

Technical Issues and Update

Mark S. Graham, NRCA Vice President of Technical Services



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- | | |
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NRCA technical committees and task forces

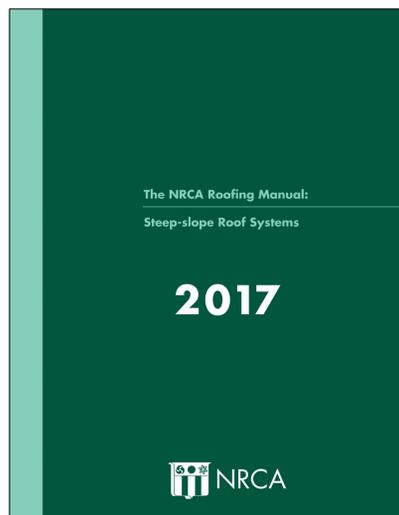
- Technical Operations Committee (TOC)
- Manual Update Committee
- Manufacturers Spec Review Task Force
- QA/QC Guidelines Task Force
- Repair Manual Task Force
- Vegetative Roof Manual Task Force

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The NRCA Roofing Manual: Steep-slope Roof Systems-2017

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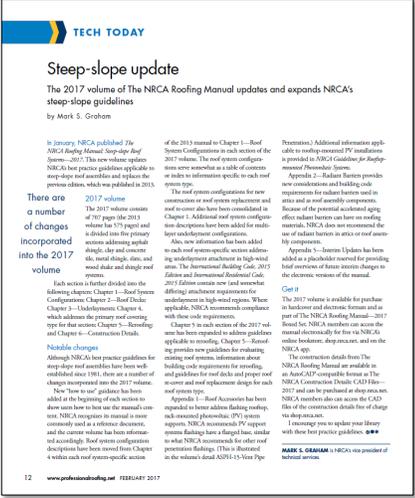
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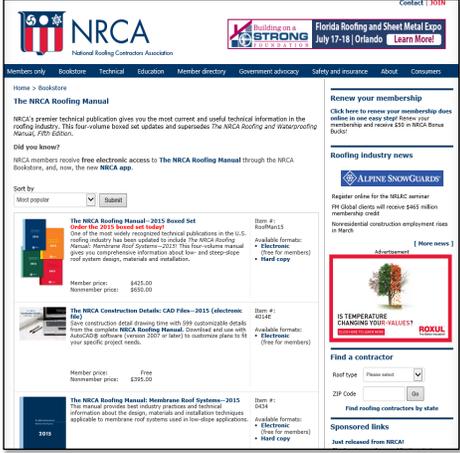
The NRCA Roofing Manual - 2017



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Manual online

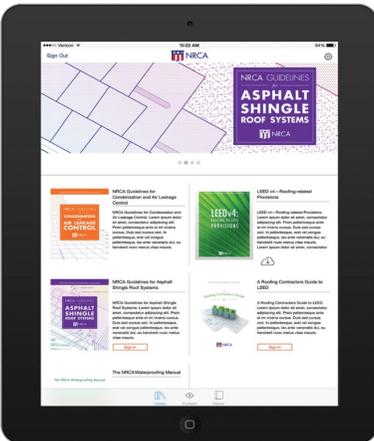


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- NRCA App available on the Apple Store and Google Play Store for tablets
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- The NRCA Roofing Manual is viewable to NRCA members
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Guidelines for Air Retarders in Roof Assemblies

- Ch. 1: IECC and ASHRAE
- Ch. 2: Industry research
- Ch. 3: Recommendations

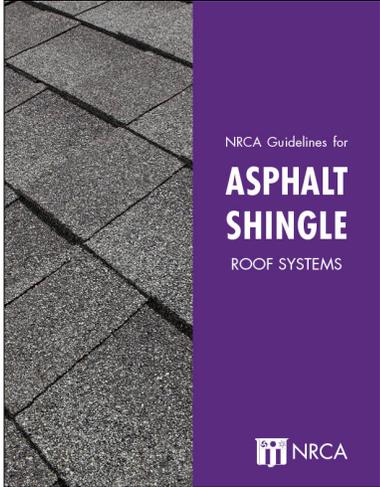
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Some key points...
Air retarders

