposed limiter is composed of a three-phase coupling transformer, a three-phase bridge rectifier, a dc reactor, and a dc-bias voltage source. The dc reactor is connected in the three-phase coupling transformer's secondary winding and can automatically provide high impedance at the instant of energization, thus restraining the energizing transients of the three-phase capacitor. In the steady state, the bias voltage causes all rectifier diodes to conduct simultaneously, and the limiter freewheels. Therefore, the voltage across the coupling transformer's secondary side is nearly zero, and the transformer's primary side acts as a short circuit.

The limiter will not result in a voltage rise at the capacitor's terminals or a distortion of the capacitor's current waveform in the steady state. Due to the freewheeling effect in the limiter, no transient over voltage appears across the switching device at the instant of de-energization. Analytical equations to describe the performance of the system have been developed. Finally, a 2.7-kVAR three-phase capacitor is used for demonstration, and simulation and experimental results are carried out to verify the feasibility of the proposed limiter.

C. Capacitor Switching Transients

The simple per-phase system of Figure. 4.1 is used to provide a conceptual introduction to some of the common transients involved in capacitor bank switching. R1 and L1represent the system source impedance. CB4 feeds two capacitor banks, represented byC1 and C2. S1 and S2 represent the circuit breakers used to switch the capacitor banks.LB is the inductance of the bus spanning between the capacitor banks. R2 and L2 are thetotal impedance of the feeder and distribution transformer. A distribution-level capacitorbank is attached to the transformer secondary.CB3 can be used to initiate and interrupta ground fault on the bus at some distance down the feeder, depending on location of theground. Using different portions of this system, five transients can be addressed:

IJRECE Vol. 6 ISSUE 4 (OCTOBER- DECEMBER 2018)

- Energization inrush
- 2. Back-to-back energization
- 3. Outrush into a nearby fault
- Voltage magnification, and 4.
- Transient recovery voltage (TRV).

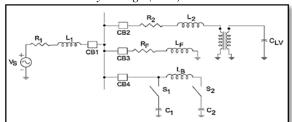


Fig.1: Illustration of capacitor bank transients by per phase system

Novel Technique for Mitigation of Capacitor Switching Transient using Capacitor energizing transient limiter (CETL)

The mitigation methods we have seen above are mainly works on the below basic principles, [4]Either they increase the line impedance at the instant of switching on, orthey close the switch when the magnitude of the voltage across the switch is zeroIn case of increased line Impedance, there is a possibility of system resonance, which may damage the capacitor bank. And adding a reactor in series required the higher voltagerating of capacitor. In second approach of voltage zero switching need to have an additional control circuit, which will increase the cost and complexity and reduce reliability. Hence, this it proposes a rectifier type capacitor energizing transient limiter (CETL)so as to suppress the energizing transients without adding impedance during the steady state. The configuration of the proposed limiter has been widely used as a fault current limiter to suppress the power system fault current when a fault occurs in the powertransmission network [4] and has also seen use as an inrush current limiter to restrain the transformer inrush current [4].

a. Circuit operation

As for mitigating the energizing transients to avoid damage to the three-phase capacitor, the proposed CETL is inserted into each phase to suppress the inrush current and transient over voltage, as shown in Figure 6.1. A CETL is mainly composed of a DC reactor, which is made from a silicon steel iron core inductor, a bridge rectifier and a DC-biasvoltage source.

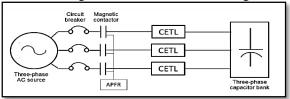


Fig.2: Installation of a CETL in three phase system

b. Single-DC Reactor-Type Transient Limiter

A three-dc reactor-type transient limiter has been proposed [4], but this limiter needs tobe installed in each phase of the three-phase power system for suppressing the three-

ISSN: 2393-9028 (PRINT) | ISSN: 2348-2281 (ONLINE)

phasecapacitor switching transients. Altogether, it is comprised of three dc reactors, 12 diodes for rectification, and three sets of dc-bias voltage sources. Moreover, the insulation levelsand current ratings for the rectifier diodes and dc reactors must depend on the voltagelevel of the distribution power system, and this level cannot be adjusted arbitrarily; thus, this approach lacks flexibility. Single DC rector type transient limiter has been proposed in [2] to make the circuit more simple and reliable. This thesis is focused on this recently develop approach.

