## ASME Y14.5M-1994 GD&T Certification Preparation Examination

## Directions: On the response sheet on the last page, fill in the circle of the letter which best completes the following statements. Do not write on any pages other than the response sheet.

- 1. \_ is the term applied to a cylinder, or two opposed surfaces or points associated with a size dimension.
  - Feature a.
  - b. Feature of size
  - Actual size c.
  - d. Size dimension
- 2. describe theoretically perfect sizes, profiles, orientations, or locations.
  - Features of size a.
  - True positions b.
  - Nominal sizes c.
  - **Basic dimensions** d.
- 3. A feature of size is said to be at \_\_\_\_\_\_ when it contains the maximum amount of material within stated limits. virtual condition
  - a.
  - b. maximum material condition
  - c. maximum tolerance
  - d. least material condition
  - A feature of size is said to be at \_\_\_\_\_\_ when it contains the minimum amount of material within stated limits.
    - virtual condition a.
    - maximum material condition b.
    - minimum limit c.
    - least material condition d.
- mm is the MMC limit of a hole of  $\emptyset$  15.0 ± 0.5. 5.
  - 14.5 a.

4.

- 15.25 b.
- 15.5 c.
- d. 16
- Gaging tolerances should add \_\_\_\_\_\_ to the gaging feature. 6.
  - size a.
  - b. bonus tolerance
  - c. material
  - d. importance
- 7. In general, the \_\_\_\_\_ modifier is used on tolerances for clearance fits, and \_\_\_\_\_ is used for press fits or centering.
  - LMC/MMC a.
  - b. **RFS/MMC**
  - LMC/RFS c.
  - d. MMC/RFS
- is implied for all geometric tolerances and datum references unless another 8. Under the 1994 standard \_\_\_\_ material condition is specified.
  - MMC a.
  - RFS b.
  - LMC c.
  - projected condition d.

- 9. Theoretically perfect planes, surfaces, points, lines, or axes from which measurements are made are referred to as
  - a. basic dimensions
  - b. datum features
  - c. datums
  - d. simulated datums
- 10. A datum reference frame can be established by \_\_\_\_\_.
  - a. three mutually perpendicular planes
  - b. a plane and a perpendicular axis
  - c. one or more degrees of freedom
  - d. a. or b.
- 11. When a geometric tolerance or datum reference applies at all actual sizes within size limits, the term \_\_\_\_\_\_ is used.
  - a. regardless of feature size
  - b. limits of size
  - c. virtual condition
  - d. geometric tolerance

12. According to Rule #1, when form tolerances are in question \_\_\_\_\_\_ is required for features of size at MMC.

- a. true form
- b. perfect form
- c. geometric form
- d. true position
- 13. What is the straightness tolerance available for a  $\emptyset$  .730 shaft with a specified size dimension of  $\emptyset$  .725 ± .005?
  - a. 0
  - b. .001
  - c. .005
  - d. .010

14. \_\_\_\_\_ controls the form and/or orientation of straight lines, multiple planar surfaces, arcs, and irregular surfaces.

- b. Orientation
- c. Straightness
- d. Profile

15. Datum shift is permitted when a datum is referenced at \_\_\_\_\_\_ and should be simulated at its \_\_\_\_\_\_.

- a. LMC; least material condition
- b. MMC; virtual condition
- c. RFS; actual mating size
- d. virtual condition; MMC
- 16. A flatness tolerance zone is formed by \_\_\_\_\_.
  - a. two parallel lines
  - b. two equidistant planar datums
  - c. two parallel planes
  - d. two parallel planes parallel with a common datum
- 17. A position tolerance zone can be formed by \_\_\_\_\_\_ related to one or more datums.
  - a. two concentric cylinders
  - b. a cylinder
  - c. two parallel planes
  - d. b. or c.

- 18. When a geometric tolerance is applied on an MMC basis, the worst case effects of the LMC feature size and geometric tolerance create what is known as a \_\_\_\_\_\_.
  - a. virtual condition
  - b. geometric boundary
  - c. nominal limit
  - d. resultant condition
- 19. A complete datum reference frame \_\_\_\_
  - a. controls three degrees of freedom
  - b. is created by three features
  - c. controls six degrees of freedom
  - d. is created by datums A, B, and C
- 20. For an internal feature of size, virtual condition (MMC basis) is calculated using the following formula:
  - a. MMC LMC
  - b. MMC geometric tolerance
  - c. MMC + bonus tolerance
  - d. a. and b.

21. \_\_\_\_\_ is usually indicated when there is a need to preserve wall thickness.