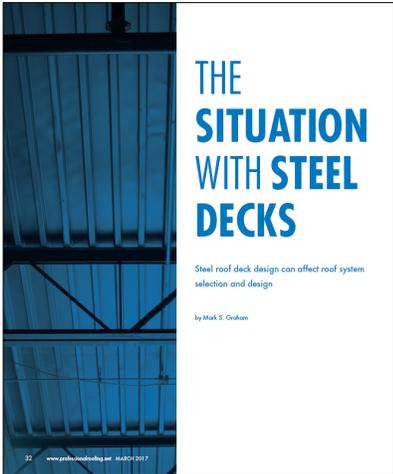
- Building and roof system designers are responsible for proper design....
- Construction Documents should clearly denote locations, materials, application methods and details
- NRCA considers a continuous, air-impermeable roof membrane to function as an air retarder
 - Built-up roof system
 - Polymer-modified bitumen roof system
 - Single-ply membrane roof system

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NRCA Guidelines for Asphalt Shingle Roof Systems

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Steel roof deck design

- SDI Design Manual
- AISI S100, "Specifications for the Design of Cold-formed Steel Structural Members"
- ANSI/SDI RD1.0-2006, "Standard for Steel Roof Deck"
- ANSI/SDI RD-2010, "Standard for Steel Roof Deck"
- *SDI Roof Deck Design Manual, First Edition* (Nov. 2012)

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Steel roof deck design

Wind uplift resistance

- Minimum 30 psf uplift (uniform loading)
- Minimum 45 psf uplift (uniform loading) at roof overhangs

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SDI bulletin

2009

STEEL DECK INSTITUTE
Publications

ATTACHMENT OF ROOFING MEMBRANES TO STEEL DECK

This document has been published by the Steel Deck Institute (SDI) as a position paper in response to discussions taking place in the roofing community about the screw attachment of roofing membranes to steel deck following line patterns spaced at up to 12 ft (3.66 m). While the membrane itself has the performance characteristics to accommodate this type of membrane loading, the existing design methods for steel deck under wind uplift are typically based on the uniform application of the wind suction to the deck. The larger spacing of the steel roof deck used for commercial buildings in North America is profiled with 1 1/2" (38 mm) flutes, with the structural supports usually spaced between 5' 0" (1.52 m) and 6' 8" (2.03 m). Under uplift conditions, the attachment of the roofing membrane along lines with large spacing could produce localized loads that can exceed the capacity of the deck, whereas those same loads applied uniformly on the surface of the deck would be acceptable.

The SDI's research is looking at roofing systems that incorporate wide membrane sheets attached to the steel deck following line patterns spaced at up to 12 ft (3.66 m). While the membrane itself has the performance characteristics to accommodate this type of membrane loading, the existing design methods for steel deck under wind uplift are typically based on the uniform application of the wind suction to the deck. The larger spacing of the steel roof deck used for commercial buildings in North America is profiled with 1 1/2" (38 mm) flutes, with the structural supports usually spaced between 5' 0" (1.52 m) and 6' 8" (2.03 m). Under uplift conditions, the attachment of the roofing membrane along lines with large spacing could produce localized loads that can exceed the capacity of the deck, whereas those same loads applied uniformly on the surface of the deck would be acceptable.

The strength of screwed connection between the membrane and the steel deck, as well as the strength of screwed, nailed, or welded attachment of the steel deck to the structural supports can be computed according to the North American Specification for the Design of Cold-Formed Steel Structural Members. These design values are based on the specified minimum mechanical properties (i.e. base steel thickness and yield strength) specified for the steel sheet metal deck, and should be lower than the strength determined by field testing. The use of field test results for properties such as the pull-out strength of a screw into a steel deck needs to be recognized that the properties of the steel deck can be higher than the minimum limits specified by the steel specification. Therefore, field testing results must be adjusted accordingly to account for the difference between the actual properties of the deck and the minimum properties of the steel according to the material specification used in design.

The screw fastening of wide roofing membranes up to 12 ft and the corresponding spacing of the lines of screws holding the membrane on the deck, will have a very different effect on the deck and structural supports than a membrane that is attached over its entire surface. The screws will produce a line load along the deck instead of a uniform load of the entire deck surface. The line loads can be perpendicular or parallel to the deck flutes depending on the orientation of the membrane; each condition can have different implications of the loading that is applied to the deck.

If the roofing membrane seam is perpendicular to the flutes of the deck, as illustrated in Figure 1, there are two special conditions that need to be considered:

1. If the membrane seam occurs at the mid-span of the steel deck and
2. If the membrane seam occurs at the structural support (joist).