Circuit configuration

The circuit configuration of the proposed single-dc reactor type transient limiter is shown in Figure 3 It is composed of a dc reactor, a three-phase bridge rectifier, a dc-bias voltagesource, and a three-phase coupling transformer. The three-phase coupling transformer is inserted in series between the voltage source and the capacitor bank, and its main function is to react the impedance of the dc reactor into the primary circuit at the instantof energization. DC reactor is connected at the dc output terminal of the three-phase rectifier, and is connected in series with a bias voltage source, supplied by a single-phase

or three-phase full wave rectifying voltage from a step-down potential transformer or aswitching-mode power supply. For reducing the power loss before switching on, the bias voltage source is synchronously supplied at the instant of energization.

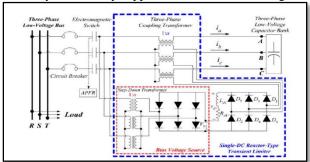


Fig.3: Circuit configuration of single-dc reactor-type transient

d. Operation principles

The proposed single-dc reactor-type transient limiter can be simplified as a single-phase circuit, as shown in Figure 4, to illustrate the operation principles.

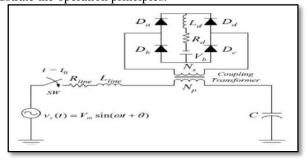


Fig.4: Circuit diagram of the Single-DC reactor-type transient limiter

IJRECE Vol. 6 ISSUE 4 (OCTOBER- DECEMBER 2018)

According to the charging and discharging behaviour of the dc reactor, its operation is done in the simulation model in two mode viz. Limiting mode and freewheeling mode.

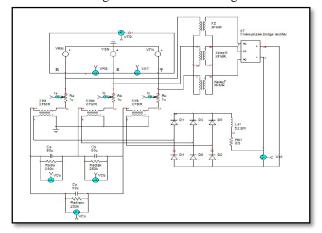
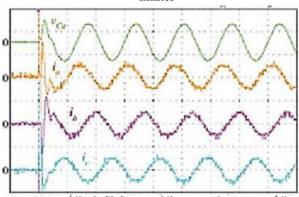


Fig.5: ICAP/4 simulation for DC reactor type transient limiter



Vca: 400V/div, ia/ib/ic: 20A/div Time: 10ms/div Fig.6: Simulated Output waveform without limiter

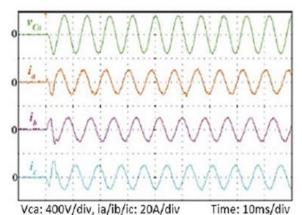


Fig.7: Simulation Output waveform with DC reactor type limiter

IV. RESULTS AND DISCUSSION

As shown in Figure 6 and 7, it is clearly observed that if we switch on the capacitor without any type of limiter, it will generate the transients which are five times higher than the rated current of capacitor.But, if we implement the DC reactor

ISSN: 2393-9028 (PRINT) | ISSN: 2348-2281 (ONLINE)

for switching of the capacitor, there is almost no distortionin the line current waveforms. Qualitative Comparison of the approaches for reducing capacitor switching transients is given below.

Table I: Qualitative Comparison of the approaches for reducing capacitor switching transients

Approach	Cost	Performance
		Advantages
	Moderate	1. The effect of suppression
	CONC. 000-1967-01	is appreciable and viable.
Three-DC	(for Low-Voltage	2.Ready to restrain the
Reactor -	Control of the Contro	energizing transients at
Type		any time without any control
Transient	Applications)	3.No voltage rise at
Limiter [2]		the capacitor's terminal in the steady state
		4.No appearance of the de-energizing transients.
		5.Suitable for both High- and Low voltage system
		Disadvantages
		1. The ratings of bridge rectifier, dc-bias
	High	voltage source and de reactor must
	rugu	depend on the system voltage level.
	(for High-Voltage	2.Continuous steady state power loss in the limiter
	Applications)	2. Continuous steady state power loss in the limiter
	Applications)	4.1 .
e. 1	Moderate	Advantages
	Moderate	The effect of suppression is appreciable and viable.
	# T W	2.Ready to restrain the energizing
Single	(for Low-Voltage	transients at any time without any control
DC Reactor	Applications)	3.No voltage rise at the capacitor's terminal in the steady state
Transient	***	4. No appearance of the de-energizing transients.
Limiter [2]	High	5.Suitable for both High- and Low voltage system
	(for High-Voltage	6.The ratings of bridge rectifier,
	Ten Chennis et al.	de-bias voltage source and de reactor can
	Applications)	be changed by adjusting the turns
		ratio of the 3-PH coupling transformer
		Disadvantages
		1. Continuous steady state power loss in the limiter
	sasserous resease	Advantages
	Moderate	 The effect of suppression is appreciable and viable.
	(for Low-Voltage	2.Ready to restrain the energizing transients
	29/20/20/20/20/20/20/20/20/20/20/20/20/20/	at any time without any control
	Applications)	3.No voltage rise at the capacitor's terminal in the steady state
		4. No appearance of the de-energizing transients.
		5.Suitable for both High- and Low voltage system
		Disadvantages
		1. Complicated control method.
Zero	High	2. Need the precise detection.
Voltage	(for High-Voltage	3. PIV concern of power electronics-based switching devices,
closing	Applications)	e.g. SCRs, for high-voltage applications.
control [3]		4. For high-voltage applications each pole of the
		circuit breaker must be independently controlled.