- a. MMC
- b. LMC
- c. RFS
- d. Virtual condition

22. Basic angles must be shown on the print for \_\_\_\_\_ but are implied for \_\_\_\_\_.

- a. perpendicularity/angularity
- b. angularity/perpendicularity
- c. angularity/parallelism
- d. both b. and c.

23. When rule #1 applies, a form tolerance must always be \_\_\_\_\_\_ than the \_\_\_\_\_\_ tolerance.

- a. less/size
- b. equal or less/bonus
- c. greater/position
- d. greater/orientation
- 24. Position can also control \_\_\_\_\_.
  - a. perpendicularity
  - b. datum precedence
  - c. circularity
  - d. roundness

25. When parallelism of a surface is controlled, \_\_\_\_\_\_ is also controlled.

- a. straightness
- b. flatness
- c. form
- d. all of the above

26. Runout can only be specified at \_\_\_\_\_, and must always be related to an axial \_\_\_\_\_.

- a. MMC/virtual condition
- b. MMC/tolerance
- c. RFS/datum
- d. both a. and b.

- 27. Straightness and circularity are examples of \_\_\_\_\_\_ controls, and are never related to a \_\_\_\_\_\_.
  - a. orientation/size tolerance
  - b. trigonometric/feature of size
  - c. surface/centerplane
  - d. form/datum

28. If a pin has a size specification of  $\emptyset$  15.0 ± 0.5 and a positional tolerance of  $\emptyset$  1.0 at MMC, what is the virtual condition?

- a. 14.5
- b. 15
- c. 15.5
- d. 16.5

29. If a hole has a size specification of  $\emptyset$  15.0 ± 0.5 and a positional tolerance of  $\emptyset$  0.5 at MMC, what is the maximum possible bonus tolerance available?

- a. 0.5
- b. 1
- c. 1.5
- d. 2

For questions 30-49, refer to the drawing below.



SECTION K-K

30.	The runout tolerance								
	a. should not have modifiers								
	b. should be changed to position								
	c. should have a diameter symbol								
	d. both a. and b.								
31.	The parallelism tolerance								
	a. is correct because it refers to a datum								
	b. is unnecessary								
	c. should be referenced to datum B at MMC								
	d. should be changed to total runout								
32.	If datum B is pressed into the mating part, it should probably be simulated using a								
	a. LMC/variable								
	b. MMC/fixed								
	c. RFS/variable								
	d. MMC/variable								
33.	The perpendicularity tolerance								
	a. should always be less than the size tolerance								
	b. is unnecessary								
	c. is valid								
	d. should be changed to a position tolerance								
34.	The maximum bonus tolerance available on the position of the internal diameter is mm.								
	a. 0.2								
	b. 0.1								
	c. 0.05								
	d. 0								
35.	The maximum possible distance between datum A and the left side of the part is mm.								
	a. 5.05								
	b. 5.1								
	c. 5.15								
	d. 5								
36.	With respect to the position tolerance, the maximum datum shift on datum B is mm.								
	a. 0								
	b. 0.025								
	c. 0.05								
	d. 0.1								
37.	Assuming a correct datum reference, if the runout tolerance were increased to 0.8 it would								
	a. control circularity also								
	b. control only coaxiality								
	c. be illegal								
	d. both a. and b.								
38.	With datum B simulated RFS, the worst-case outer boundary on the 12.2 diameter would be mm.								
	a. 12.2								
	b. 12.35								
	c. 12.4								

d. 12.5

39. With datum B simulated RFS, the worst-case axial offset on the 12.2 diameter would be \_\_\_\_\_ mm.

- a. 0.05
- b. 0.15
- c. 0.3
- d. 0.4

40. If the RFS modifiers were changed to MMC on the position tolerance and on the datum B reference on the 6.5 diameter, the worst-case inner boundary on the 6.5 diameter would be \_\_\_\_\_ mm.

- a. 6.2
- b. 6.3
- c. 6.4
- d. 6.5

41. If the RFS modifiers were changed to MMC on the position tolerance and on the datum B reference on the 6.5 diameter, the worst-case offset between datum axis B and the axis of the 6.5 diameter would be \_\_\_\_\_ mm.

- a. 0.05
- b. 0.15
- c. 0.2
- d. 0.4

42. If the RFS modifiers were changed to MMC on the position tolerance and on the datum B reference on the 6.5 diameter, the worst-case resultant condition on the 6.5 diameter would be \_\_\_\_\_ mm.