1

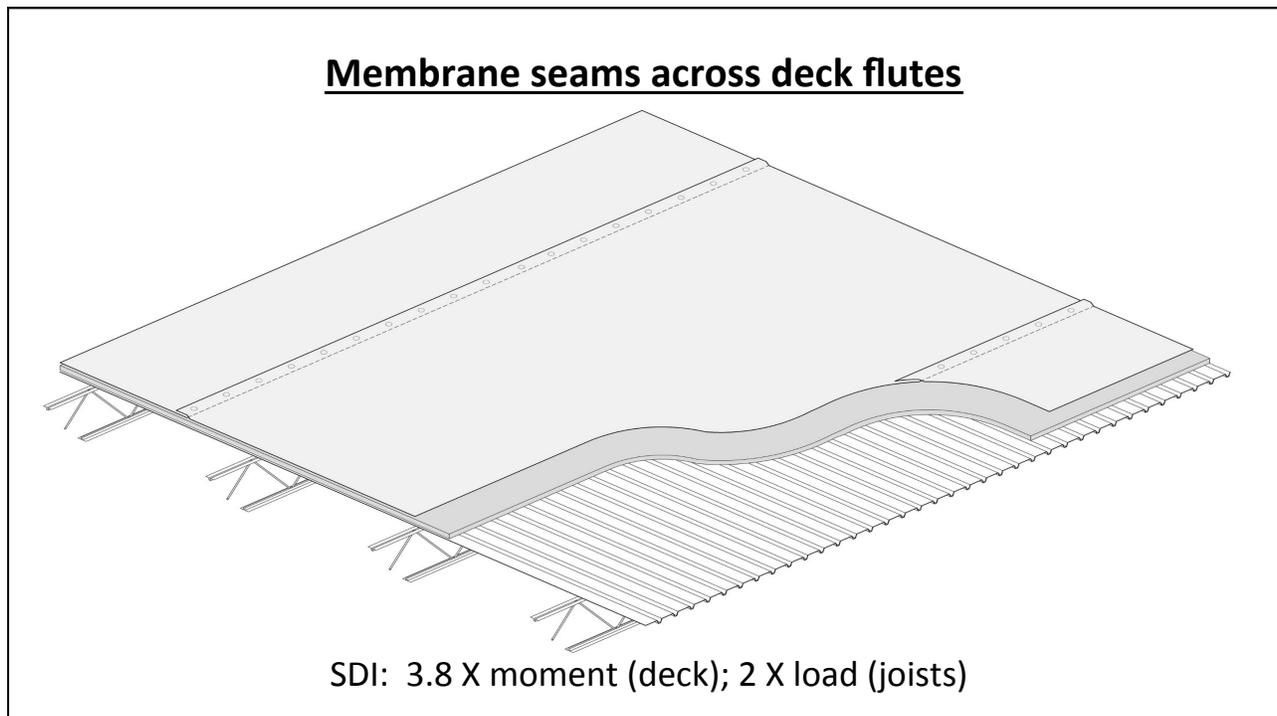
- Decks designed for joist spacing between 5' and 6' 8" o.c.
- Deck designed for uniform loading
- Seam-fastened single-ply membranes are a concern