V. CONCLUSION

Application of Single DC reactor for mitigation of the threephase capacitor inrushcurrent and transient overvoltage is presented in this thesis. The proposed limiter hasno need for any additional control circuit and the circuit topology is simple. Therefore, it can reduce complexity and increase reliability. A point that is especially to be noted s that fewer components are required for the proposed single-dc reactortype transientlimiter as compared with the three-dc reactor type. Since the transient limiter provideshigh impedance during the transient period, the energizing transients can be effectively suppressed. During the steady-state period, the limiter freewheels without adding anyimpedance between the voltage source and the capacitor. Thus, the terminal voltage ofthe capacitor will not rise, and thus, it is not necessary to increase the capacitor's voltagerating. The installation of the limiter almost will not result in voltage and currentdistortions in the capacitor or system series resonance. According to simulated results, ithas been proved that the proposed singledc reactor-type transient limiter is effective forsuppressing the three-phase capacitor switching transients and will not affect the steady-state performance of the capacitor.

IJRECE Vol. 6 ISSUE 4 (OCTOBER- DECEMBER 2018)

REFERENCES

- [1]. H. Y. Zhu and S. Chen, "Identi_cation of Capacitor Switching Transients with Consideration of Uncertain System and Component Parameters", IEEE trans. Power del., vol. 23, no. 1, Jan. 2008
- [2]. Hsu-Ting Tseng and Jiann-Fuh Chen, "Single-DC Reactor-Type Transient Limiterfor Reducing Three-Phase Power Capacitor Switching Transients", IEEE trans. Powerelectronics., vol. 27, no. 4, April 2012
- [3]. Ghanbari, T., Farjah, E., Zandnia, A.: "Solid-state transient limiter for capacitorbank switching transients", IET Gener. Transm. Distrib., 2013, 7, (11), pp. 1272-1277
- [4]. Tseng, S.-T., Chen, J.-F.: 'Capacitor energizing transient limiter for mitigatingcapacitor switch-on transients', IET Elec. Power Appl., 2011, 1, (3), pp. 260-266
- [5]. Jayanth R. Ramamurthy, Doug Mader, Sharma Kolluri, "Shunt Capacitor BankSwitching Solutions for Transient Mitigation -Design Approach and EMTP Simulations IEEE 2016
- [6]. G Pardhasaradhi, P.S.Raju, "Real and Reactive Power Control of Electrical Distribution Network with SMES and Capacitor" 2014 International Conference on Circuit, Power and Computing Technologies [ICCPCT]

ISSN: 2393-9028 (PRINT) | ISSN: 2348-2281 (ONLINE)

- [7]. Bhargava, B., Khan, A.H., Imece, A.F., et al.: 'Effectiveness of pre-insertion inductors for mitigating remote overvoltages due to shunt capacitor energizing', IEEE Trans. Power Deliv., 1993, 8, (3), pp. 1226-1238
- [8]. IEEE Guide for the Application of Capacitance Current Switching for AC High-Voltage Circuit Breakers Above 1000 V
- [9]. J. C. Das "Analysis and Control of Large-Shunt-Capacitor-Bank Switching Transients" IEEE Transaction on Industrial application, Vol. 41, no. 6, Nov 2005
- [10]. Michael Beanland "Pre insertion Resistors in High Voltage Capacitor Switching", WPRC 2004