- a. 6.7
- b. 6.8
- c. 6.9
- d. 7

43. If the RFS modifier were changed to LMC on the position tolerance on the 6.5 diameter, the worst-case resultant condition on the 6.5 diameter would be \_\_\_\_\_ mm.

- a. 6.2
- b. 6.3
- c. 6.35
- d. 6.4

44. If the RFS modifiers were changed to LMC only on the position tolerance on the 6.5 diameter, the minimum wall thickness between the 6.5 diameter and the datum B diameter would be \_\_\_\_\_\_ mm.

- a. 1.1
- b. 1.15
- c. 1.8
- d. 2.4
- 45. If the print were based on ASME Y14.5M-1994, \_\_\_\_\_
  - a. the use of the RFS symbol would be illegal
  - b. the datum feature symbol would be different
  - c. the interpretation of rule number 5 would be different
  - d. both a. and b.
- 46. The flatness specification \_\_\_\_\_.
  - a. is valid
  - b. should be changed to 1.2
  - c. should be changed to parallelism
  - d. is unnecessary

- 47. Assuming datum B is simulated RFS, if the runout tolerance were correctly changed to a concentricity tolerance it would be \_\_\_\_\_\_.
  - a. more restrictive
  - b. less restrictive
  - c. the same interpretation
  - d. incorrect
- 48. If the RFS modifiers were changed to MMC on the position tolerance and datum B reference on the 6.5 diameter, the maximum bonus tolerance on the 6.5 diameter would be \_\_\_\_\_ mm.
  - a. 0.05
  - b. 0.1
  - c. 0.15
  - d. 0.2
- 49. If the RFS modifiers were changed to MMC on the position tolerance and on the datum B reference, the maximum wall thickness between datum feature B the 6.5 diameter would be \_\_\_\_\_ mm.
  - a. 0.5
  - b. 1.4
  - c. 1.5
  - d. 2

50-53 refer to the drawing below.



50. Datum C establishes a \_\_\_\_

- a. planar datum
- b. center plane datum
- c. datum axis
- d. sixth degree of freedom

51. The maximum height of the part is \_\_\_\_\_ mm.

- a. 40.16
- b. 40.8
- c. 40.2
- d. 40

52. The maximum allowable form error on the top surface of the part is \_\_\_\_\_ mm.

- a. 0.16
- b. 0.8
- c. 0.2
- d. 0.1

53. The second segment of the feature control frame controls \_\_\_\_\_\_.

- a. form
- b. size
- c. orientation
- d. both a. and c.

54-60 refer to the drawings below.



54. The functional virtual condition calculated to ensure assembly with the mating part on both prints is \_\_\_\_\_ mm.

a. 14

- b. 14.1
- c. 14.25
- d. 14.5

55. The minimum material thickness between the two rightmost holes on both prints is \_\_\_\_\_ mm.

- a. 11.1
- b. 11.6
- c. 11.7
- d. 11.9

56. The maximum cylindricity error on the four holes in both prints is \_\_\_\_\_ mm.

- a. 0.15
- b. 0.20
- c. 0.25
- d. 0.30

- 57. The feature relating tolerance zone framework in the left print controls \_\_\_\_\_\_.
  - a. distance to datum B
  - b. distance between the holes
  - c. orientation to datums A and B
  - d. all of the above
- 58. The feature relating tolerance zone framework in the right print controls \_\_\_\_\_\_.
  - a. distance to datum B
  - b. distance between the holes
  - c. orientation to datums A and B
  - d. all of the above
- 59. The pattern locating tolerance zone framework on the left print is \_\_\_\_\_\_ the right print.
  - a. more restrictive than
  - b. less restrictive than
  - c. the same interpretation as
  - d. more difficult to inspect than

60. The feature relating tolerance zone framework on the left print is \_\_\_\_\_\_ the right print.

- a. more restrictive than
- b. less restrictive than
- c. the same interpretation as
- d. more difficult to inspect than

Name \_\_\_

1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30.

Division \_\_\_\_\_

| Date         |    |    |    | _  |
|--------------|----|----|----|----|
| Dept         |    |    |    |    |
| sponse Sheet |    |    |    |    |
|              | a. | b. | c. | d. |
| 31.          | 0  | 0  | 0  | 0  |