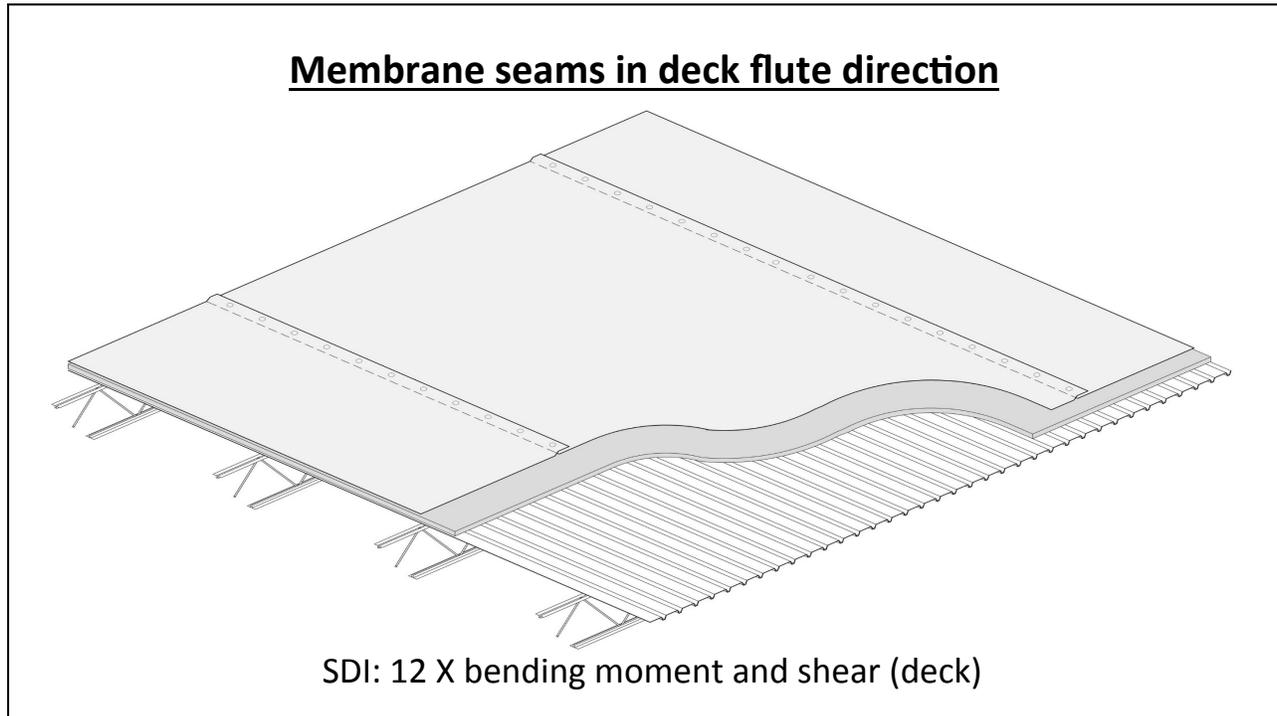
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SDI bulletin -- Conclusion

“...SDI does not recommend the use of roofing membranes attached to the steel deck using line patterns with large spacing unless a structural engineer has reviewed the adequacy of the steel deck and the structural supports to resist to wind uplift loads transmitted along the lines of attachment. Those lines of attachment shall only be perpendicular to the flutes of the deck.”

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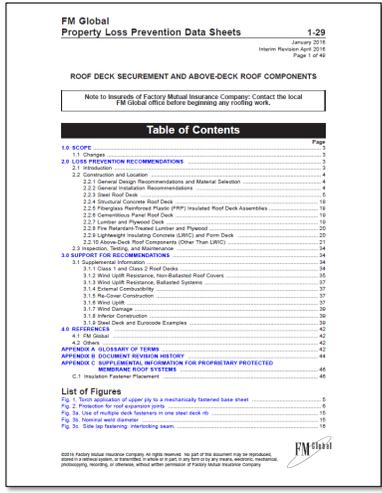
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FM 1-29 has been updated

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Revised/now criteria:

- Steel roof decks:
 - Uniformly-distributed loading
 - Concentrated loading
- Lightweight structural concrete

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FM Global
Property Loss Prevention Data Sheets

1-29
January 2016
Interim Revision April 2016
Page 1 of 44

2.2.3.2 When designing the steel deck, give consideration to the needed wind rating, and how the load is applied (concentrated vs. uniformly distributed) from the above-deck components to the deck. Where the distance between rows of roof cover fasteners is greater than half the deck span, treat as a concentrated load.

As an alternative to using Tables 1A or 1B for concentrated loads, a performance-based approach may be used if calculations are conducted by a licensed S.E. or P.E. in structural engineering. This applies to situations where the distance between rows of roof cover fasteners is greater than one-half the deck span. Make the following assumptions:

- A. Assume a 3-span structural condition.
- B. Assume the first row of roof cover fasteners is located at mid-point of the first deck span.
- C. Assume maximum allowable stresses are determined using allowable strength design (ASD) in accordance with AISI S100-2012, or comparable standard outside the United States

Due to the more brittle nature of higher grade steels, the maximum yield stress used in the analysis is 60,000 psi (414 MPa), even for 80,000 psi (552 MPa) yield stress steel. Use Tables 1A through 1E as follows to facilitate deck selection:

Table 1A. Use for roof covers or base plies that are mechanically fastened to the steel deck when the distance between rows of roof cover fasteners is more than half the deck span and the deck is 1-1/2 in. (38 mm) deep, wide rib (Type B) with a minimum yield stress of 33,000 psi (228 MPa).

Table 1B. Use for roof covers or base plies that are mechanically fastened to the steel deck when the distance between rows of roof cover fasteners is more than half the deck span and the deck is 1-1/2 in. (38 mm) deep, wide rib (Type B) with a minimum yield stress of 60,000 psi (414 MPa).

Note: Where the minimum specified yield stress is between 33,000 psi (228 MPa) and 60,000 psi (414 MPa), it is reasonably accurate to interpolate the maximum deck span linearly based on Tables 1A and 1B.

Table 1C. Use for roof covers or base plies that are adhered to insulation or cover board, or mechanically fastened to the steel deck when the distance between rows of roof cover fasteners is one-half the deck span or less and the deck is 1-1/2 in. (38 mm) deep, wide rib (Type B) with minimum yield stresses of 33,000 psi (228 MPa) and ultimate wind ratings of from 60 to 225 psf (2.9 to 10.8 kPa).

**FM Global
Property Loss Prevention Data Sheets** 1-29

Table 1C. Maximum Steel Deck Span (ft) for 1½ in. (38 mm) Deep, Wide Rib (Type B) Steel Deck with an Adhered Roof Cover, for Wind Ratings from 60 to 225 psf (2.9 to 10.8 kPa)
(NOTE: Use this table when the distance between rows of roof cover fasteners is one-half the deck span or less. Green font indicates that deflection governs over bending stress.)

Yield Stress psi	Deck Gauge	Ultimate Wind Rating per RoofNav (psf)											
		Maximum Span (ft)											
		60	75	90	105	120	135	150	165	180	195	210	225
33,000	22	7.10	7.10	7.10	7.10	7.07	6.67	6.33	6.03	5.78	5.55	5.35	5.17
	20	7.78	7.78	7.78	7.78	7.78	7.43	7.05	6.72	6.44	6.18	5.96	5.76
	18	9.08	9.08	9.08	9.08	9.08	8.66	8.22	7.84	7.50	7.21	6.95	6.71
40,000	16	10.36	10.36	10.36	10.36	10.36	9.89	9.38	8.94	8.56	8.23	7.93	7.66
	22	7.10	7.10	7.10	7.10	7.10	7.10	6.96	6.67	6.35	6.10	5.88	5.68
	20	7.78	7.78	7.78	7.78	7.78	7.78	7.76	7.40	7.08	6.80	6.56	6.33
45,000	18	9.08	9.08	9.08	9.08	9.08	9.08	9.04	8.62	8.25	7.93	7.64	7.38
	16	10.36	10.36	10.36	10.36	10.36	10.36	10.32	9.84	9.42	9.05	8.72	8.43
	22	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.04	6.74	6.48	6.24	6.03
50,000	20	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.51	7.22	6.95	6.72
	18	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	8.76	8.41	8.11	7.83
	16	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	9.99	9.60	9.25	8.94
55,000	22	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	6.93	6.66	6.42	6.20
	20	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.72	7.42	7.15	6.91
	18	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.00	8.65	8.33	8.05
60,000 +	16	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.28	9.87	9.51	9.19
	22	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	6.90	6.67
	20	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.69	7.43
60,000 +	18	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	8.97	8.66
	16	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.24	9.89
	22	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	7.10	6.97
60,000 +	20	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.78	7.77
	18	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.06
	16	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.36	10.34

Green font indicates that deflection governs over bending stress.

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**FM Global
Property Loss Prevention Data Sheets** 1-29

January 2016
Interim Revision April 2016

Table 1A. Maximum Steel Deck Span (ft) for 1½ in. (38 mm) Deep, 33,000 psi (228 MPa) Yield Stress with a Mechanically Fastened Roof Cover
(Note: Use this table when the distance between rows of roof cover fasteners is more than one-half the deck span.)

Max Deck Spans By Wind Rating/Fastener Spacing, Sheet Gauge for 33 ksi, 1½ in. Deep Wide Rib Deck