**GD&T** Certification Examination

| a.                                      | b.                                      | c.                                      | d.                                      |  | a.                                      | b.                                      | c.                                      | d.                                      |
|---|---|---|---|--|---|---|---|---|
| 000000000000000000000000000000000000000 | 000000000000000000000000000000000000000 | 000000000000000000000000000000000000000 | 000000000000000000000000000000000000000 | 31.<br>32.<br>33.<br>34.<br>35.<br>36.<br>37.<br>38.<br>39.<br>40.<br>41.<br>42.<br>43.<br>44.<br>45.<br>46.<br>47.<br>48.<br>49.<br>50.<br>51.<br>52.<br>53.<br>54.<br>55.<br>56.<br>57.<br>58.<br>59.<br>60. | 000000000000000000000000000000000000000 | 000000000000000000000000000000000000000 | 000000000000000000000000000000000000000 | 000000000000000000000000000000000000000 |

| Name       | Date         |              |             |        | _          |              |             |              |              |
|------------|--------------|--------------|-------------|--------|------------|--------------|-------------|--------------|--------------|
| Division   |              |              |             |        | Dept       | Dept         |             |              |              |
|            |              |              |             |        | Answer Key |              |             |              |              |
|            | a.           | b.           | c.          | d.     |            | a.           | b.          | c.           | d.           |
| 1.         | 0            | 0            | 0           | 0      | 31.        | 0            | 0           | 0            | 0            |
| 2.         | 0            | 0            | 0           | 0      | 32.        | 0            | 0           | 0            | 0            |
| 3.         | 0            | 0            | 0           | 0      | 33.        | 0            | 0           | 0            | 0            |
| 4.         | 0            | 0            | 0           | 0      | 34.        | 0            | O           | 0            | 0            |
| 5.         | $\odot$      | 0            | 0           | 0      | 35.        | 0<br>@       | <b>.</b>    | 0            | 0            |
| 6.<br>7    | $\circ$      | $\mathbf{O}$ |             | 0<br>@ | 36.<br>27  |              |             | $\mathbf{O}$ | $\mathbf{O}$ |
| 7.         | Õ            | 0            | Õ           | Õ      | 37.        | 0            | Õ           | õ            | 0            |
| 9.         | Õ            | Õ            | 0           | Õ      | 30.<br>39. | Õ            | 0           | Õ            | Õ            |
| 10.        | 0            | 0            | 0           | 0      | 40.        | 0            | 0           | 0            | 0            |
| 11.        | 0            | 0            | 0           | 0      | 41.        | 0            | 0           | 0            | 0            |
| 12.        | 0            | 0            | 0           | 0      | 42.        | 0            | 0           | 0            | 0            |
| 13.        | 0            | 0            | 0           | 0      | 43.        | 0            | 0           | 0            | 0            |
| 14.        | 0            | 0            | 0           | 0      | 44.        | 0            | 0           | 0            | 0            |
| 15.        | 0            | ©            | 0<br>@      | 0      | 45.        | 0            | ()<br>()    | 0            | 0<br>@       |
| 16.        | $\mathbf{O}$ | $\mathbf{O}$ |             | 0<br>@ | 46.        | $\mathbf{O}$ | 0<br>@      | $\circ$      |              |
| 17.        | $\tilde{O}$  | $\tilde{O}$  | $\tilde{O}$ | 0      | 47.        | Õ            | 0           | $\tilde{O}$  | $\tilde{O}$  |
| 18.        | Õ            | õ            | 0           | Õ      | 48.        | õ            | 0           | Õ            | õ            |
| 20.        | Õ            | 0            | Õ           | Õ      | 50.        | Õ            | 0           | Õ            | Õ            |
| 21.        | 0            | 0            | 0           | 0      | 51.        | 0            | 0           | 0            | 0            |
| 22.        | 0            | 0            | 0           | 0      | 52.        | 0            | 0           | 0            | 0            |
| 23.        | 0            | 0            | 0           | 0      | 53.        | 0            | 0           | 0            | 0            |
| 24.        | 0            | 0            | 0           | 0      | 54.        | 0            | 0           | 0            | 0            |
| 25.        | 0<br>O       | U<br>C       | 0<br>©      | 0      | 55.        | 0            | 0<br>O      | 0<br>©       | 0<br>C       |
| 26.        | 0            | 0            | ()<br>()    |        | 56.        | $\bigcirc$   |             | ()<br>()     | $\mathbf{O}$ |
| 27.        | $\bigcirc$   | $\bigcirc$   | $\bigcirc$  | @<br>@ | 57.        | $\circ$      | ©<br>∩      | $\bigcirc$   | 0<br>@       |
| 28.<br>29  | $\tilde{O}$  | 0<br>0       | $\tilde{O}$ | Ő      | 58.<br>50  | $\tilde{O}$  | $\tilde{O}$ | ©            | Ő            |
| 29.<br>30. | ©            | Õ            | õ           | õ      | 60.        | õ            | 0           | õ            | õ            |