Roof Cover Fastener Row Spacing (ft)	Gauge	Wind Rating [psf]																			
		330	315	300	285	270	255	240	225	210	195	180	165	150	135	120	105	90	75	60	
3.5	18	4.5	5.5	5.5	5.5	5.5	5.5	6	6	6	6	6	6	6	6	6	6	6	6	6	
	20	-	4	4	4.5	4.5	4.5	5	5.5	5.5	5.5	6	6	6	6	6	6	6	6	6	
	22	-	-	-	-	-	4	4	4.5	4.5	4.5	5.5	5.5	5.5	6	6	6	6	6	6	
4	18	4.5	4.5	5	5	5	6	6	6	6	6	6	6	6	6	6	6	6	6	6	
	20	-	-	-	-	4	4.5	4.5	5	5.5	6	6	6	6	6	6	6	6	6	6	
	22	-	-	-	-	-	-	-	-	4	4.5	5	5	6	6	6	6	6	6	6	
4.5	18	-	4	4	4.5	5	5	5.5	6	6	6	6	6	6	6	6	6	6	6	6	
	20	-	-	-	-	-	-	-	4	4	5	5	5.5	6	6	6	6	6	6	6	
	22	-	-	-	-	-	-	-	-	-	4	4.5	5	5.5	6	6	6	6	6	6	
5	18	-	-	-	4	4	4.5	5	5	5.5	6	6	6	6	6	6	6	6	6	6	
	20	-	-	-	-	-	-	-	4	4.5	5	5.5	6	6	6	6	6	6	6	6	
	22	-	-	-	-	-	-	-	-	-	4	4.5	5	5.5	6	6	6	6	6	6	
5.5	18	-	-	-	-	-	-	4	4.5	5	5.5	6	6	6	6	6	6	6	6	6	
	20	-	-	-	-	-	-	-	-	-	4	4.5	5	6	6	6	6	6	6	6	
	22	-	-	-	-	-	-	-	-	-	-	4	4.5	5	6	6	6	6	6	6	
6	18	-	-	-	-	-	-	-	-	4	5	5.5	6	6	6	6	6	6	6	6	
	20	-	-	-	-	-	-	-	-	-	-	4.5	5.5	6	6	6	6	6	6	6	
	22	-	-	-	-	-	-	-	-	-	-	-	4.5	5.5	6	6	6	6	6	6	
6.5	18	-	-	-	-	-	-	-	-	-	-	-	-	4.5	5.5	6	6	6	6	6	
	20	-	-	-	-	-	-	-	-	-	4	4.5	5.5	6	6	6	6	6	6	6	
	22	-	-	-	-	-	-	-	-	-	-	-	-	4.5	5.5	6	6	6	6	6	
7	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.5	5.5	6	6	6	
	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.5	6	6	6	6
	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.5	5.5	6	6
7.5	18	-	-	-	-	-	-	-	-	-	-	-	-	4	5.5	6	6	6	6	6	
	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4	5	6	6	6	6
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FM Global
Property Loss Prevention Data Sheets

1-29
January 2016
Interim Revision April 2016
Page 1 of 42

Table 1B. Maximum Steel Deck Span (ft) for 1 1/2 in. (.38 mm) Deep, Yield Stress ≥ 60,000 psi (414 MPa) with a mechanically fastened Roof Cover (continued)
(Note: Use this table when the distance between rows of roof cover fasteners is more than one-half the deck span.)

Max Deck Spans By Wind Rating/Fastener Spacing, Sheet Gauge for 80 ksi, 1 1/2 in. Deep Wide Rib Deck

Roof Cover Fastener Row Spacing (ft)	Gauge	Wind Rating [psf]																		
		330	315	300	285	270	255	240	225	210	195	180	165	150	135	120	105	90	75	60
8.5	18	-	-	-	-	-	4	4	4.5	5	5.5	6	6	6	6	6	6	6	6	6
	20	-	-	-	-	-	-	-	-	4	4	4.5	5.5	6	6	6	6	6	6	6
	22	-	-	-	-	-	-	-	-	-	-	-	4	4.5	5	5.5	6	6	6	6
9	18	-	-	-	-	-	-	4	4	4.5	5	5.5	6	6	6	6	6	6	6	6
	20	-	-	-	-	-	-	-	-	-	4	4.5	5	5.5	6	6	6	6	6	6
	22	-	-	-	-	-	-	-	-	-	-	-	4	4.5	5	5.5	6	6	6	6
9.5	18	-	-	-	-	-	-	-	4	4	4.5	5	5.5	6	6	6	6	6	6	6
	20	-	-	-	-	-	-	-	-	-	4	4	4.5	5	6	6	6	6	6	6
	22	-	-	-	-	-	-	-	-	-	-	-	4	4.5	5	6	6	6	6	6
10	18	-	-	-	-	-	-	-	-	4	4	4.5	5	6	6	6	6	6	6	6
	20	-	-	-	-	-	-	-	-	-	4	4.5	5	6	6	6	6	6	6	6
	22	-	-	-	-	-	-	-	-	-	-	4	4.5	5.5	6	6	6	6	6	6
10.5	18	-	-	-	-	-	-	-	4	4	4.5	4.5	5	5.5	6	6	6	6	6	6
	20	-	-	-	-	-	-	-	-	-	-	4	4	4.5	5	6	6	6	6	6
	22	-	-	-	-	-	-	-	-	-	-	-	4	4.5	5.5	6	6	6	6	6
11	18	-	-	-	-	-	-	-	-	4	4	4.5	5	6	6	6	6	6	6	6
	20	-	-	-	-	-	-	-	-	-	-	-	4	4.5	5	5.5	6	6	6	6
	22	-	-	-	-	-	-	-	-	-	-	-	-	4	4.5	5.5	6	6	6	6
11.5	18	-	-	-	-	-	-	-	-	-	4	4	4.5	5	5.5	6	6	6	6	6
	20	-	-	-	-	-	-	-	-	-	-	4	4	4.5	5	5.5	6	6	6	6
	22	-	-	-	-	-	-	-	-	-	-	-	4	4.5	5	5.5	6	6	6	6
12	18	-	-	-	-	-	-	-	-	-	4	4	4.5	5	5.5	6	6	6	6	6
	20	-	-	-	-	-	-	-	-	-	-	-	-	4	4.5	5	6	6	6	6
	22	-	-	-	-	-	-	-	-	-	-	-	-	-	4	5	5.5	6	6	6
Roof Cover Fastener Row Spacing	Gauge	330	315	300	285	270	255	240	225	210	195	180	165	150	135	120	105	90	75	60
		Wind Rating [psf]																		

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FM Global
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1-29
January 2016

Table 1B. Maximum Steel Deck Span (ft) for 1 1/2 in. (.38 mm) Deep, Yield Stress ≥ 60,000 psi (414 MPa) with a mechanically fastened Roof Cover
(Note: Use this table when the distance between rows of roof cover fasteners is more than one-half the deck span.)

Max Deck Spans By Wind Rating/Fastener Spacing, Sheet Gauge for 80 ksi, 1 1/2 in. Deep Wide Rib Deck

Roof Cover Fastener Row Spacing (ft)	Gauge	Wind Rating [psf]																		
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3.5	18	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
	20	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
	22	5.5	5.5	5.5	5.5	5.5	5.5	6	6	6	6	6	6	6	6	6	6	6	6	6
4	18	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
	20	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
	22	4.5	5	5	5	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
4.5	18	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
	20	5.5	5.5	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
	22	4	4	4.5	5	5	5.5	5.5	6	6	6	6	6	6	6	6	6	6	6	6
5	18	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
	20	4.5	5	5.5	5.5	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
	22	-	4	4	4.5	4.5	5	5.5	6	6	6	6	6	6	6	6	6	6	6	6
5.5	18	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
	20	4	4.5	4.5	5	5.5	5.5	6	6	6	6	6	6	6	6	6	6	6	6	6
	22	-	-	-	-	4	4.5	5	5.5	6	6	6	6	6	6	6	6	6	6	6
6	18	5	5.5	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
	20	-	-	-	4	4.5	5	5.5	6	6	6	6	6	6	6	6	6	6	6	6
	22	-	-	-	-	-	-	4	4.5	5	5.5	6	6	6	6	6	6	6	6	6
6.5	18	4.5	5	5	5.5	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
	20	-	-	-	-	4	4.5	5	5.5	6	6	6	6	6	6	6	6	6	6	6
	22	-	-	-	-	-	-	-	-	4	5	5.5	6	6	6	6	6	6	6	6
7	18	-	4	4	4.5	5.5	6	6	6	6	6	6	6	6	6	6	6	6	6	6
	20	-	-	-	-	-	4	4	5	5.5	6	6	6	6	6	6	6	6	6	6
	22	-	-	-	-	-	-	-	-	-	4	4.5	5.5	6	6	6	6	6	6	6
7.5	18	-	-	-	4	4.5	4.5	5.5	6	6	6	6	6	6	6	6	6	6	6	6
	20	-	-	-	-	-	-	-	-	4	4.5	5.5	6	6	6	6	6	6	6	6
	22	-	-	-	-	-	-	-	-	-	-	4	4.5	6	6	6	6	6	6	6
8	18	-	-	-	-	4	4	4.5	5	6	6	6	6	6	6	6	6	6	6	6
	20	-	-	-	-	-	-	-	-	-	4	4.5	5.5	6	6	6	6	6	6	6
	22	-	-	-	-	-	-	-	-	-	-	-	4	5	6	6	6	6	6	6
Roof Cover Fastener Row Spacing	Gauge	330	315	300	285	270	255	240	225	210	195	180	165	150	135	120	105	90	75	60
		Wind Rating [psf]																		

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NRCA's recommendations

Uniformly-loaded vs. non-uniform, linear pattern loaded steel roof decks

New construction:

- Structural engineer awareness of roof system design
 - Note load pattern and steel's yield strength on structural drawings and shop drawings
- Roof system designer awareness of steel roof deck design

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NRCA's recommendations – cont.

Uniformly-loaded vs. non-uniform, linear pattern loaded steel roof decks

Reroofing:

- Realize steel roof decks are not likely designed to current SDI, FM Global and FM Approvals' standards
- If steel deck design cannot be verified:
 - Use narrow fastener row/seam spacing (rows/seams \leq joist spacing)
 - Use a uniform uplift loading roof system (BUR, MB, adhered single ply)

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Fastener pull-out tests...

There is little correlation between fastener pull-out resistance and a steel roof deck's yield strength and uplift (bending) strength

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Although roofing contractors sometimes are given the responsibility of inspecting and accepting steel roof decks to receive a new roof system, determining a roof deck's design adequacy is beyond the expertise of most roofing contractors.

This determination is best made during a project's design phase.

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CONSTRUCTION ISSUES

discussion of construction issues and techniques

Are Your Roof Members Overstressed?

By James M. Fisher, Ph.D., FRC, FASCE, and Thomas Stone, Ph.D., P.E., S.E., FASCE

James M. Fisher is Vice President, Director, Commercial Development Group, International WFL and Consulting Engineer in the State of Florida, registered as a Professional Engineer. Thomas Stone is President of Stone and Company, Inc., and National Director of WFL and Consulting Engineer in the State of Florida, registered as a Professional Engineer.



Membrane roof systems installed on steel roof decks traditionally result in a weather-tight membrane in the steel roof deck and underlying supporting structure (e.g., steel joists). For example, in a hot-applied membrane roof system—which has been used commonly in the U.S. roofing industry for more than 125 years—the built-up membrane is continuously adhered to rigid/semi-rigid members. The rigid/semi-rigid members, which is used to span the steel deck's ribs, is mechanically attached to the steel roof deck in a closely spaced pattern (e.g., 1 fanner per every 2 supports), resulting in a more uniform load path.

In the 1970s, single-ply membrane roof systems were first introduced into the U.S. roofing market. By the late 1970s, the water-tight, mechanical attachment method of installation was first introduced. With this installation method, the single-ply membrane was mechanically attached along its outer edges into the roof deck, which results in a larger tributary load per fanner and placement of fans into lower load-bearing configurations of the roof deck and underlying supporting structure. When first introduced, membrane roof systems were fastened single-ply membrane roof systems typically used for flat roofs, resulting in a more uniform load path of five feet on-center. Since the early 2000s, single-ply membrane roof systems have become wider, with 10-foot-wide sheets more commonplace—resulting in more of mechanical fans spaced at 10 feet on-center.

Currently, single-ply membrane roof systems have made membrane construction both fast and perform membrane membrane systems in a similar time. The water-tight, mechanically attached method of installation also has somewhat requirements related to application. The National Building Contractors Association (NBCA) and International Brotherhood of Roofers (IBR) have both established single-ply membrane roof systems make-up the majority of membrane roof systems currently installed.

With the growing emphasis on wind resistance in design, a closer look at how water-tight mechanically attached single-ply membrane roof systems interact with steel roof deck and joint construction is vital.

A common method of single-ply membrane attachment is shown in Figure 1. A common placement of mechanical fasteners is shown in Figure 2. These conventional fasteners can severely overstress the steel deck and may also cause the steel joist below the deck to be overstressed under uplift loading. The balance of each fastening system, which the roof system is subjected to uplift loading, is shown in Figure 3. The current best attachment is for the membrane installer to mechanically fasten the membrane to the deck while along the edge of the sheet with no spread up the roof installation, thereby lowering installation costs. Unfortunately, the Structural Engineer of Record, and the steel deck and joist supplier, are usually unaware of the conventional load pattern of the roof membrane attachment. In fact, the architect of record may not be aware of the ramifications of such attachments. The Architectural writing specifications now simply state that the roof membrane shall be installed per manufacturer recommendations. The writing installer/contractor is the one who generally decides on the exact layout of the membrane deck on the roof. That decision is made based on what layout can be installed in the shortest and least expensive

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Some numbers...

- Average life of a commercial roof: 17.4 years
- IRS allowable roof depreciation: 39.5 years

We need to be manufacturing, designing, installing and maintaining well beyond “average”

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NRCA Roofing Industry Regional Summit

15



Some (more) numbers...

- UL certified roofing products: 65,000+
- FM Approvals approved assemblies: 953,500+

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